

# Newtonian Noise Measurement with TOrsion-Bar Antenna

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9/11/21 KAGRA FWG open meeting @ online

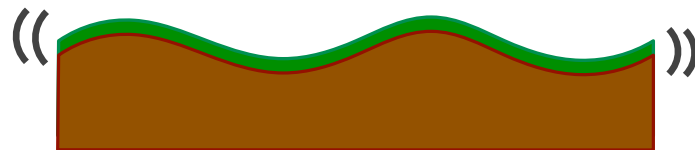


# Newtonian Noise

Newtonian noise: comes from local gravity gradient fluctuation

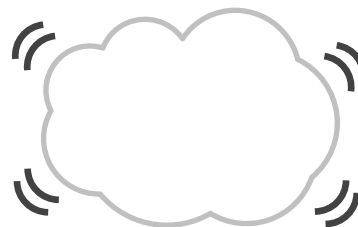
- Seismic waves

- ▶ body wave
- ▶ surface wave
- ▶ etc.



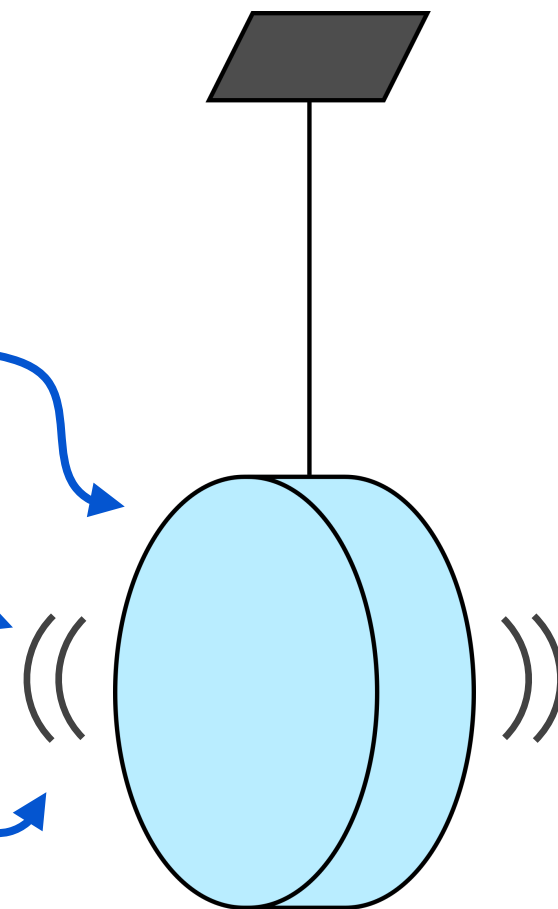
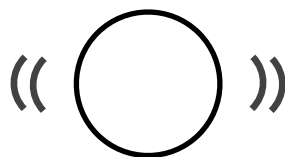
- Atmospheric fluctuation

- ▶ temperature fluctuation
- ▶ infrasound waves
- ▶ etc.



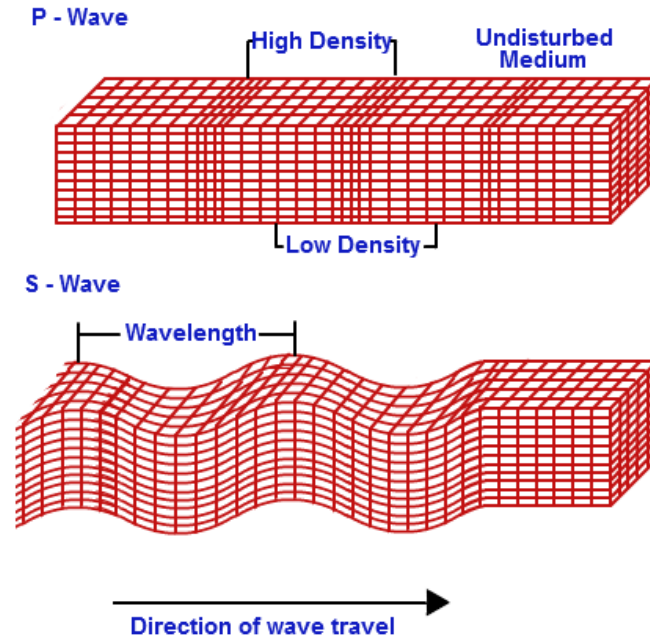
- Moving masses

- ▶ water
- ▶ human activity
- ▶ etc.



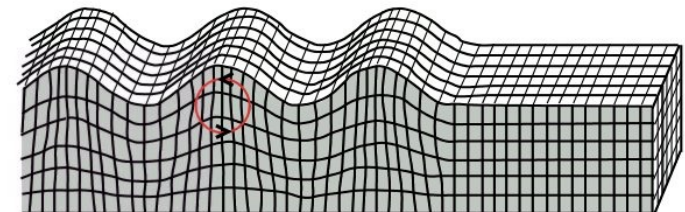
# Seismic Wave

- Seismic waves:
  - ◉ body wave
    - P-wave: compressional wave
    - S-wave: shear wave
    - ▶ propagate through media
  - ◉ surface waves
    - Rayleigh wave
    - ▶ propagates on the surface of media
- can be divided by **surface** and **bulk** contribution



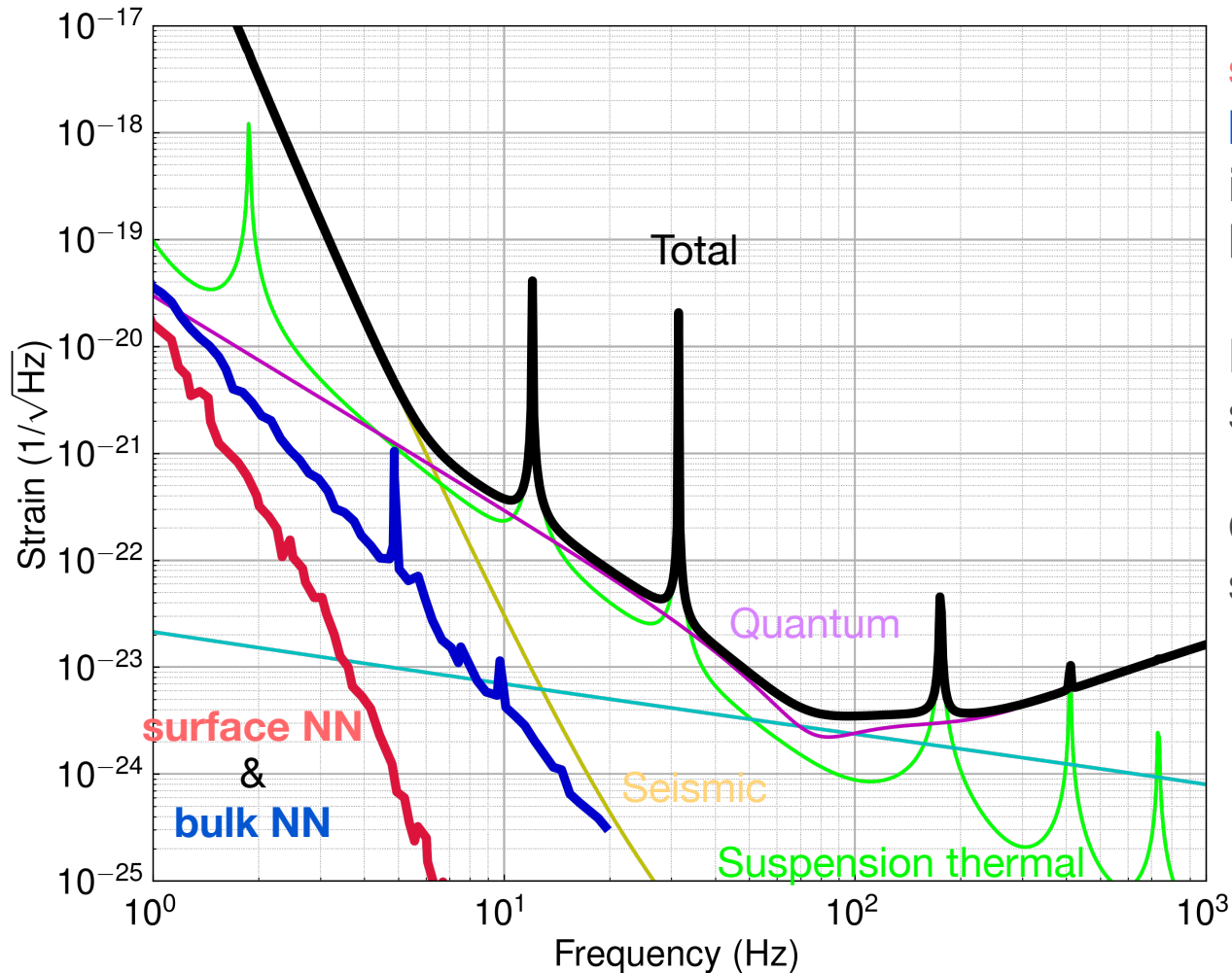
<http://physics.tutorcircle.com/waves/p-wave.html>

Rayleigh Wave



[https://earthquake.usgs.gov/learn/glossary/images/rayleigh\\_web.jpg](https://earthquake.usgs.gov/learn/glossary/images/rayleigh_web.jpg)

# NN in KAGRA



**surface NN** and **bulk NN** in KAGRA site based on Somiya+ (2012)

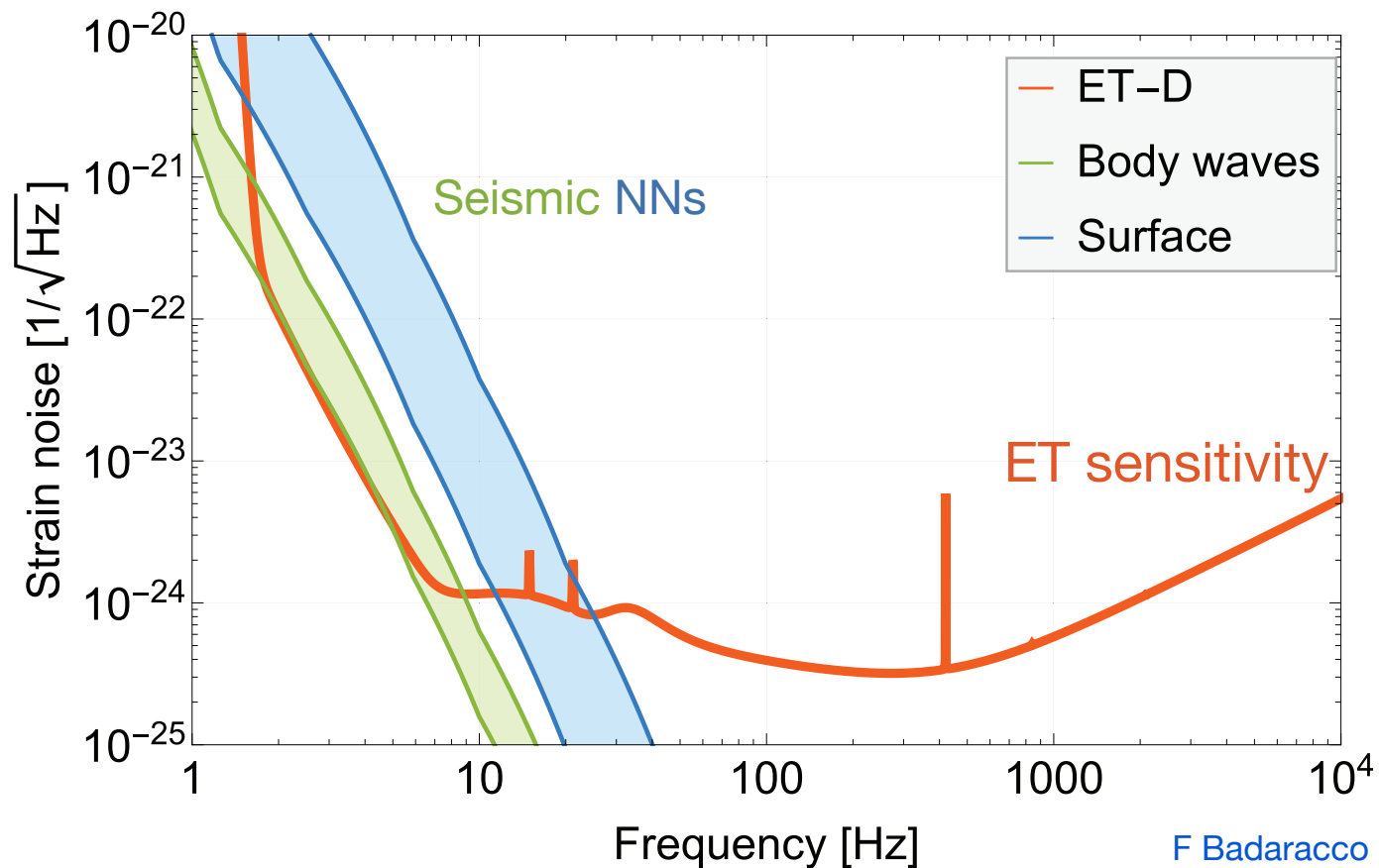
Estimated to be enough small for seismic

Other source could affect sensitivity

Mirror thermal

# NN in 3G Detectors

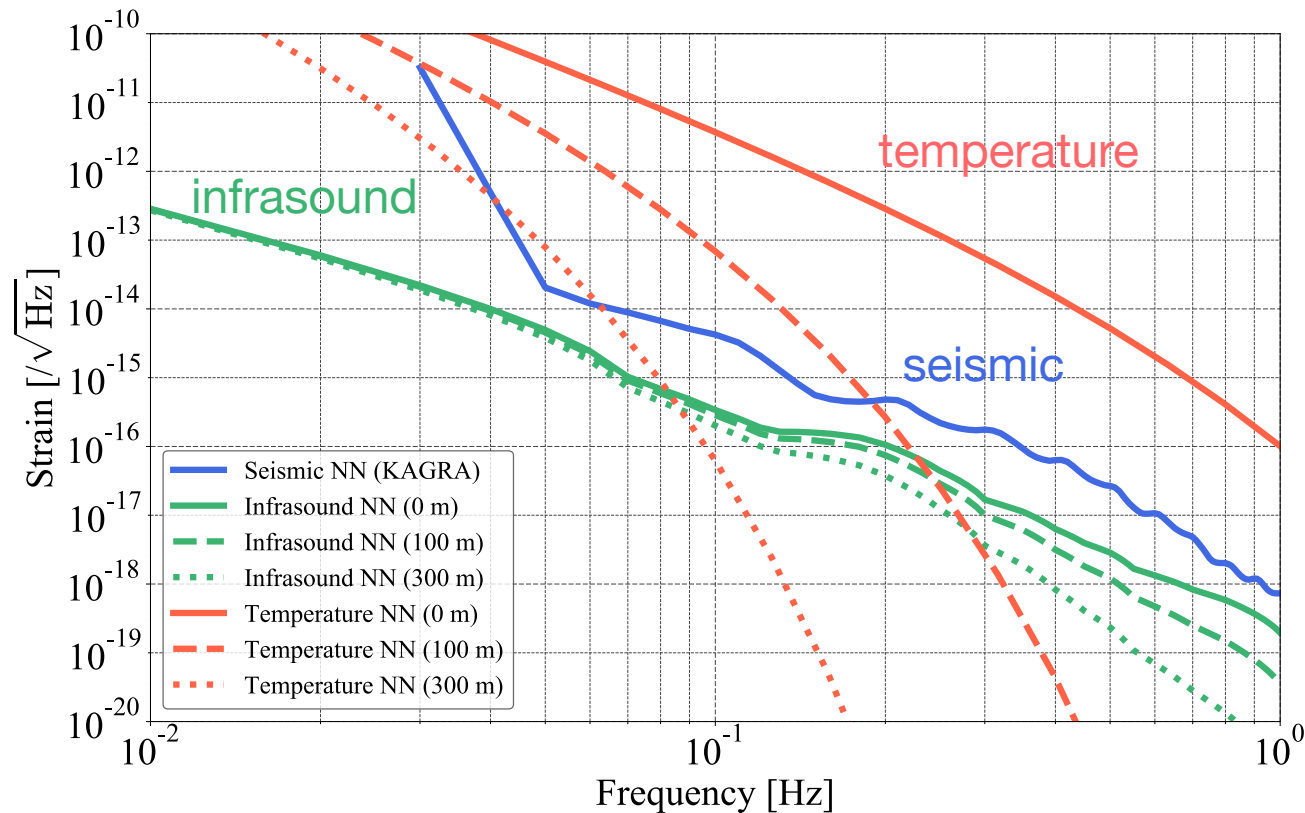
- For 3G detectors NN could be a dominant noise source in low frequencies



F Badaracco and J Harms 2019

# Strategy

- Basically NN cannot be distinguished from GW signal
- Coupling path is simple, but modeling is complicated



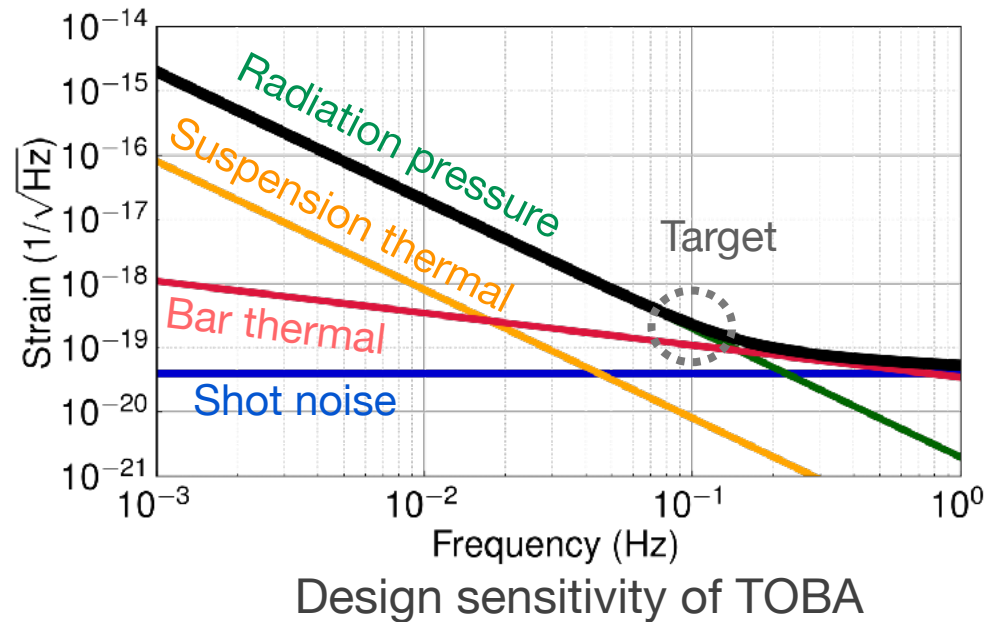
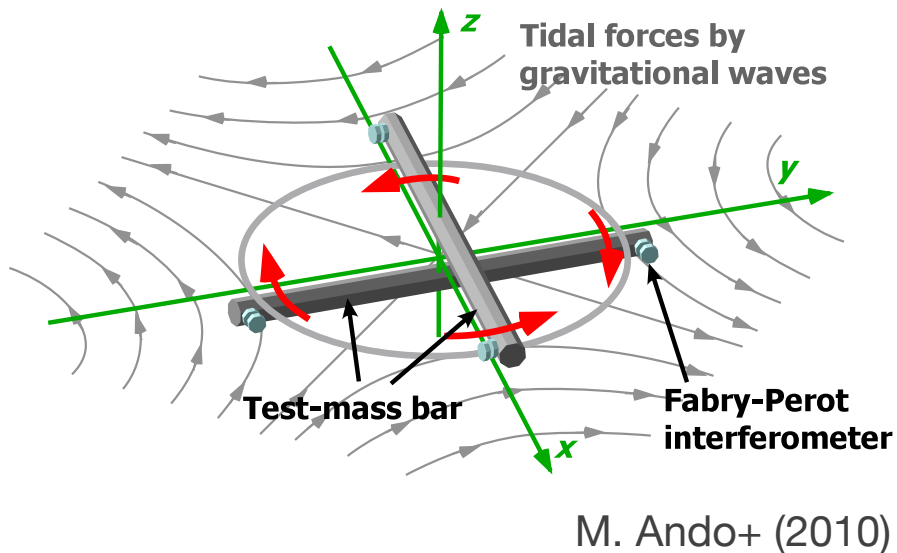
credit: T.Shimoda

- ▶ Model test by direct measurement

# Torsion Bar Antenna (TOBA)

TOBA : TORSion-Bar Antenna

- Gravitational wave detector using two torsion pendulums
- GW detector = Gravity Gradiometer
- Resonant frequency of torsion pendulum  $\sim$  mHz
  - Sensitive to **low frequency** ( $\sim 0.1$ Hz)
- Target sensitivity  $h \sim 10^{-19} / \sqrt{\text{Hz}}$  @ 0.1 Hz with **10 m** bars



# Development Plan

Phase-I  
(2009)

Phase-II  
(2015)

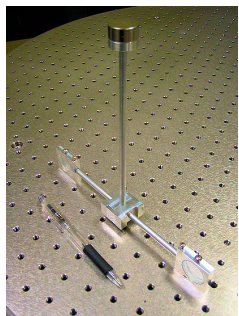
Phase-III  
(Now)

Final  
(Target)

## Principle Test

$10^{-8}/\sqrt{\text{Hz}} @ 0.1 \text{ Hz}$   
(Established)

- Room Temp.
- 25cm TM(s)

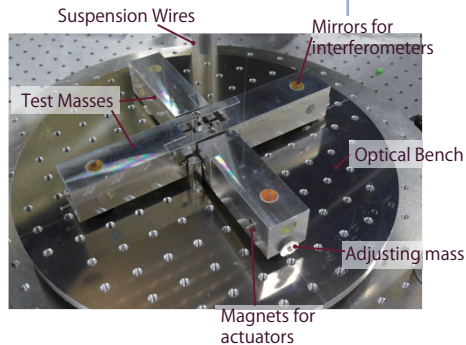


K. Ishidoshiro  
Ph.D Thesis

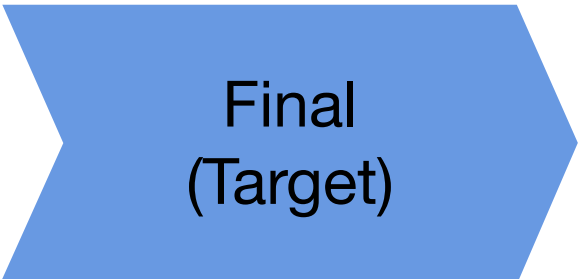
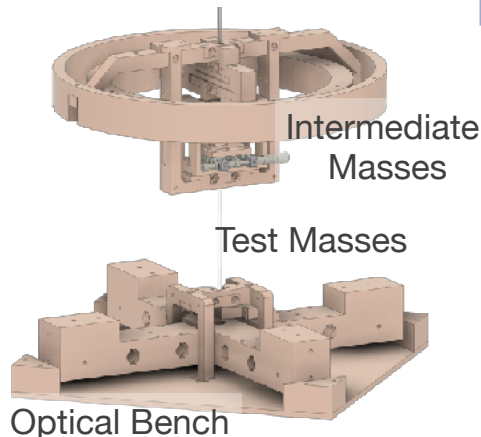
## Cryogenic Test

$10^{-15}/\sqrt{\text{Hz}} @ 0.1 \text{ Hz}$   
(Design)

- Cryo. Temp. (4K)
- 35cm TMs



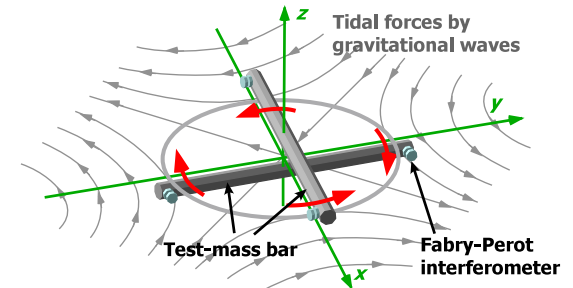
A. Shoda  
Ph.D Thesis



## Goal

$10^{-19}/\sqrt{\text{Hz}} @ 0.1 \text{ Hz}$   
(Target)

- Cryo. Temp. (4K)
- 10m TMs



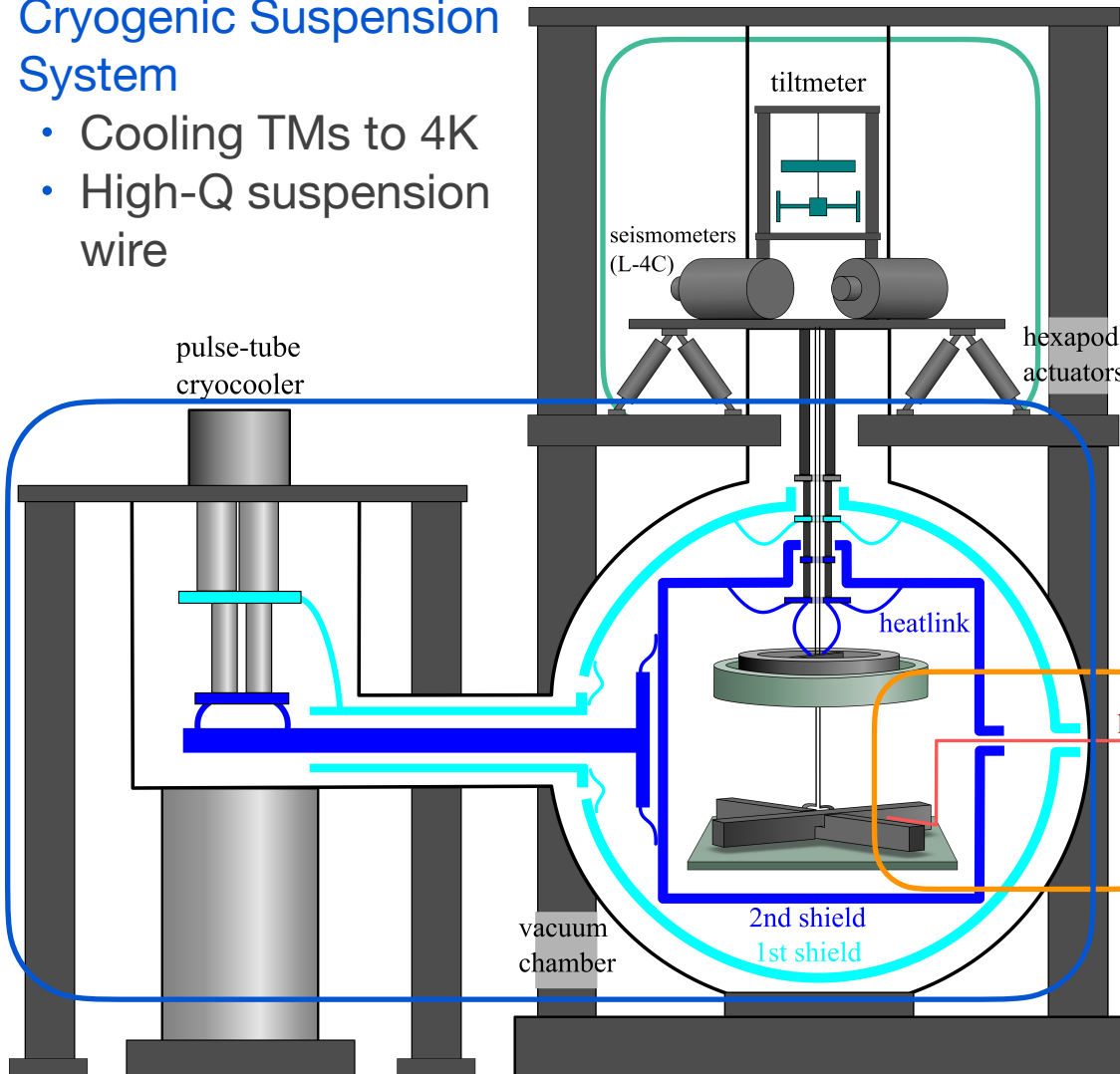


# Setup of Phase-III TOBA

## Cryogenic Suspension System

- Cooling TMs to 4K
- High-Q suspension wire

pulse-tube cryocooler



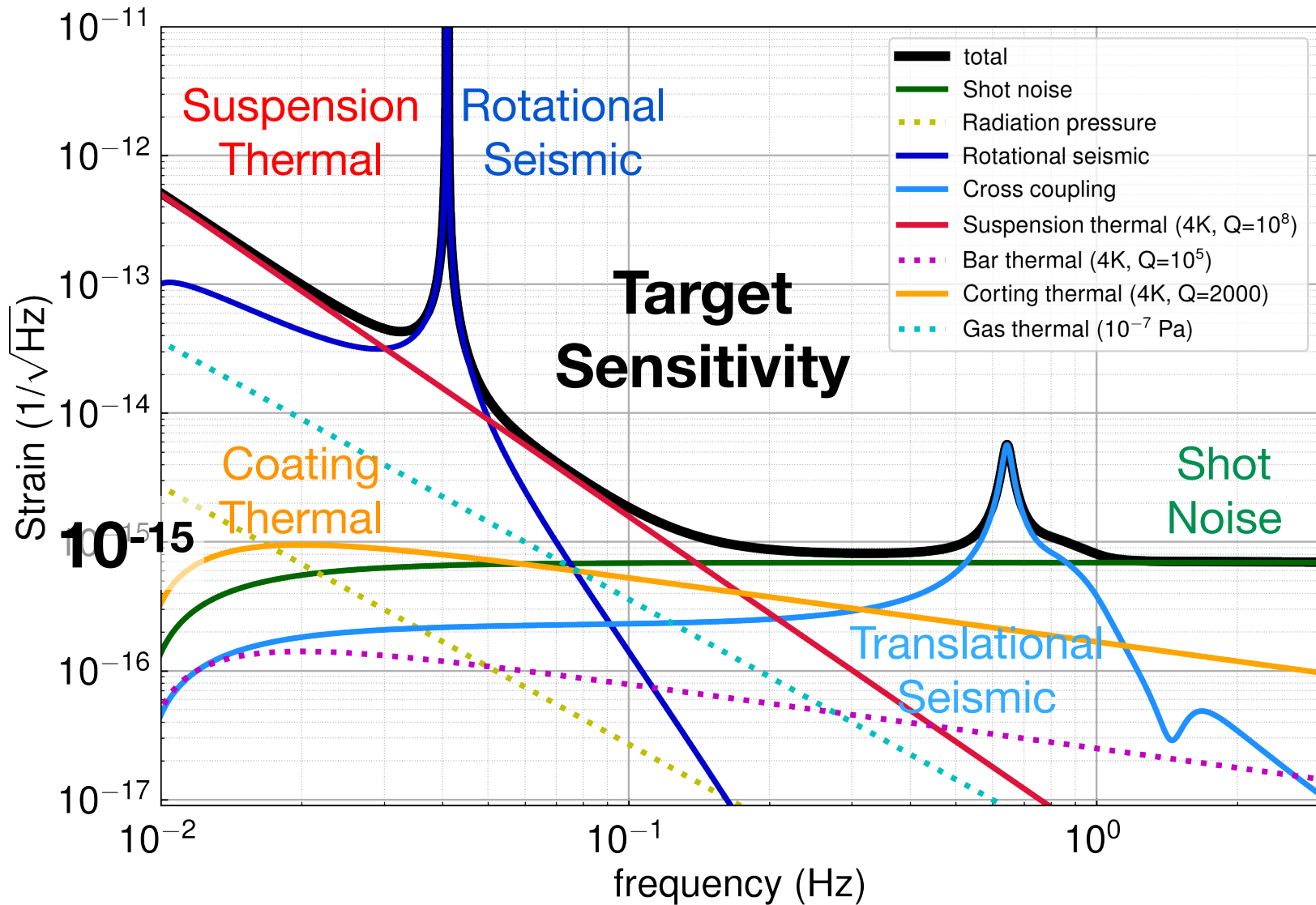
## Active Vibration Isolation System

- Reduction of vibration at the suspension point
- Reduction of vibration induced cryocooler

## Optical System

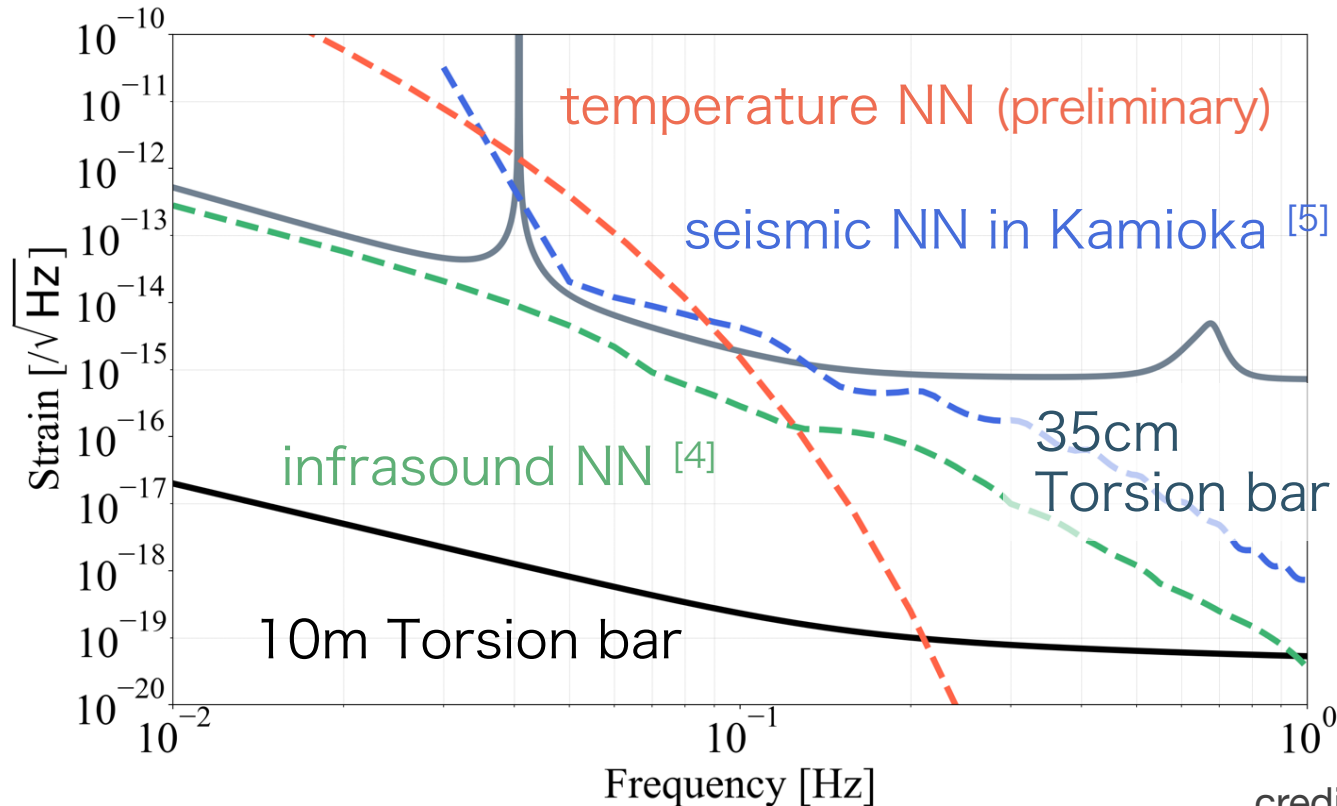
- Rotation measurement by high-sensitive wave front sensor
- Monolithic interferometer for reducing readout noise

# Design Sensitivity



# Direct Measurement of NN with TOBA

- TOBA sensitivity vs NN estimation



- Phase-III TOBA can measure NN directly below 0.1 Hz
- Higher S/N for Final TOBA

# Development Items

- Cryogenic Suspension System
  - Cooling System → Cooled down to **6.1 K**
  - High-Q suspension fiber
- Optical System
  - New angular sensor with higher sensitivity
  - Monolithic interferometer under cryogenic temp.
- Active Vibration Isolation
  - Reduction of translational seismic noise
    - Reduced by **1/1000** at most
  - Reduction of vibration induced by cooler

# Cryogenic Suspension System

## Cryogenic Cooler

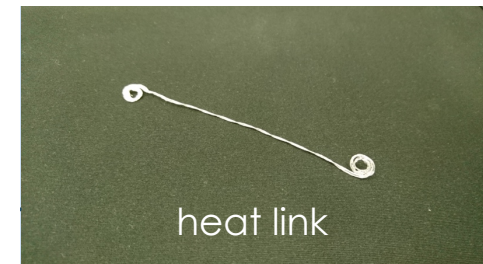
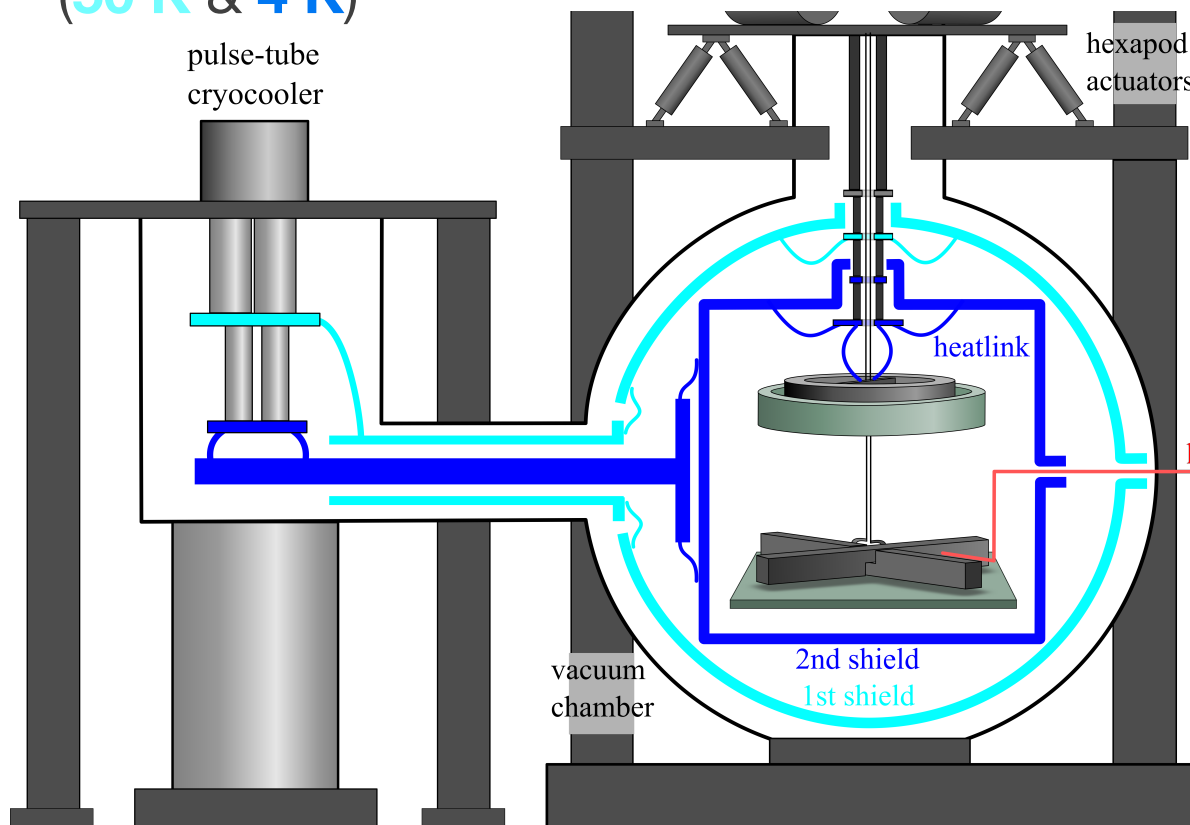
- Cool down TMs to 4 K
- Two radiation shields (50 K & 4 K)

## Suspension wire

- Si wire
- High Q value ( $>10^8$ )

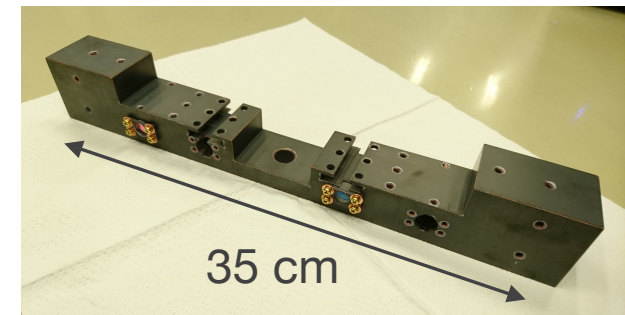
## Heat Links

- High-purity aluminum
  - ▶ Conductive cooling



## TMs

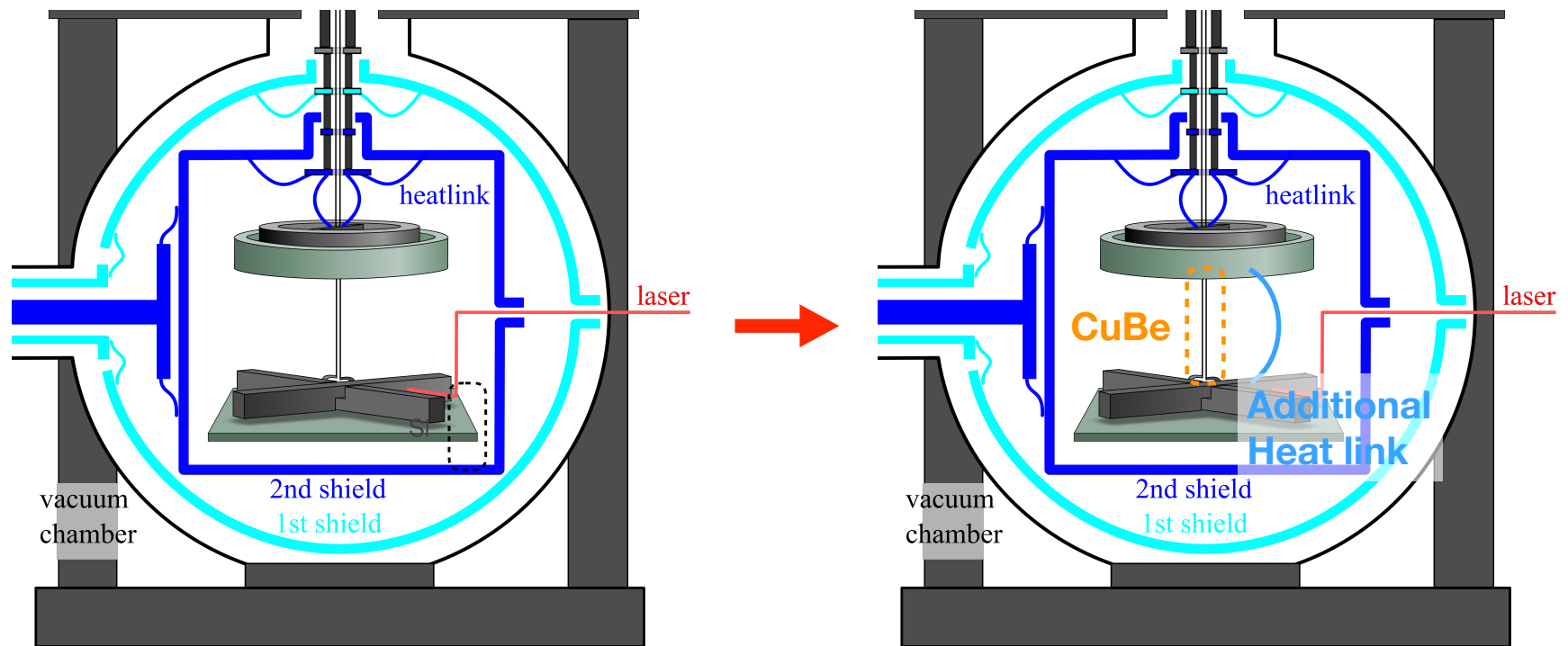
- Copper
- Surface is oxidized



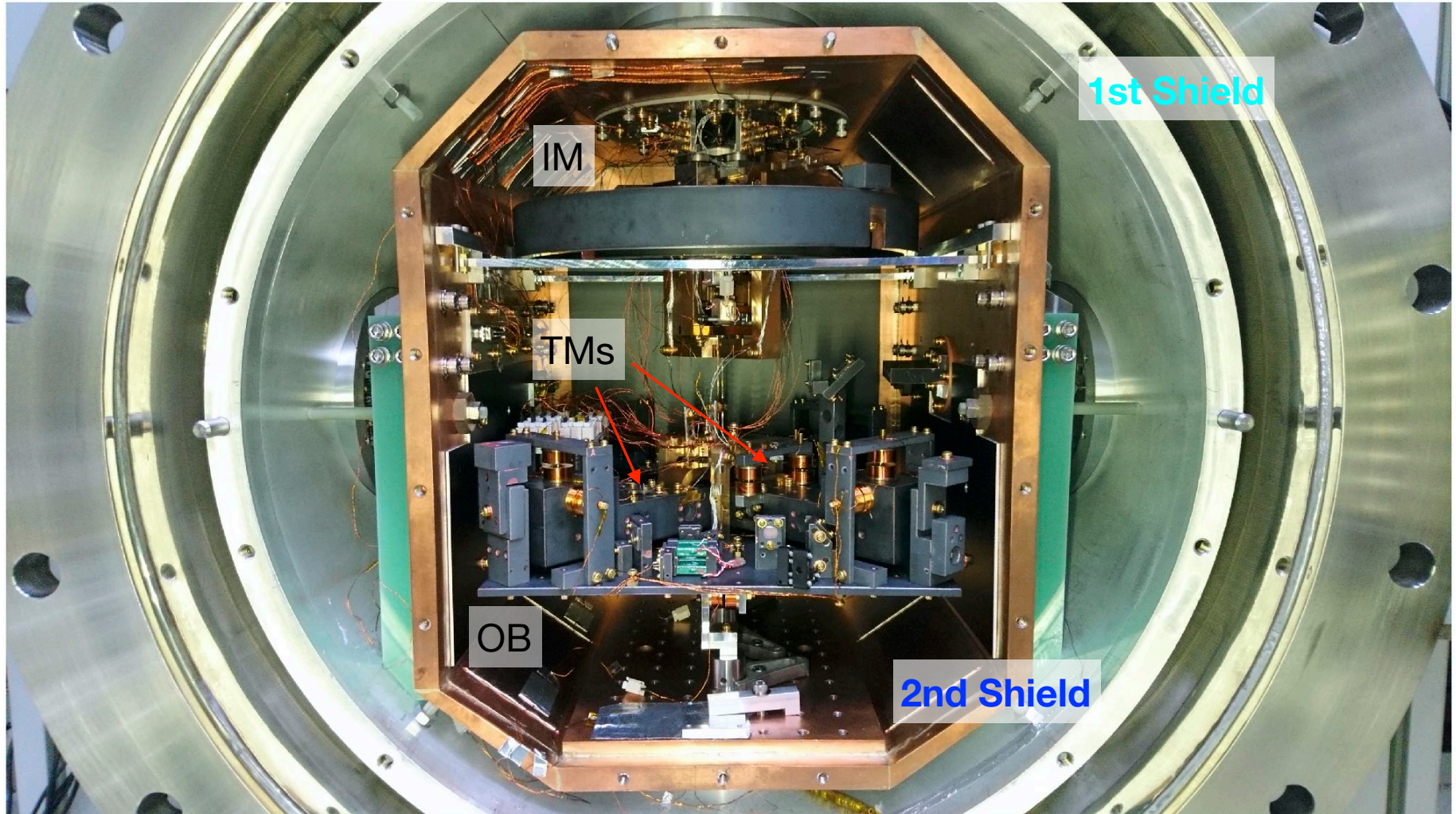
# Current Suspension System

Test for cryogenic, simplified configuration

- Silicon fiber → CuBe wire
- Heatlinks between IM and TMs
- Readout: only optical levers

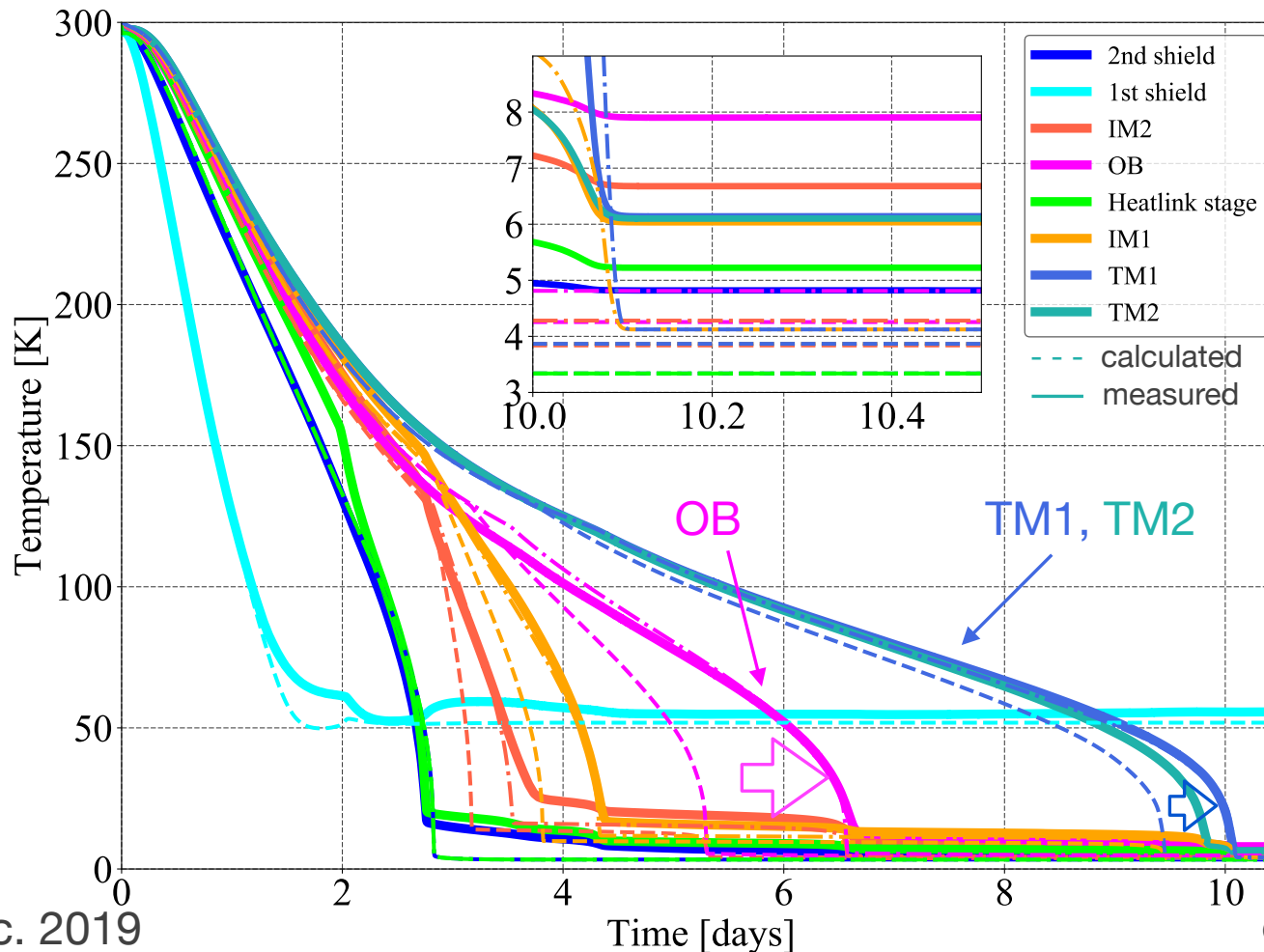


# Current Setup



# Cooling Result

- Cool down to 6.1 K
- Slower cooling speed → Bad heat contact?

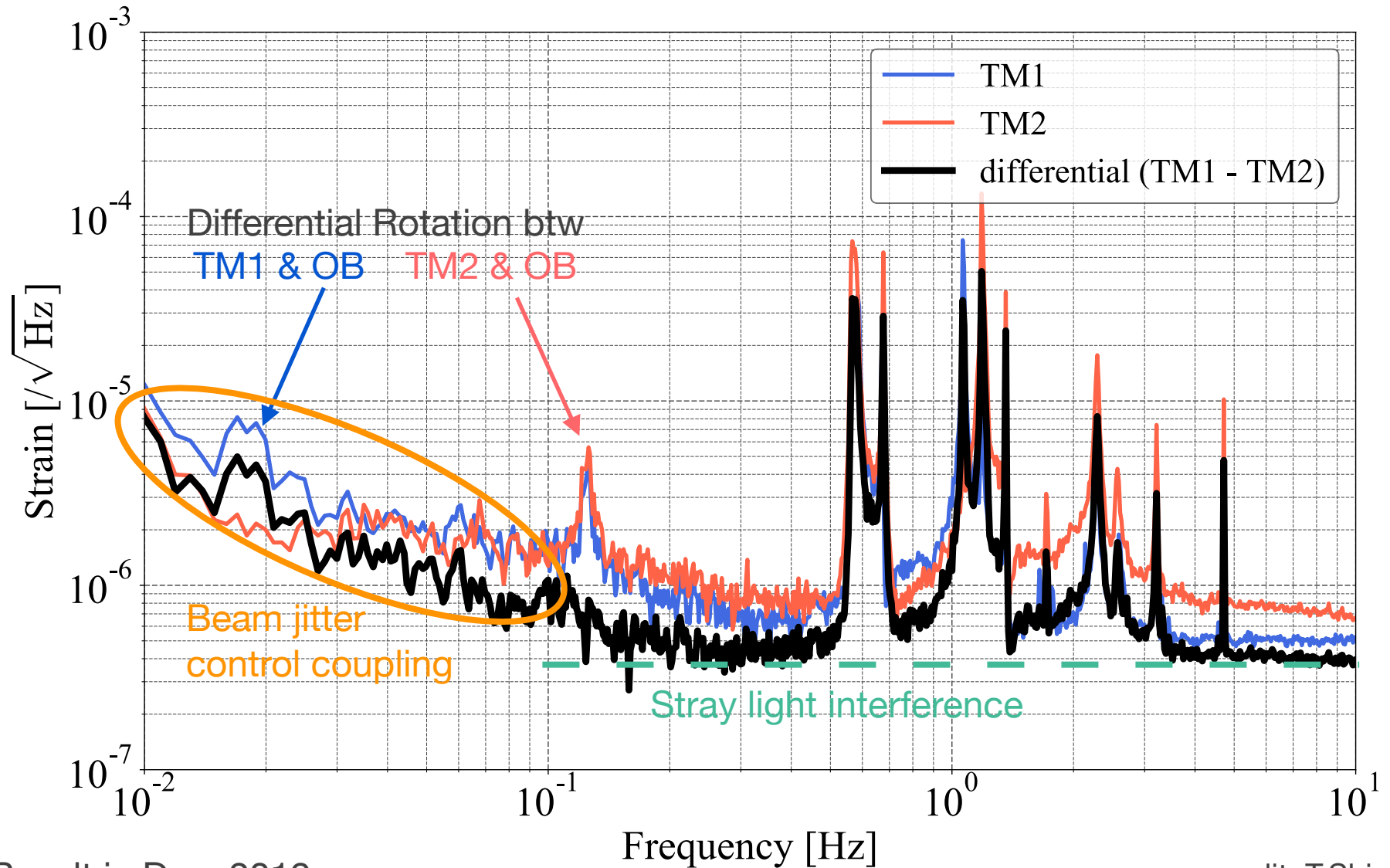


Result in Dec. 2019

credit: T.Shimoda



# Sensitivity of differential motion



Result in Dec. 2019

credit: T.Shimoda

# Active Vibration Isolation System

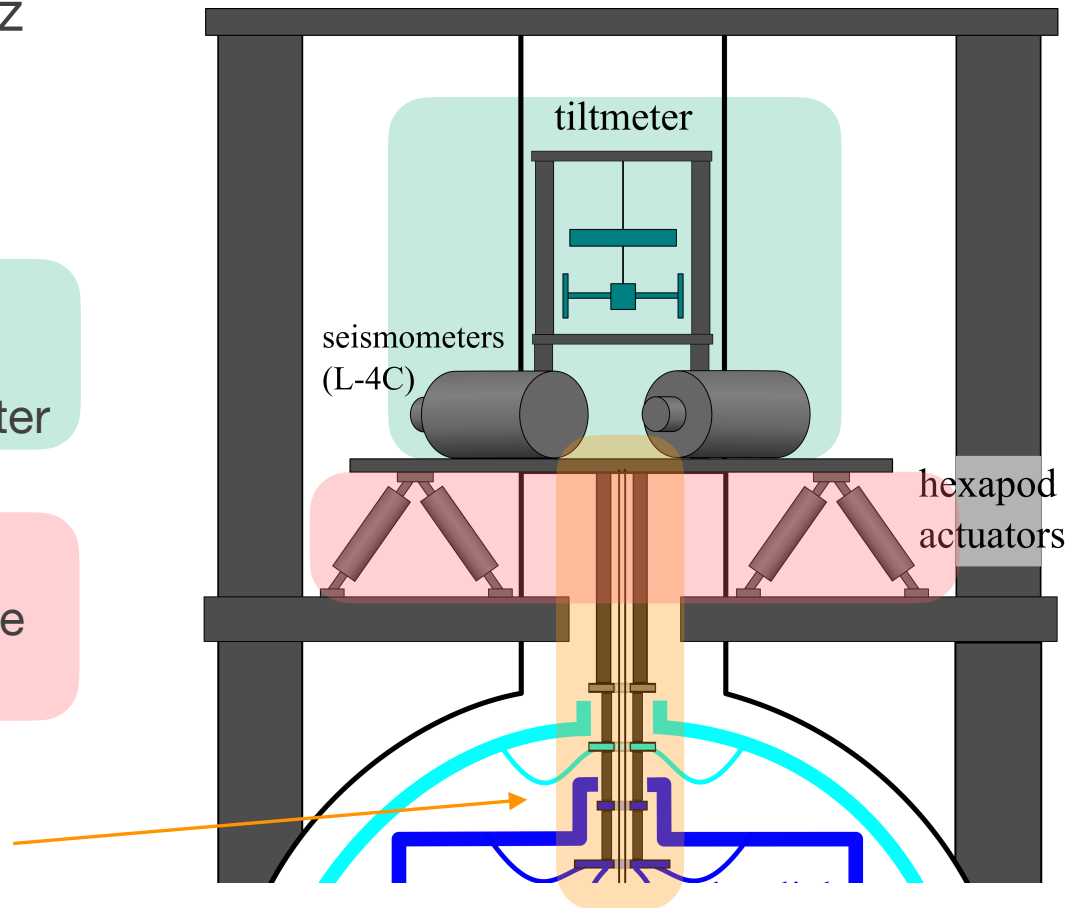
- Reduction of seismic vibration
  - Coupling from horizontal vibration
    - ▶  $10^{-7}$  m/ $\sqrt{\text{Hz}}$  @ 0.1 Hz
  - Nonlinear coupling
    - ▶  $10^{-10}$  m/ $\sqrt{\text{Hz}}$  @ 1 Hz

Measure motion at the suspension point by seismometer & tilt meter



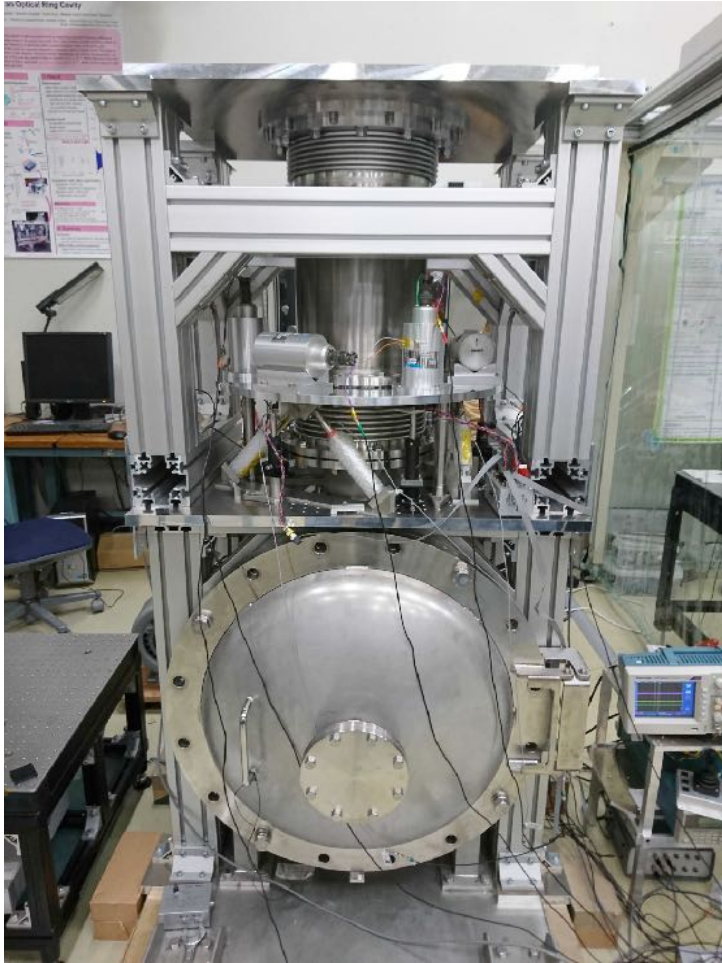
Feedback the signal to actuators to cancel out the motion

- Reduction of vibration induced by cooler



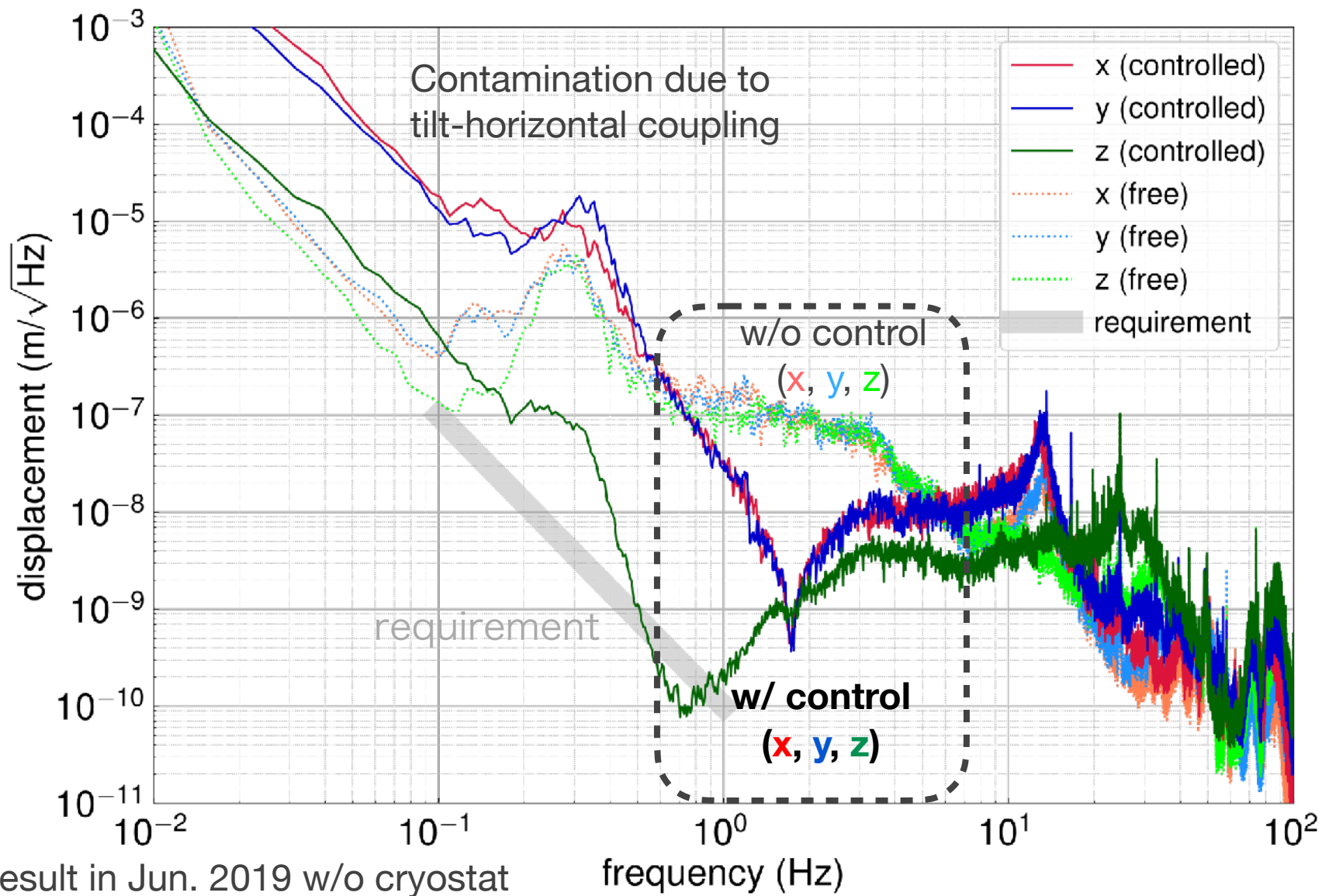
# Active Vibration Isolation System

- Tested w/o the suspension and the cryostat
- Tiltmeter is not install



- Sensor: L4C (inertial) x6, PS (local) x6
- Actuator: PZT (range:  $\sim 60\mu\text{m}$ ) x6

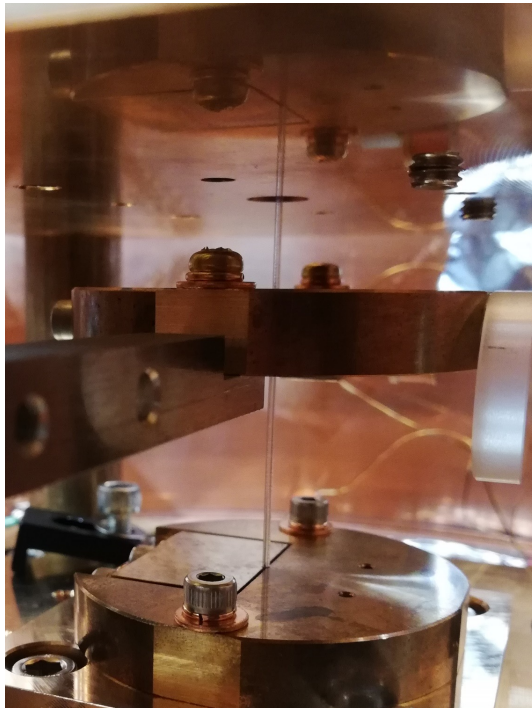
# Performance of AVIS



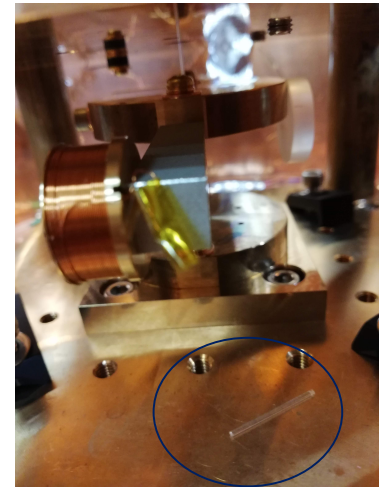
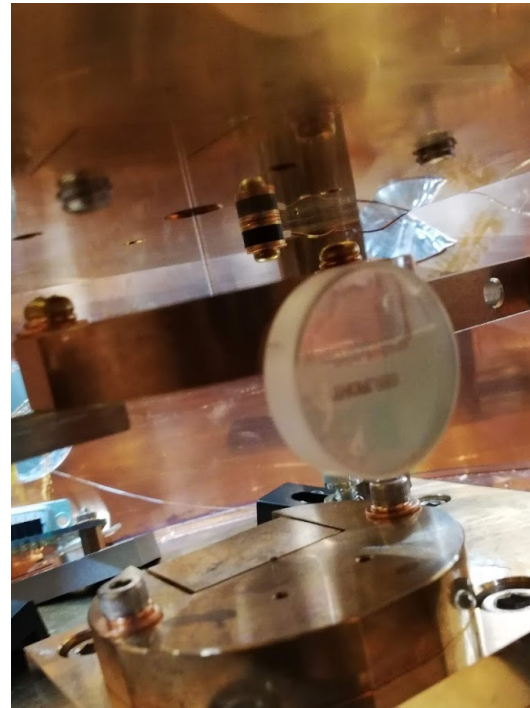
# High-Q Suspension Fiber

- Measurement of torsional Q of Sapphire fiber
- Coefficient of expansion is larger for CuBe than sapphire

Before  
cooling:



After  
cooling:



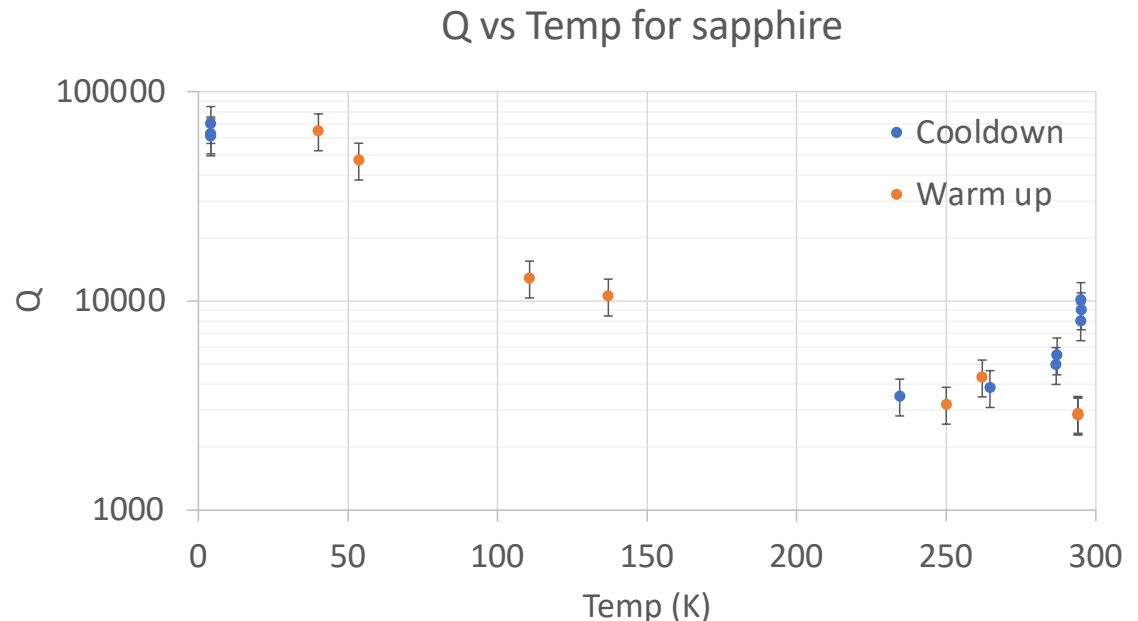
Broken piece

15

credit: C. P. Ooi

# High-Q Suspension Fiber

- Achieved to  $7 \times 10^4$  at 4 K
- Currently seemed to be limited by loss at the clamp
- Q ranged from 3 000 to **70 000 at 4 K**
- Single clamp mode
  - Due to breakage
- Adjustments have been made to shift the pendulum frequency from the torsion frequency
  - Cannot be ruled out as source of interference

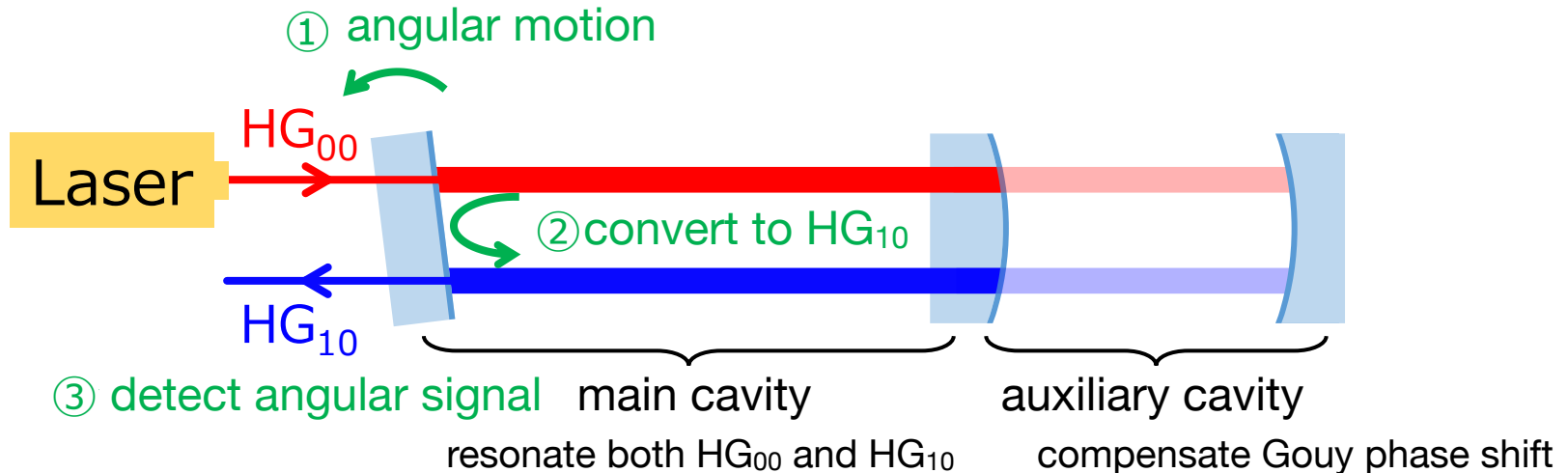


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credit: C. P. Ooi

# High Sensitive Angular Sensor

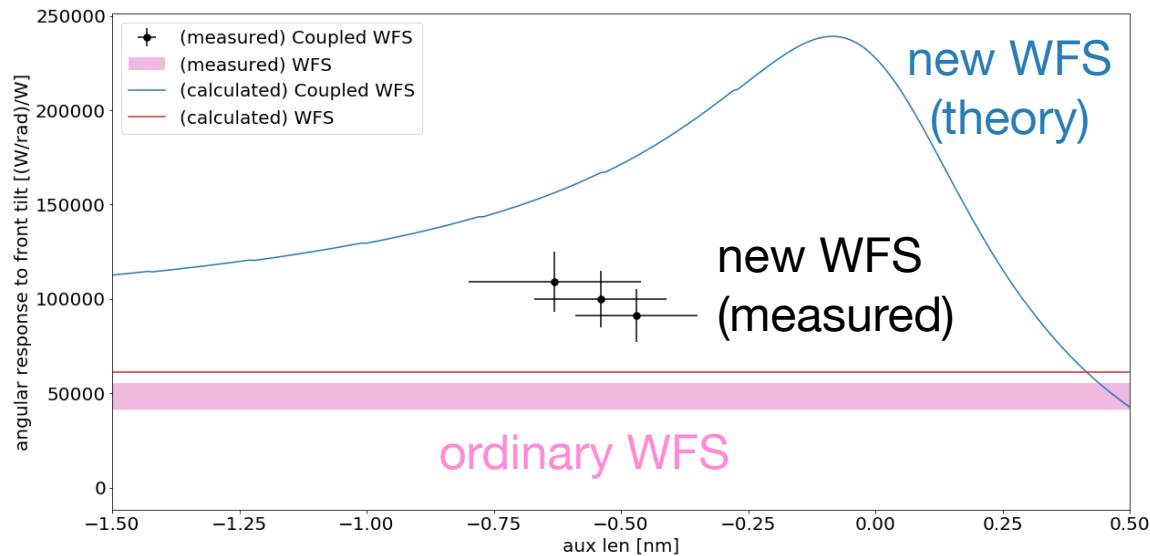
- An improved wave front sensor



- Enhance angular signal by resonating both  $HG_{00}$  and  $HG_{10}$ 
  - ▶ Ordinary it's impossible due to Gouy phase shift
  - ▶ Compensate it by an auxiliary cavity

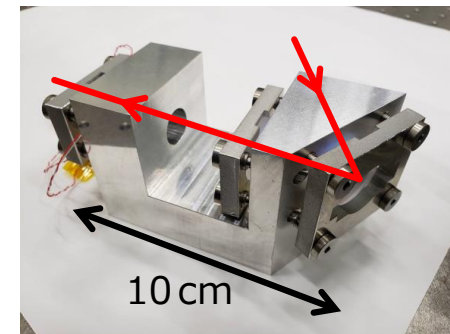
# High Sensitive Angular Sensor

- Demonstration was done
  - ▶ Still need further improvement



credit: Y. Miyazaki

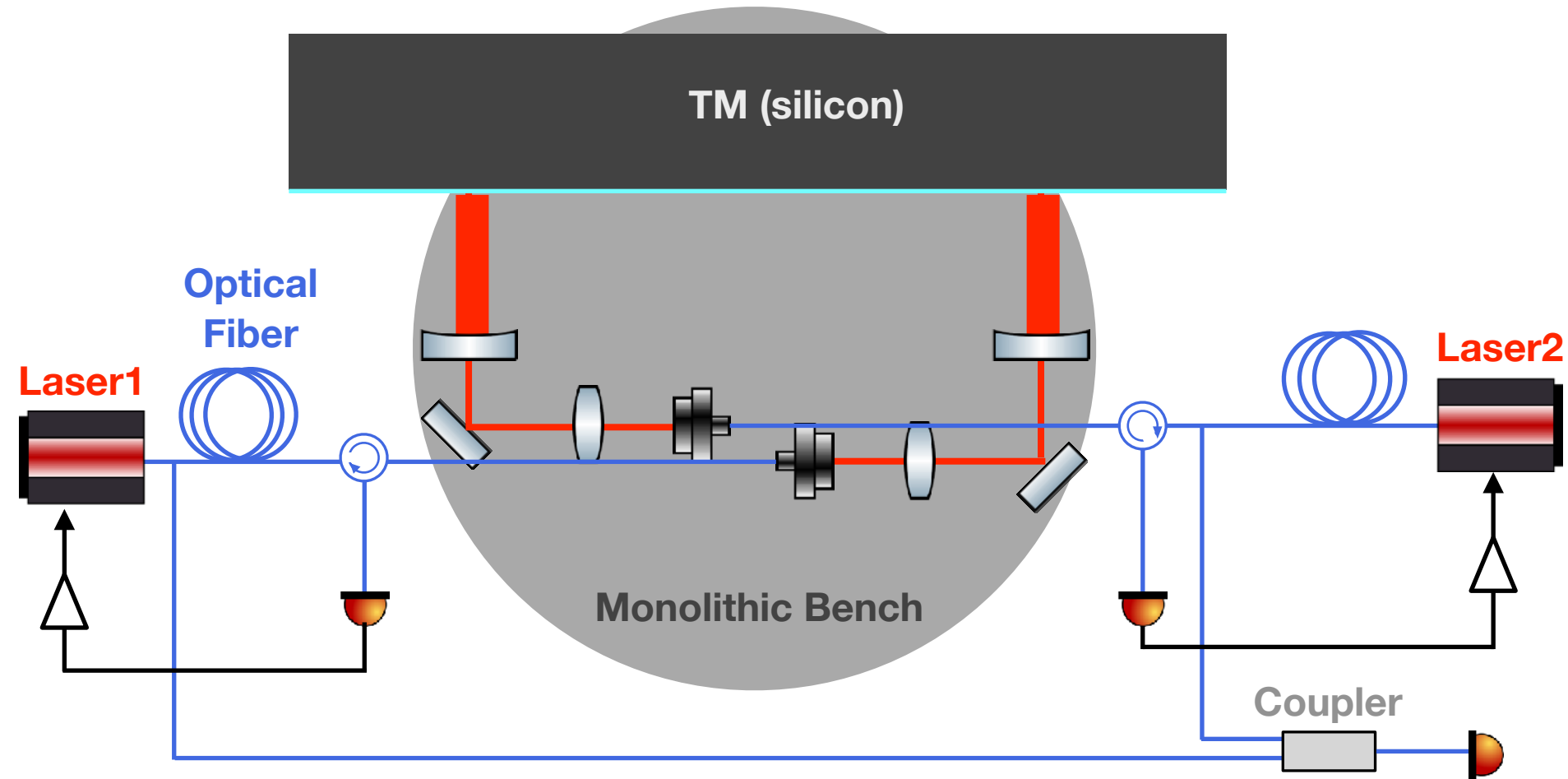
- A new prototype is under development



credit: Y. Oshima



# Monolithic Interferometer



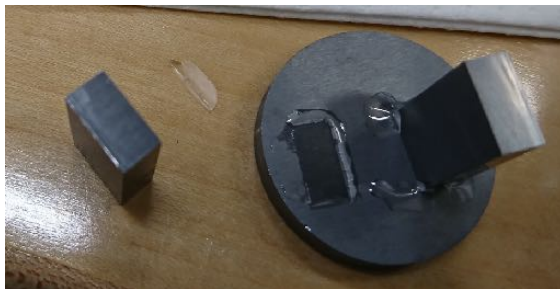
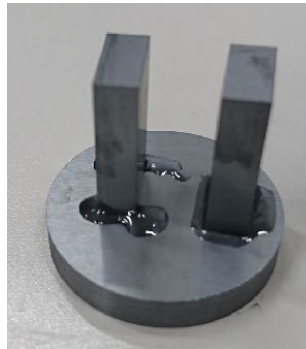
- Read displacement of each arm cavity independently (2 laser)
- Feedback to each laser's frequency
- Measure beat frequency to read differential motion

**Beat  
Signal**

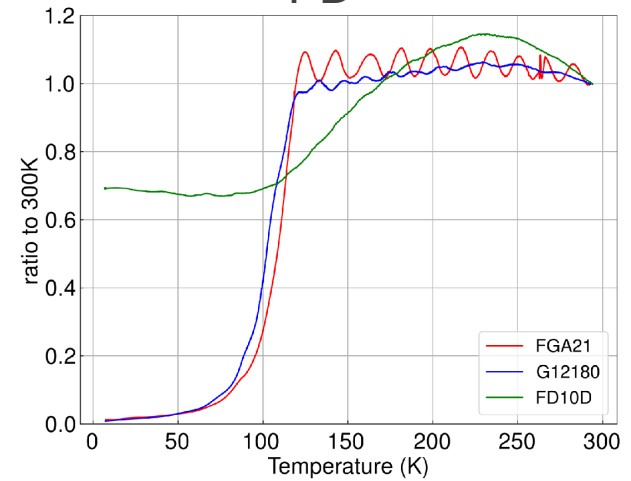
# Monolithic Interferometer

- Component selection is on going

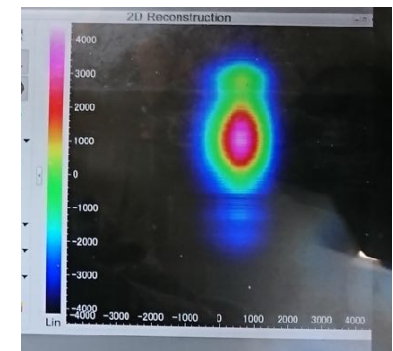
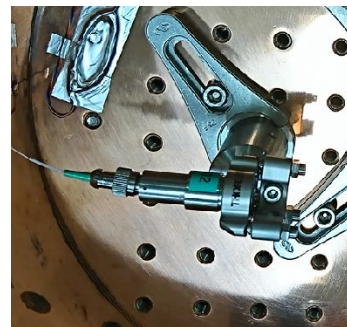
Bonding



PD

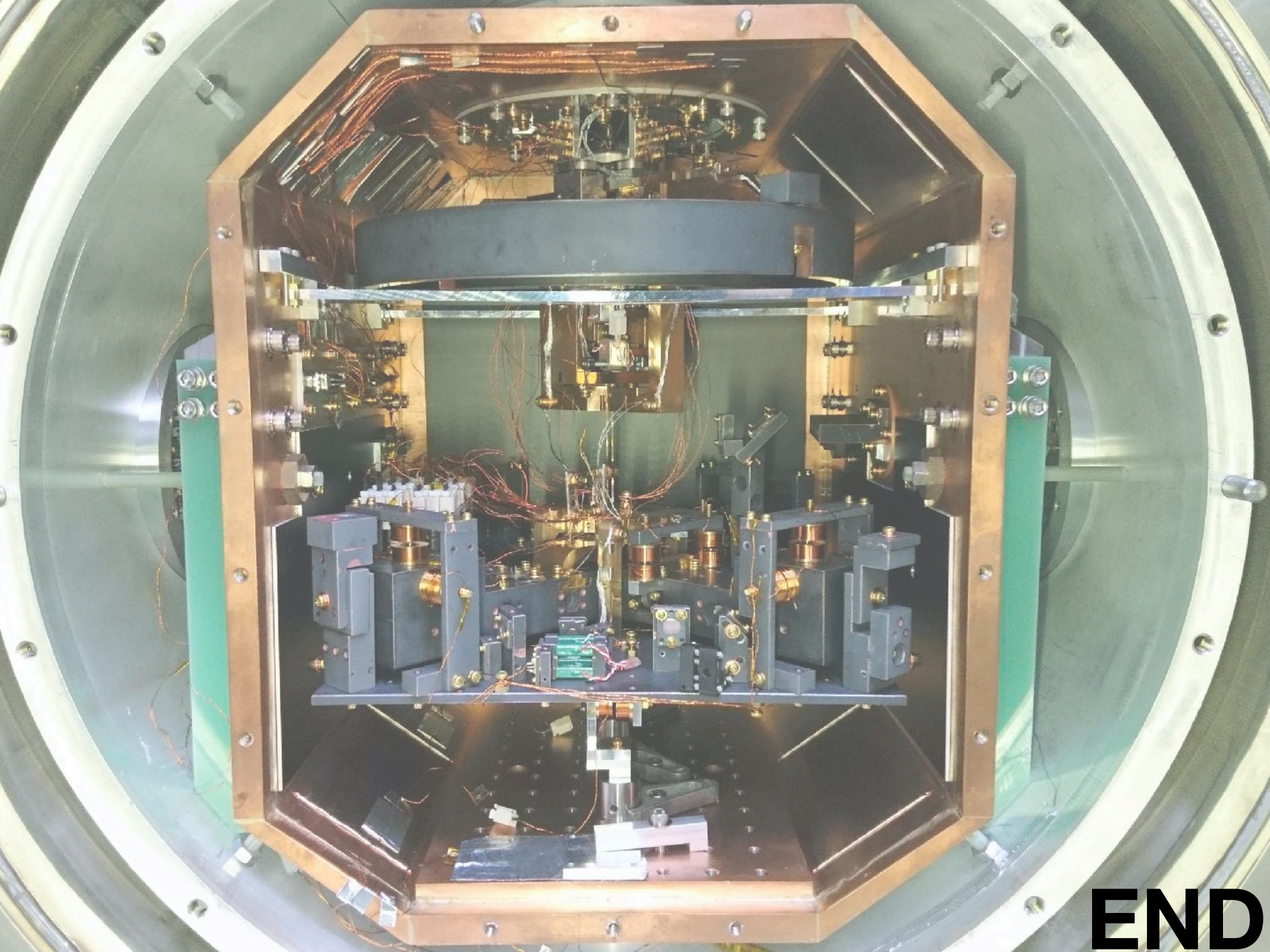


Collimator



# Summary

- Direct measurement of Newtonian Noise with TOBA
  - ◉ S/N >  $10^3$  in  $f < 0.1$  Hz
  - ◉ Put upper limit  $10^{-21}$  @ 10 Hz on NN of KAGRA
- Current achievement
  - ◉ Cryogenic → basically demonstrated
    - ▶ Need some improvements (cooling speed, achieved temp.)
  - ◉ Active isolation vibration → 3 DoF controlled
    - ▶ Decouple tilt motion from horizontal translation
- On-going issues
  - ◉ Development of high-Q silicon fiber
  - ◉ Demonstration of coupled WFS
  - ◉ Cryogenic monolithic interferometer



**END**

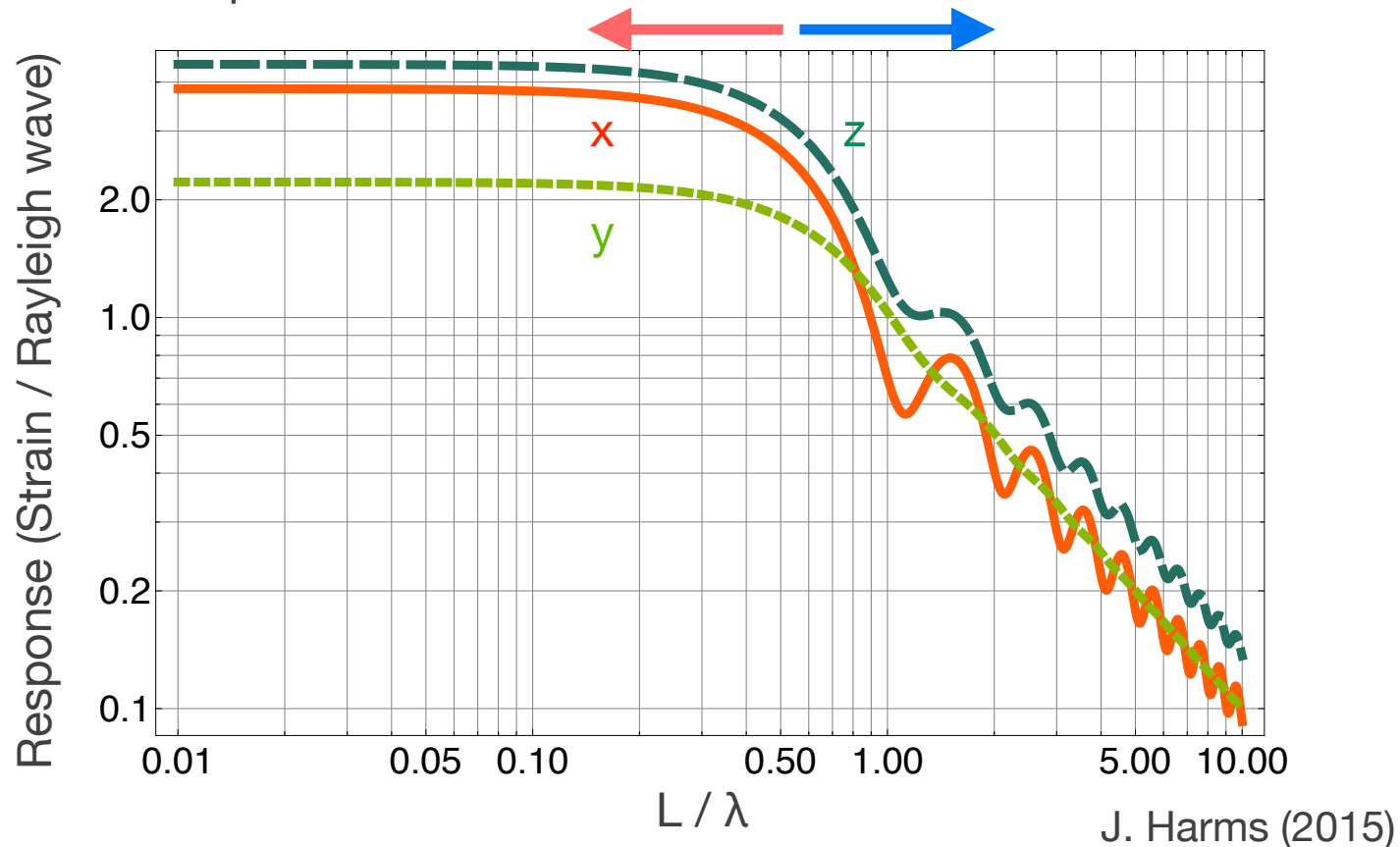


# Seismic NN in Different Scale

- Response from Rayleigh waves to NN (arm: x direction)

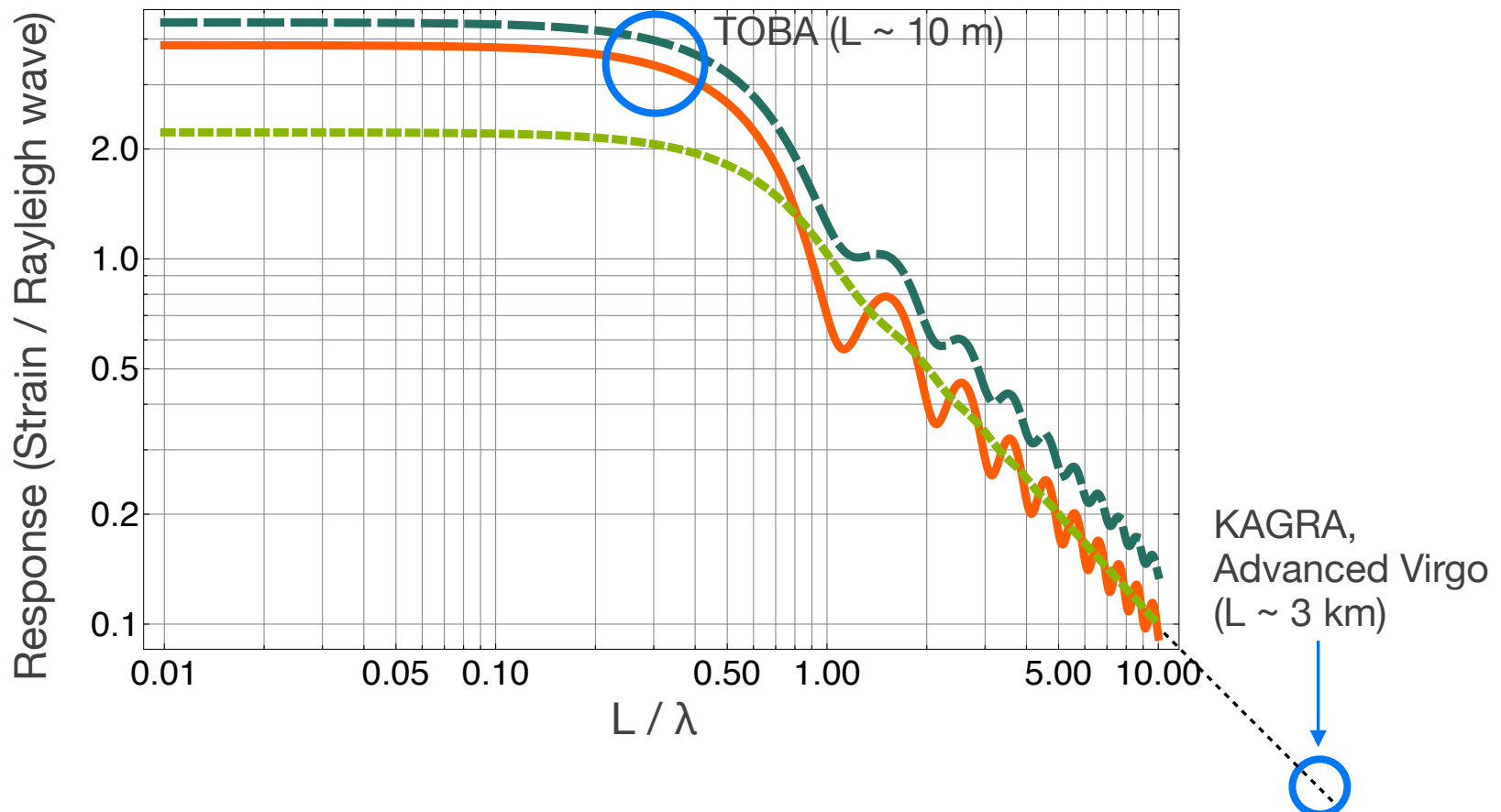
NN is coherent in detector scale

- ▶ independent in scale



# Seismic NN in Different Scale

- Rayleigh wave length:  $\lambda \sim 30 \text{ m @ } 10 \text{ Hz}$  ( $v \sim 300 \text{ m/s}$ )
- TOBA:  $L \sim 10 \text{ m}$   $\longleftrightarrow$  KAGRA, Advanced Virgo:  $L \sim 3 \text{ km}$   
▶ **more sensitive** ET:  $L \sim 10 \text{ km}$

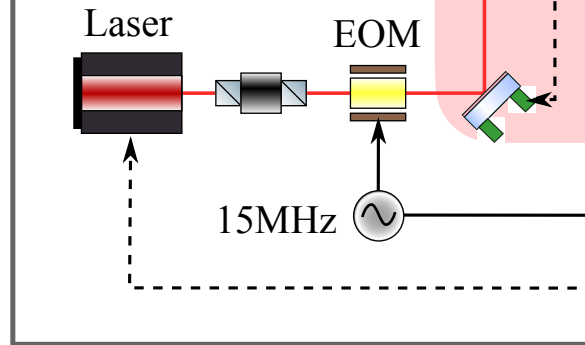


# Optical System

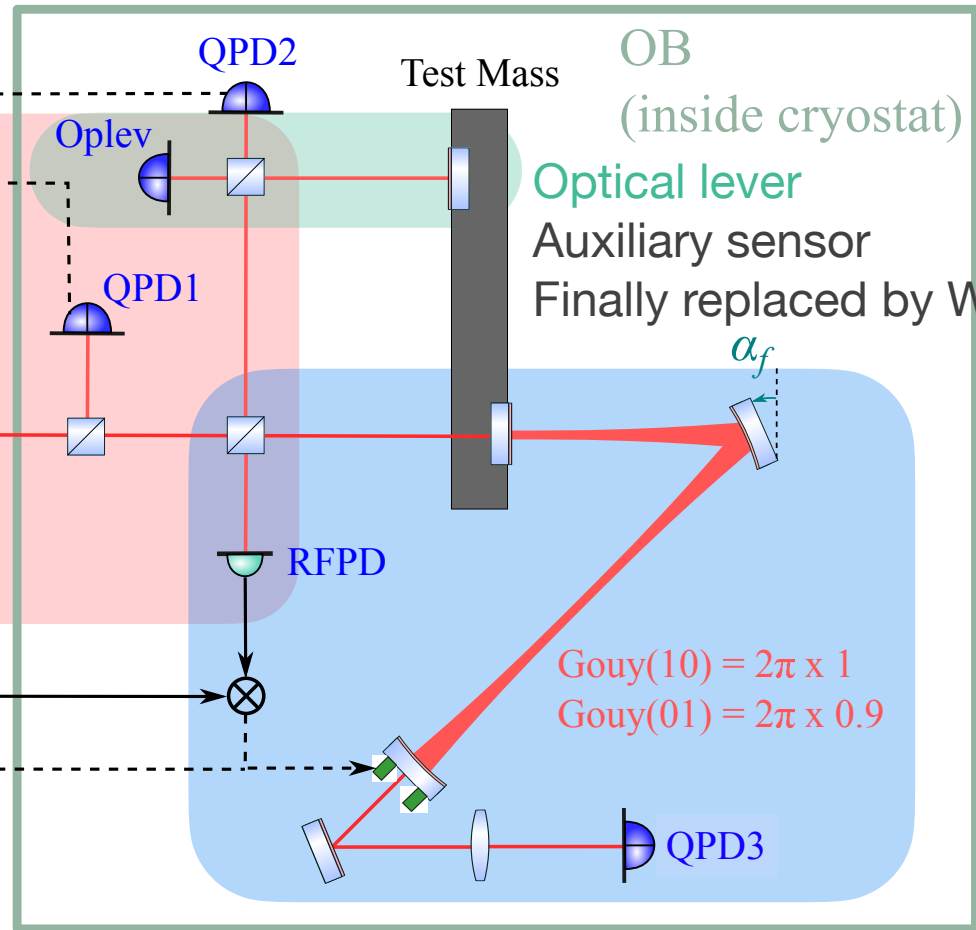
## Beam jitter control

Control incident beam to follow pendulums

Optical table  
(outside chamber)



mix  
& filter



Optical lever

Auxiliary sensor

Finally replaced by WFS

$$\begin{aligned} \text{Gouy}(10) &= 2\pi \times 1 \\ \text{Gouy}(01) &= 2\pi \times 0.9 \end{aligned}$$

High sensitive angular sensor

Measure HG10 mode

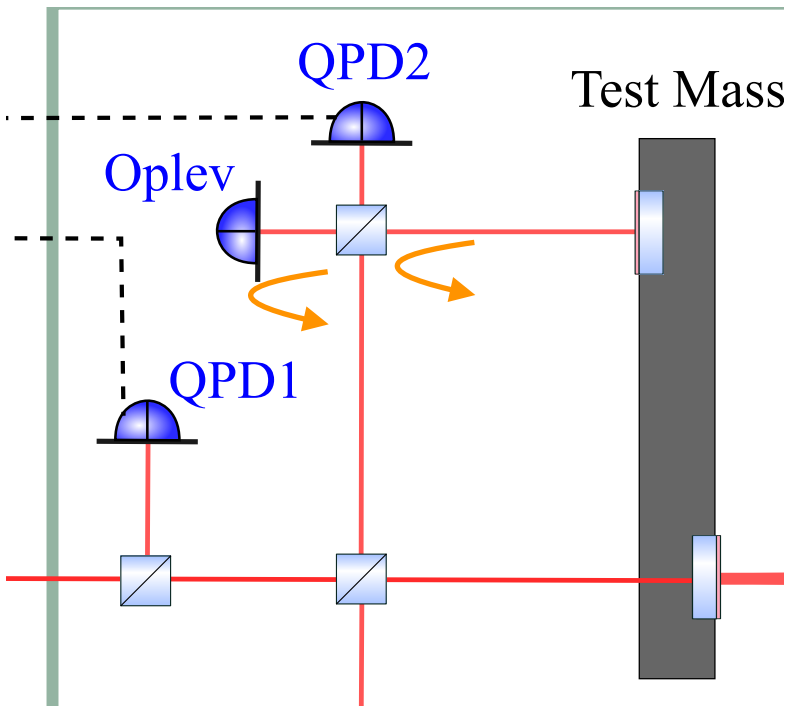
induced by rotational motion



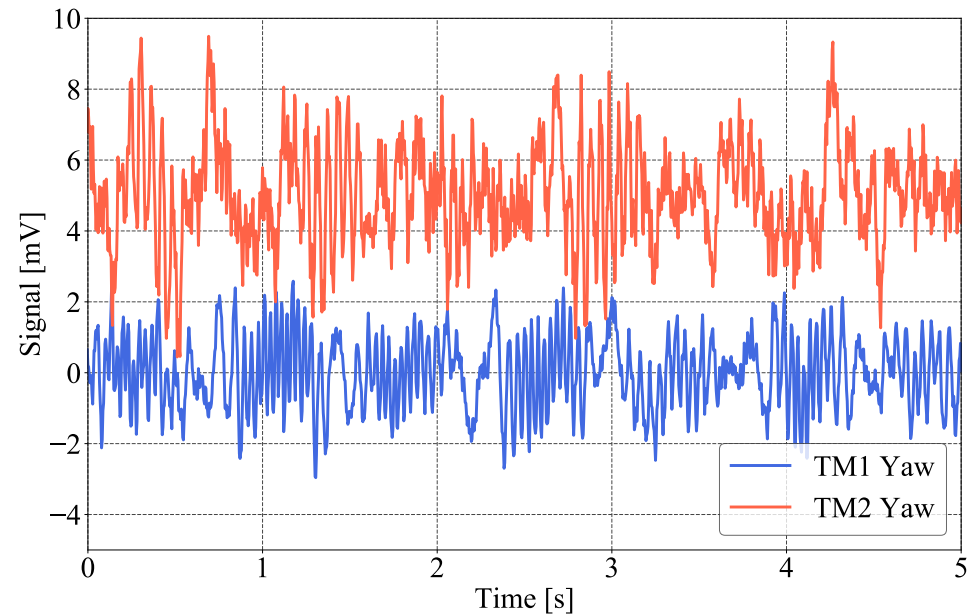
# Stray Light Problem

Front reflection at

- Cube BS
- QPD surface
- ▶ Stray light

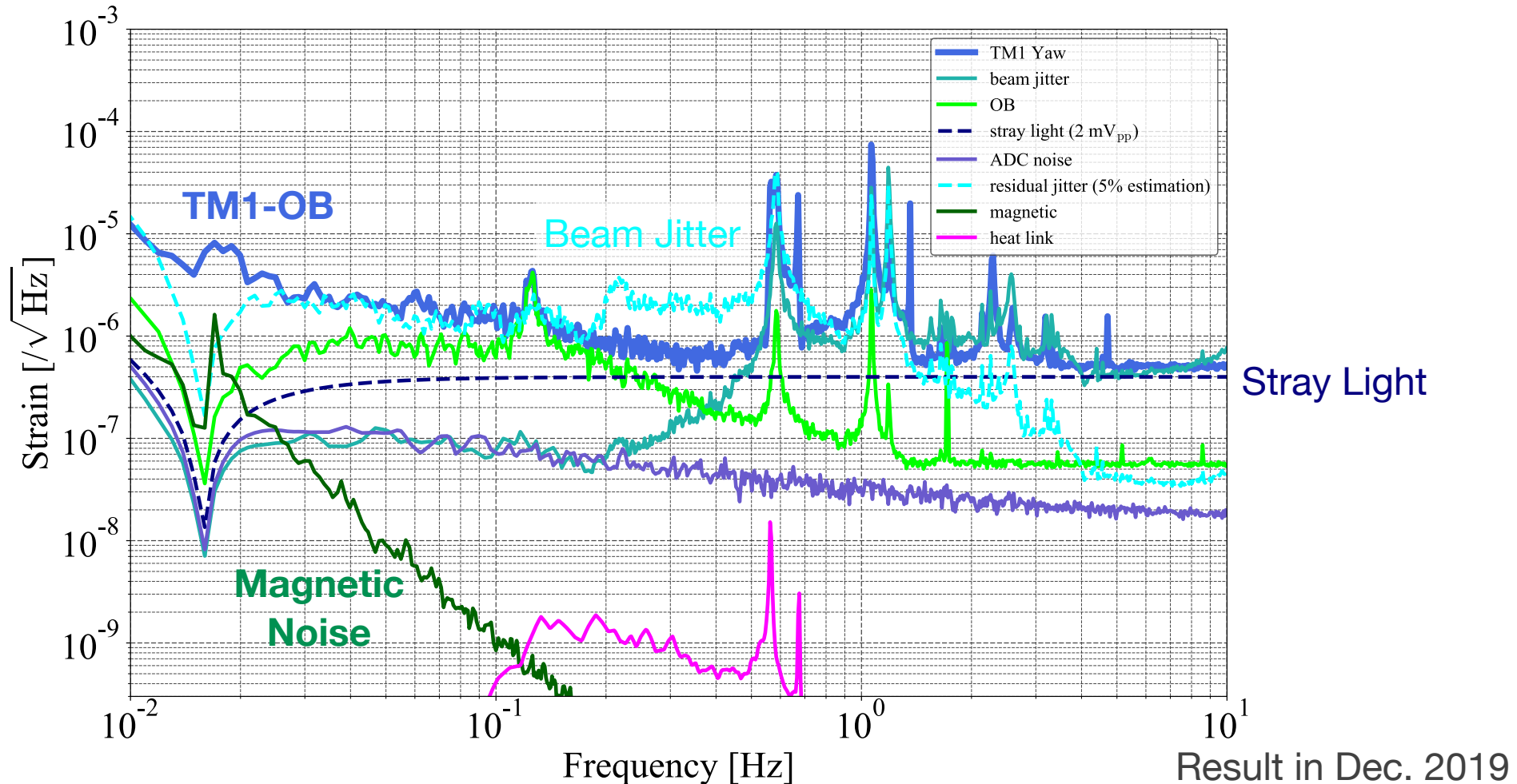


Interference with stray light  
contaminates oplev signal



# Sensitivity of one TM

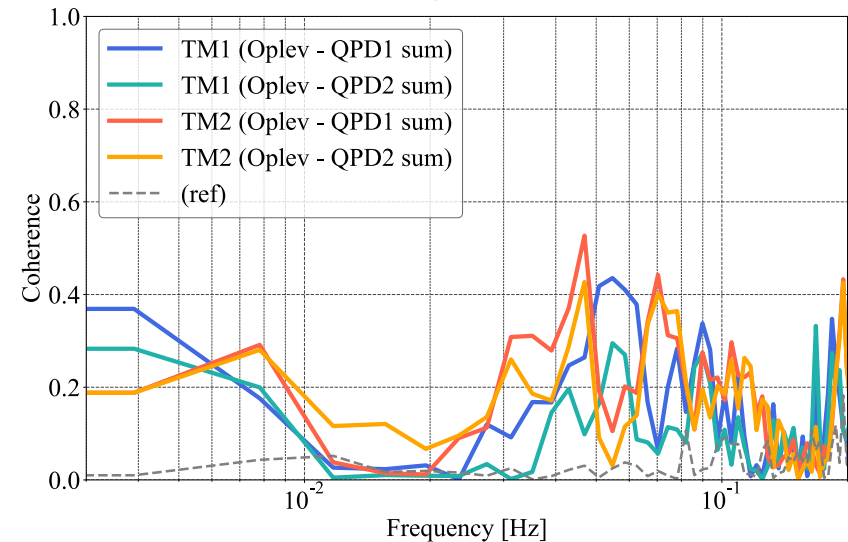
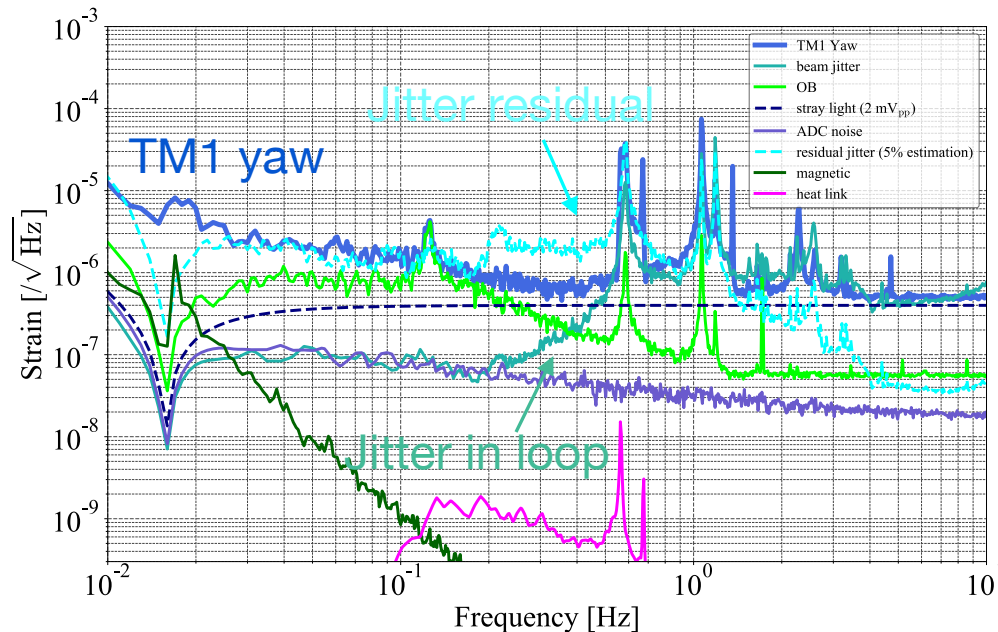
- Limited by **beam jitter**, **interference of stray light**
- Unexpected noise: **magnetic noise** due to eddy current flowing TM



# Beam Jitter Control Noise

- Some coherence btw TM oplev yaw & Jitter QPD sum
  - ▶ Beam jitter control signal shakes beam additionally
  - ▶ Contaminates oplev signal

Coherence btw  
TM oplev yaw & QPD sums

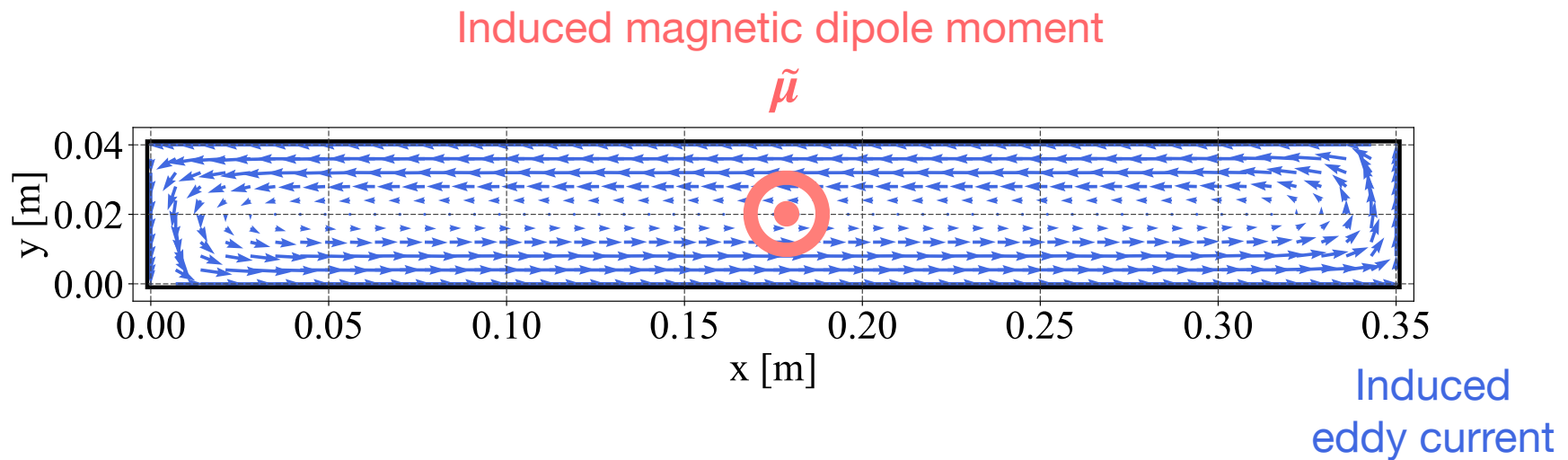


5% residual assumption

- ▶ can be explained the noise budget well

# Magnetic Noise Due to Eddy Current

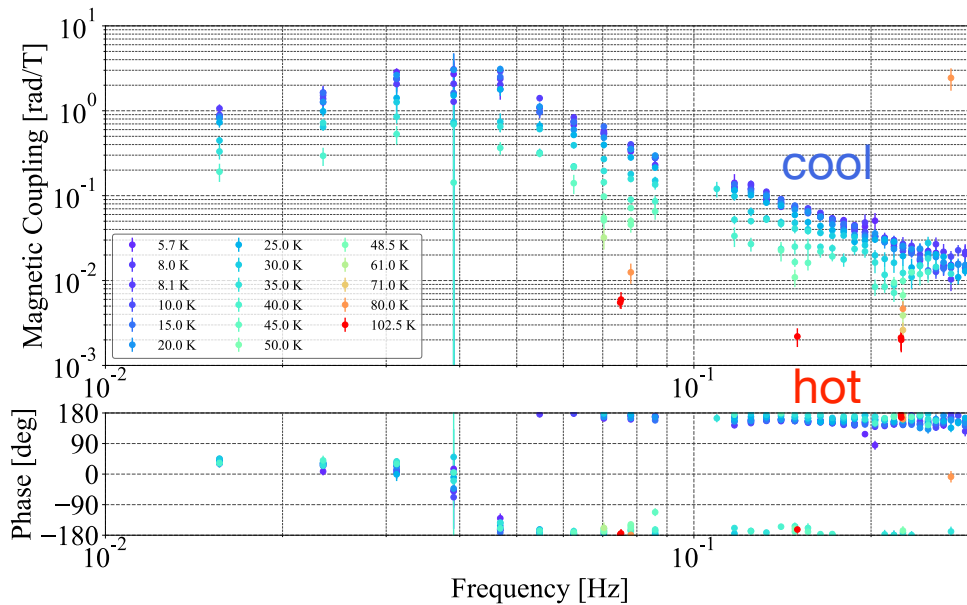
- Ambient magnetic fluctuation induces eddy current
  - ▶ TM has magnetic dipole moment  $\tilde{\mu}$



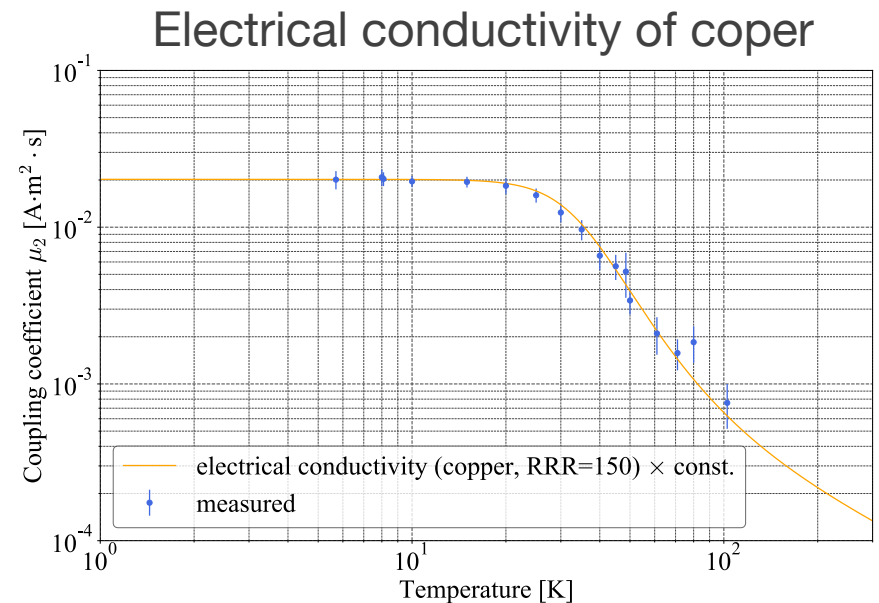
- ▶ This  $\tilde{\mu}$  induces torque noise  $\tilde{\mu} \times \mathbf{B}$  with DC magnetic field  $\mathbf{B}$

# Magnetic Noise Due to Eddy Current

- Induced eddy current  $\propto$  electric conductivity
- For metals electric conductivity gets larger when cooled down
  - ▶ Coupling gets larger at lower temperature



Transfer function  
from magnetic fluctuation to TM yaw



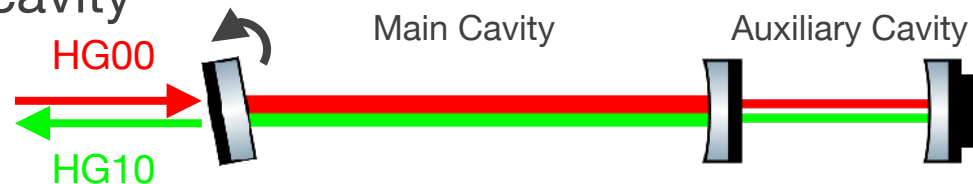
# High Sensitive Angular Sensor

Cavity-enhanced wave front sensor (new idea)

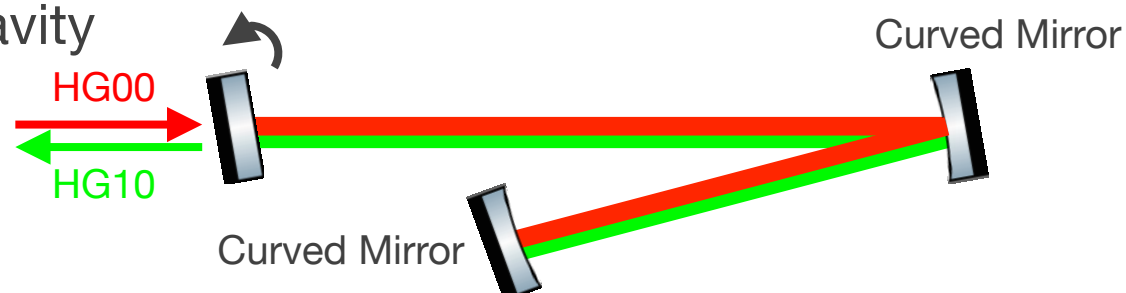
- Compensate Gouy phase difference between HG00 and HG10
  - ▶ HG10 mode resonates as well as HG00
  - ▶ Induced HG10 is enhanced
  - ▶ Higher sensitivity than normal WFS  
 $5 \times 10^{-16} \text{ rad}/\sqrt{\text{Hz}} @ 0.1 \text{ Hz}$

- How to compensate

- ▶ Auxiliary cavity

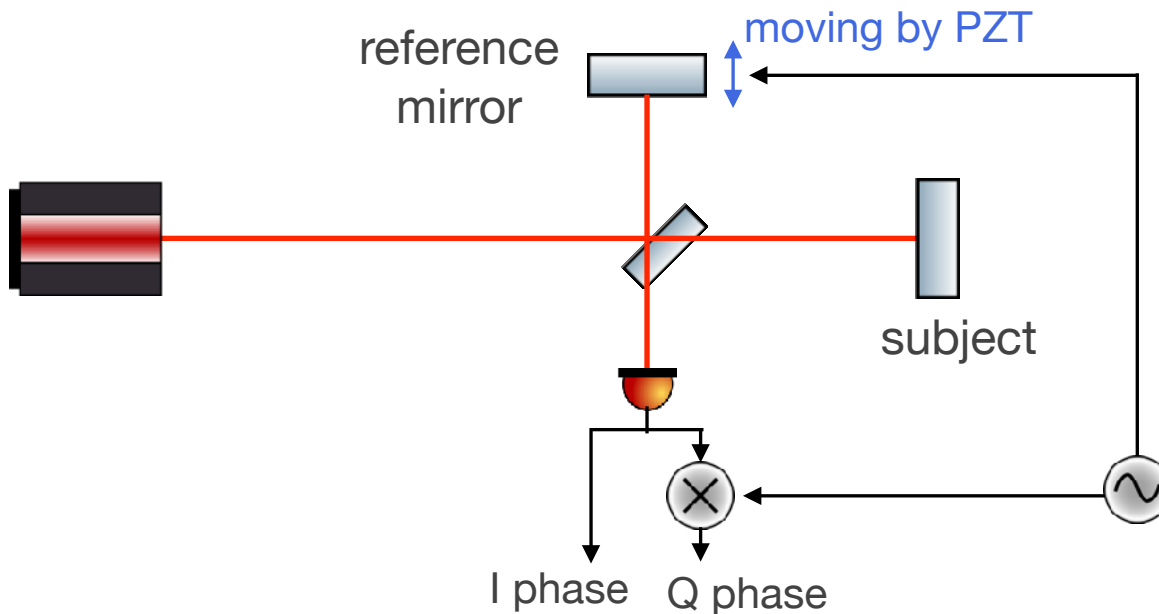


- ▶ Folded cavity

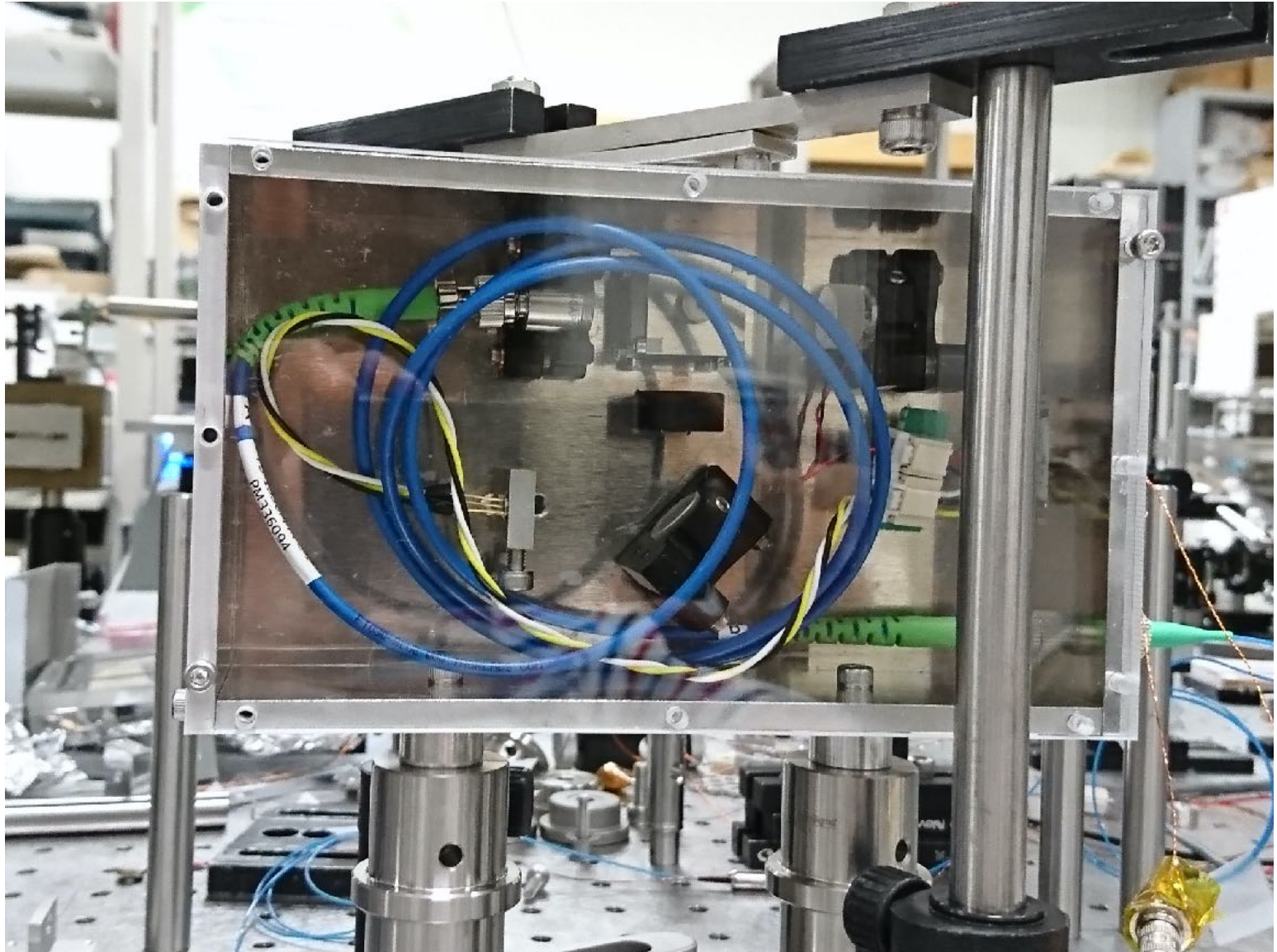


# Local Quadrature Interferometer

- Quadrature Interferometer for a local sensor of AVIS
- Michelson interferometer with a dithered reference mirror
  - ▶ Resolution: same as Michelson interferometer
  - ▶ Range:  $\infty$  (ideally)
- No polarization optics
- Generate quadrature signal by moving reference mirror



# Picture





# Performance

