

# Estimated sensitivity for auxiliary degrees of freedom of KAGRA interferometer

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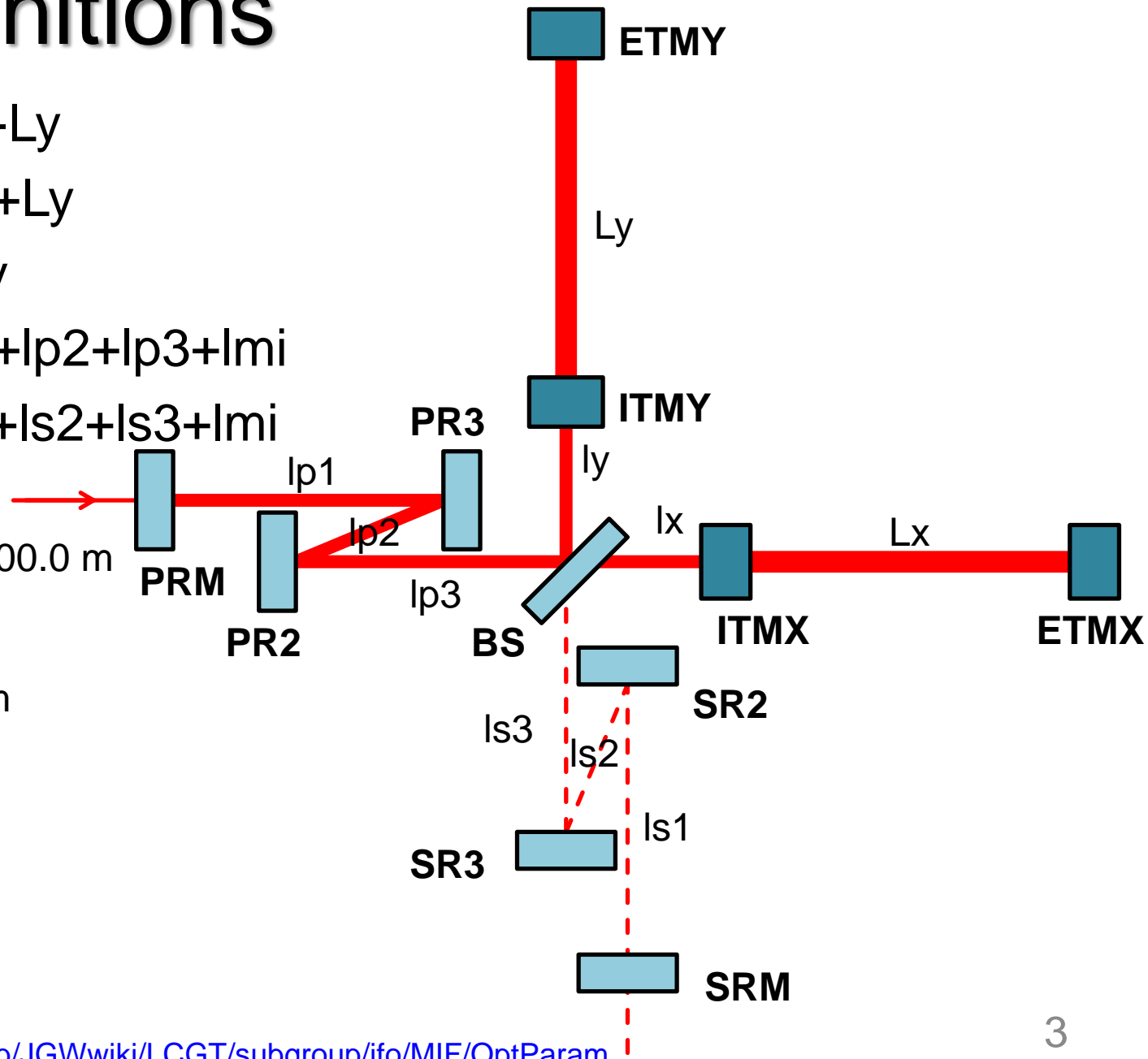
# Scope

- Estimate the displacement sensitivity for CARM, MICH, PRCL, SRCL
  - useful for the noise budget of auxiliary DoFs
- Based on the latest estimated sensitivity code ([JGW-T1707038](#))
- Seismic noise
  - fitted function from suspension model
- Suspension thermal noise
  - analytical calculation
- Mirror thermal noise
  - analytical calculation (we have to guess coating thickness)
- Quantum noise
  - analytical calculation for DARM, fitting of Optickle result for auxiliary DoFs

# Definitions

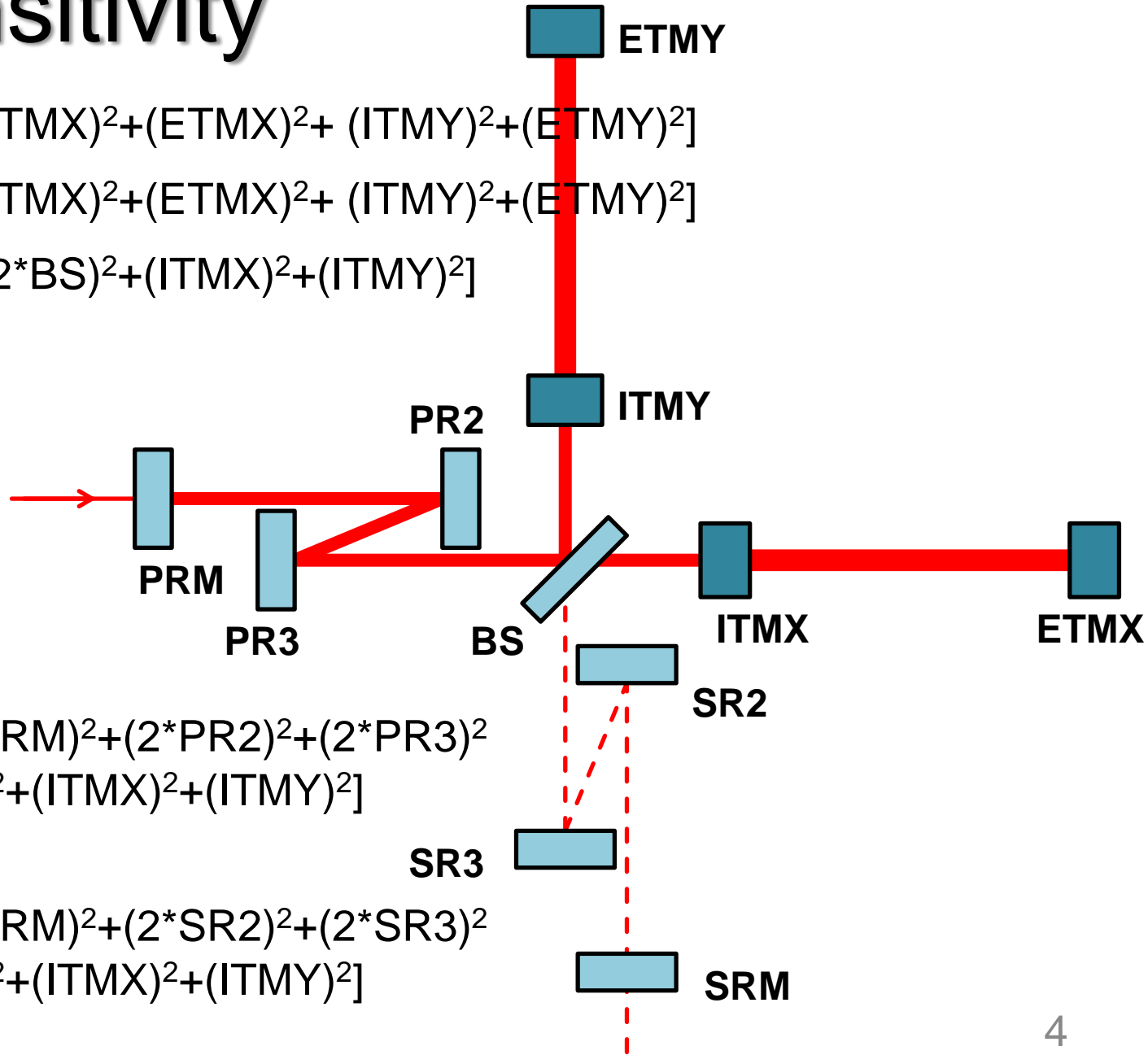
- DARM:  $L_x - L_y$
- CARM:  $L_x + L_y$
- MICH:  $l_x - l_y$
- PRCL:  $l_{p1} + l_{p2} + l_{p3} + l_{mi}$
- SRCL:  $l_{s1} + l_{s2} + l_{s3} + l_{mi}$

$L_x = L_y = L_{arm} = 3000.0 \text{ m}$   
 $L_x = 26.6649 \text{ m}$   
 $l_y = 23.3351 \text{ m}$   
 $l_{mi} = (l_x + l_y) / 2 = 25 \text{ m}$   
 $l_{p1} = 14.7615 \text{ m}$   
 $l_{p2} = 11.0661 \text{ m}$   
 $l_{p3} = 15.7638 \text{ m}$   
 $l_{s1} = 14.7412 \text{ m}$   
 $l_{s2} = 11.1115 \text{ m}$   
 $l_{s3} = 15.7386 \text{ m}$



# Sensitivity

- DARM:  $\sqrt{[(ITMX)^2+(ETMX)^2+ (ITMY)^2+(ETMY)^2]}$
- CARM:  $\sqrt{[(ITMX)^2+(ETMX)^2+ (ITMY)^2+(ETMY)^2]}$
- MICH:  $\sqrt{[(\sqrt{2}*BS)^2+(ITMX)^2+(ITMY)^2]}$

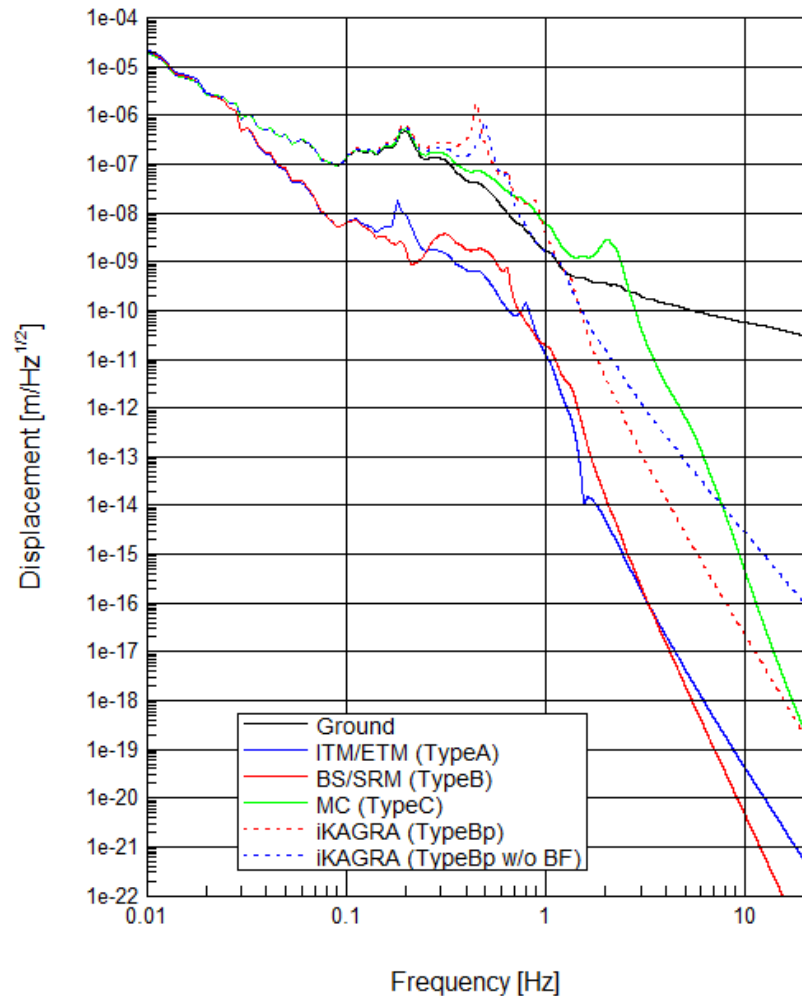


- PRCL:  $\sqrt{[(PRM)^2+(2*PR2)^2+(2*PR3)^2 +(\sqrt{2}/2*BS)^2+(ITMX)^2+(ITMY)^2]}$
- SRCL:  $\sqrt{[(SRM)^2+(2*SR2)^2+(2*SR3)^2 +(\sqrt{2}/2*BS)^2+(ITMX)^2+(ITMY)^2]}$

# Seismic noise

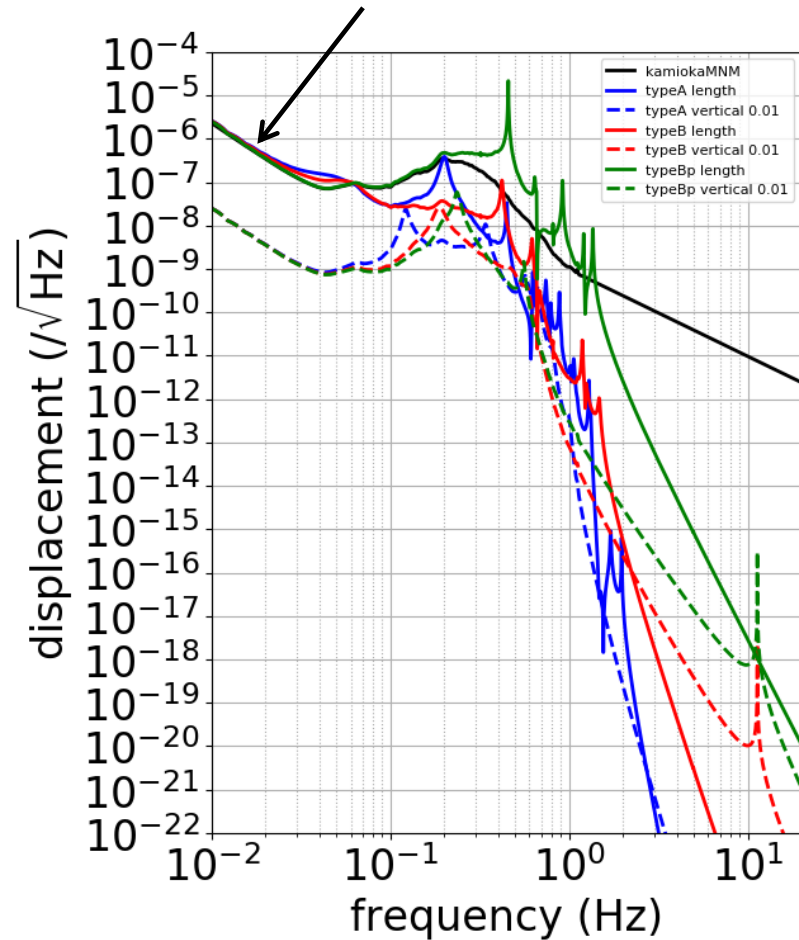
# Models

- There exists several models



TypeA-C rev3.png  
 from R. Takahashi  
 (used for K. Somiya's fitting)

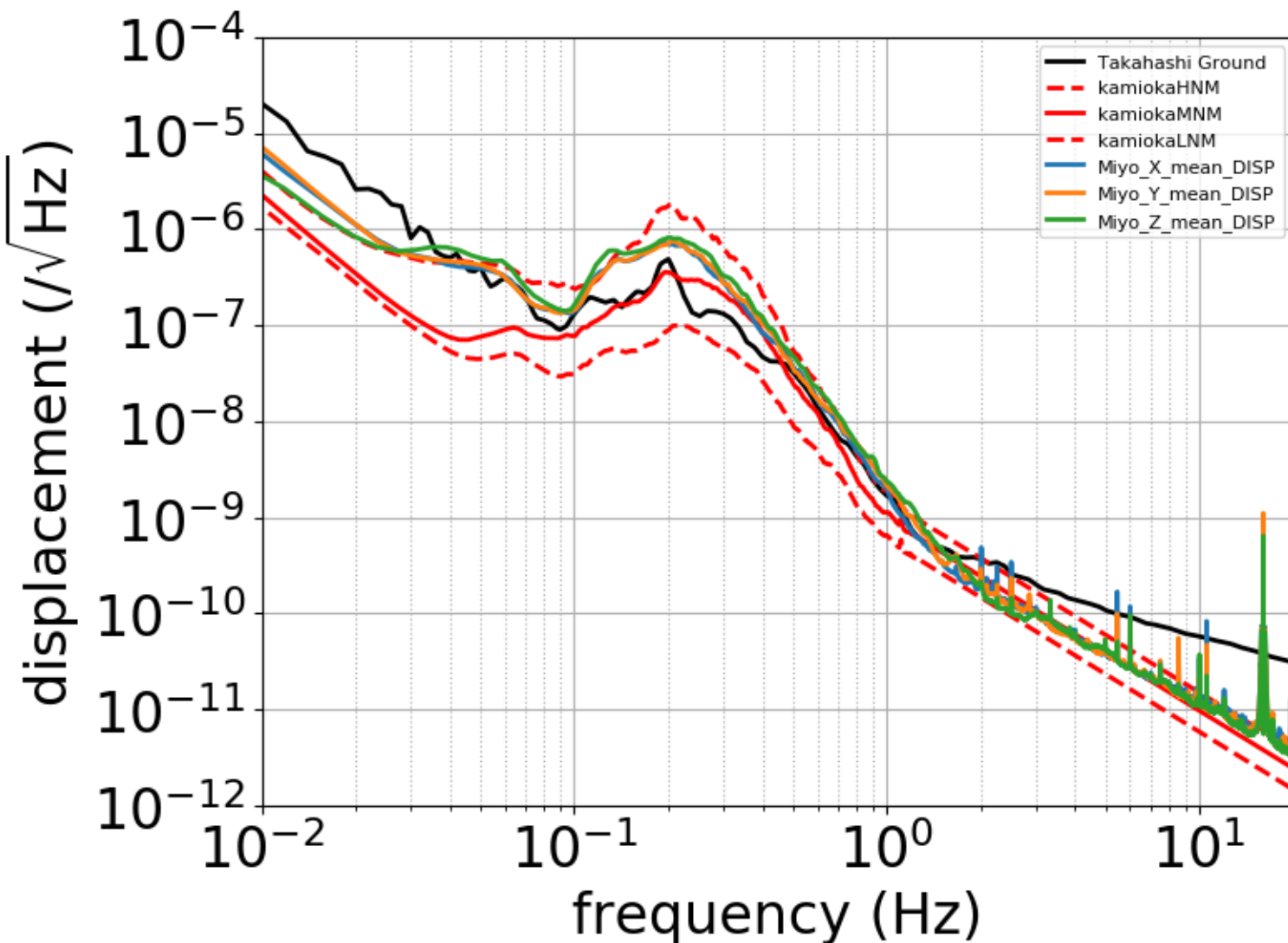
Medium Noise Model  
 from [JGW-T1402971](https://www.jgwg.org/jgw-t1402971)



Model from T. Sekiguchi  
 (used for actuator modeling in  
[JGW-P1707051](https://www.jgwg.org/jgw-p1707051))

# Seismic Noise Spectra

- Let's just use [JGW-T1402971](#) MNM for simplicity



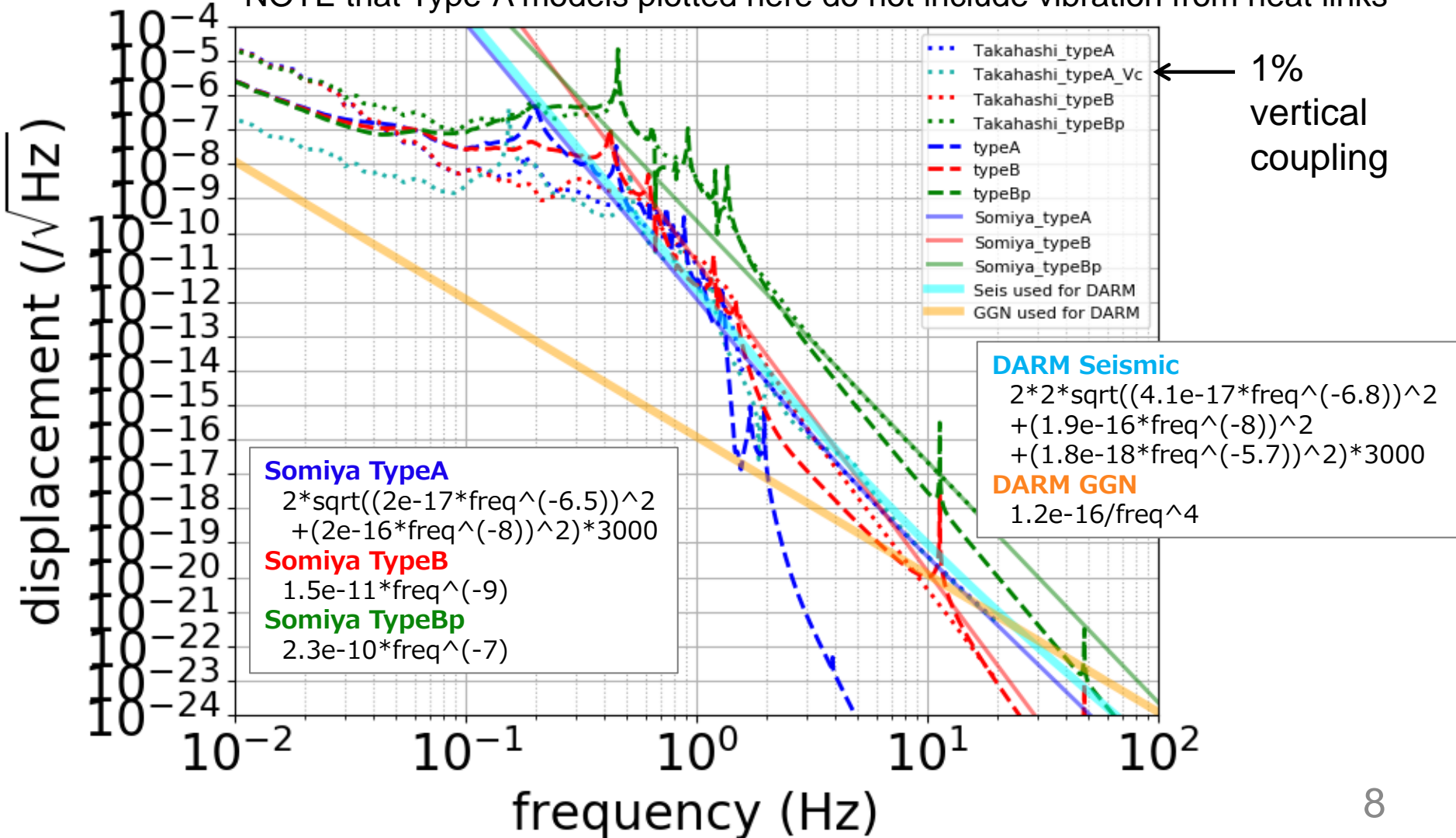
By Sekiguchi  
[JGW-T1402971](#)

By Miyo  
[JGW-T1910436](#)

# Comparison Between Models

- Fitting function by Somiya based on Takahashi model

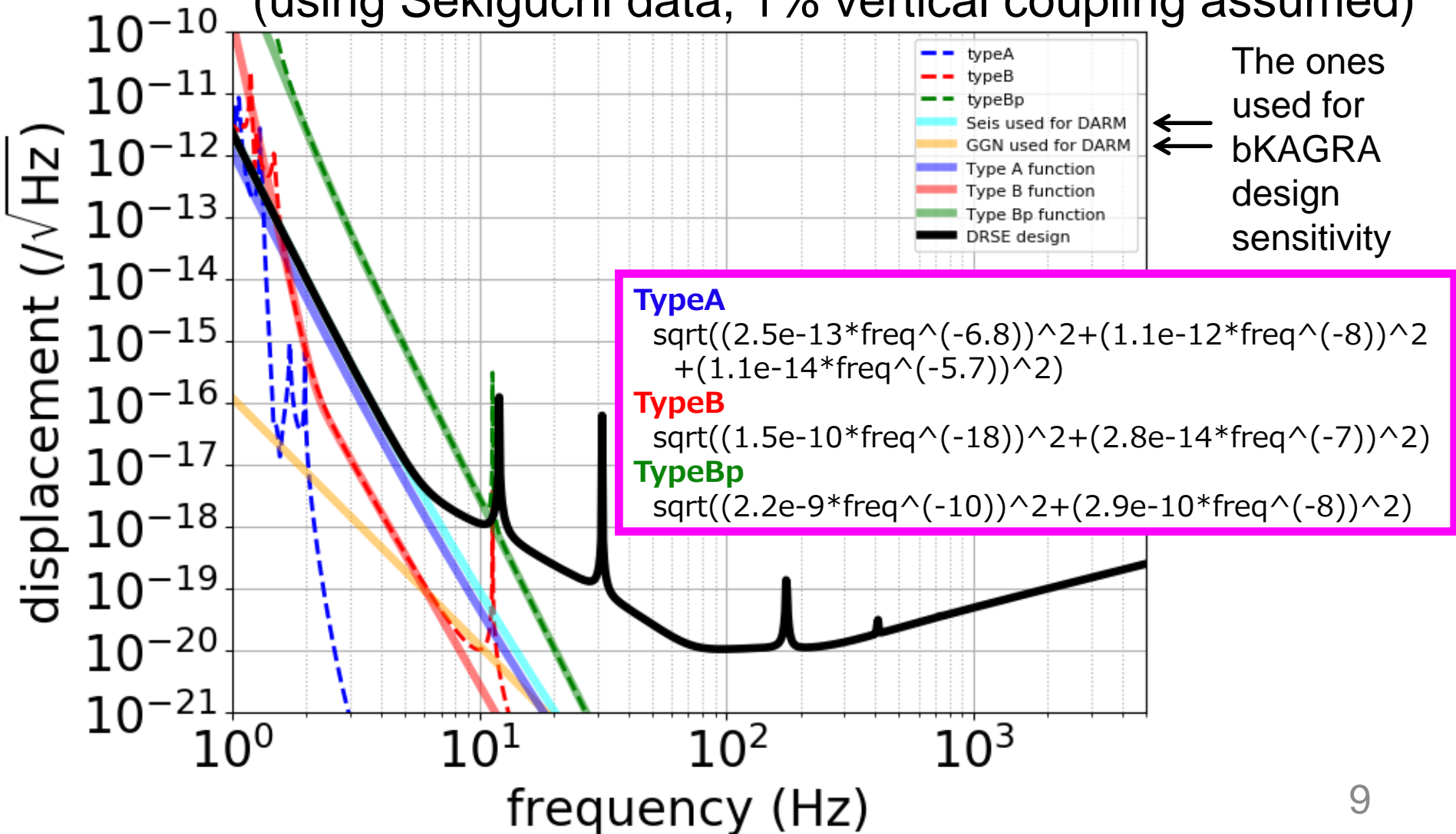
NOTE that Type-A models plotted here do not include vibration from heat links





# New Seismic Function

- Function for one optic that work above ~3 Hz  
(using Sekiguchi data, 1% vertical coupling assumed)



# Suspension thermal noise

# Type-A Payload Configuration

[CQG 34, 225001 \(2017\)](#)

## IM suspension

4 CuBe wires  
16 K  
26.1 cm long, 0.6 mm dia.  
loss angle  $5e-6$

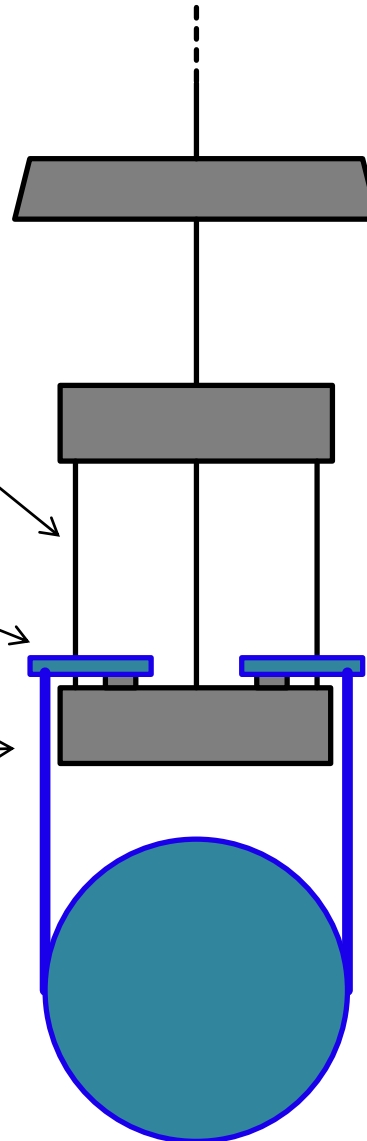
## Blade springs

4 Sapphire  
55 g each  
16 K  
loss angle  $7e-7$

## TM suspension

4 Sapphire fibers  
19 K (average of 16 K and 22 K)  
35 cm long, 1.6 mm dia.  
loss angle  $2e-7$

Vertical to horizontal coupling 1/200



**Platform**

**Marionette**

16 K

**Intermediate mass**

16 K

20.5 kg

**Test mass**

22 K

22.8 kg

# Type-B Payload Configuration

## IM suspension

1 maraging steel rod  
62.5 cm long, 3.6 m dia. body for BS  
59.85 cm long, 2.5 mm dia. body for SRs  
(neck 2.65 cm long, 2 mm dia.)  
loss angle  $2e-4$

[CQG 34, 225001 \(2017\)](#)

Type-B info from Fabian

Type-B maraging rod [JGW-D1605614](#)

BS mass budget [JGW-E1604966](#)

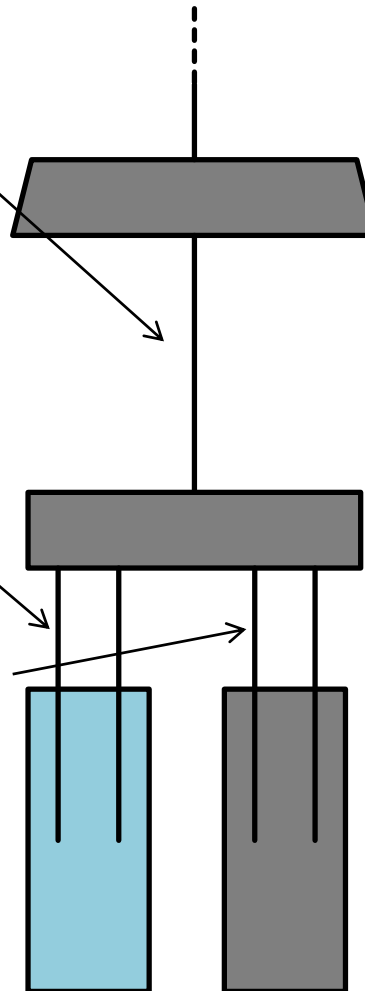
## TM suspension

4 piano wires  
55.1 cm long, 0.3 mm dia. for BS  
58.7 cm long, 0.2 mm dia. for SRs  
loss angle  $2e-4$

## RM suspension

4 tungsten wires  
55.1 cm long, 0.65 mm dia. for BS  
58.7 cm long, 0.6 mm dia. for SRs  
loss angle  $1.7e-4$

Vertical to horizontal coupling  $1/200$   
("neck" is ignored in the calculation)  
OK since vertical thermal noise is dominating



**Bottom filter**

**Intermediate mass**

34.6 kg for BS  
15.6 kg for SRs

**Test mass**

18.71 kg for BS  
10.71 kg for SRs

**Recoil mass**

22.3 kg for BS  
12.036 kg for SRs

# Type-Bp Payload Configuration

## IM suspension

1 maraging steel rod  
59.85 cm long, 2.5 mm dia. body for PRs  
(neck 2.65 cm long, 2 mm dia.)  
loss angle  $2e-4$

[CQG 34, 225001 \(2017\)](#)

Type-Bp info from Shoda (same as SRs)

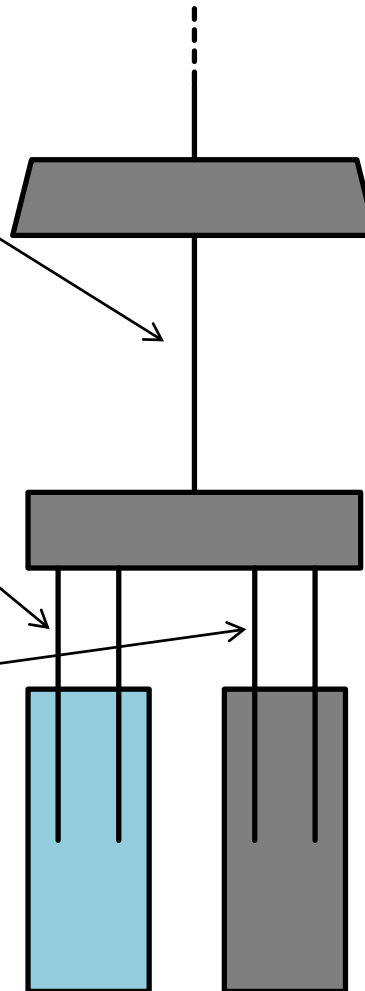
## TM suspension

4 piano wires  
58.7 cm long, 0.2 mm dia. for PRs  
loss angle  $2e-4$

## RM suspension

4 tungsten wires  
58.7 cm long, 0.6 mm dia. PRs  
loss angle  $1.7e-4$

Vertical to horizontal coupling  $1/200$   
("neck" is ignored in the calculation)  
OK since vertical thermal noise is dominating



**Bottom filter**

**Intermediate mass**  
15.6 kg for PRs

**Test mass**  
10.71 kg for PRs

**Recoil mass**  
12.036 kg for PRs

# Material Properties of Wires

- Sapphire (see [JGW-T1707038](#))
  - density:  $4.0 \times 10^3 \text{ kg/m}^3$
  - Young's modulus:  $4.0 \times 10^{11} \text{ Pa}$
  - loss angle:  $2 \times 10^{-7}$
- Piano wire (Nilaco 711267)
  - density:  $7.83 \times 10^3 \text{ kg/m}^3$  ([W. R. Bennett Jr., Science of Musical Sound: Volume 1](#))
  - Young's modulus:  $2 \times 10^{11} \text{ Pa}$  ([W. R. Bennett Jr., Science of Musical Sound: Volume 1](#))
  - loss angle:  $2 \times 10^{-4}$  ([RSI 86, 084501 \(2015\)](#))
- Tungsten wire (Nilaco 461406)
  - density:  $19.3 \text{ kg/m}^3$  ([matweb](#))
  - Young's modulus:  $4.0 \times 10^{11} \text{ Pa}$  ([matweb](#))
  - loss angle:  $1.7 \times 10^{-4}$  ([PLA 255, 230 \(1999\)](#))
- Maraging steel rod (Daido MAS-1)
  - density:  $8.02 \text{ kg/m}^3$  (see right)
  - Young's modulus:  $1.82 \times 10^{11} \text{ Pa}$  (see right)
  - loss angle:  $2 \times 10^{-4}$  ([N. A. Robertson 2001](#))

Maraging steel spec sheet from R. Takahashi

30

マルエージング鋼 MAS-1 (MAS-1は大同特許)

要 旨 MAS-1は低炭素 18%Ni 鋼に時効硬化元素として Co, Mo, Ti, Al 等を加えた材料で、時効硬化処理によって 1960N/mm<sup>2</sup> 以上の強度を得られると共に靱性も持ち合わせた代表的な超強力鋼で時計部品、電算機部品、精密パネ、ダイヤモンドその他の極めて高度の信頼性を要求される部品等に使用されています。

特 長 (1) 比較的簡単な時効硬化処理のみによって 1960N/mm<sup>2</sup> 以上の引張強さが得られます。この強度は冷間加工を施すと更に上昇し、例えば 50%圧延材の時効硬化後の引張強さは 2110N/mm<sup>2</sup> 以上になります。  
 (2) この高強度の上、靱性もあり、高い切欠強度や疲労強度を有しております。  
 (3) 熱処理が急冷等の必要もなく簡単で、熱処理による歪も極小です。  
 (4) 比較的良い溶接性と切削性を有しております。  
 (5) 冷間加工による硬化がわずかです。(50%圧延でHV40 前後の増加程度)

組成化学成分

	%								
C	Si	Mn	P-S	Ni	Co	Mo	Ti	Al	
≤0.03	≤0.10	≤0.10	≤0.010	18.00~ 19.00	8.50~ 9.50	4.70~ 5.20	0.50~ 0.70	0.05~ 0.15	

物理的性質

密度	比熱	電気抵抗	ヤング率	熱膨張係数	熱伝導率
Mg/m <sup>3</sup>	J/(kg·K)	μΩ·cm	N/mm <sup>2</sup>	(20~480°C)	W/(m·K)
8.02	335	60~70	182,000	10.1×10 <sup>-6</sup> /K	19.7 (25°C)

取扱い上の注意事項 (1) 固溶化熱処理は 820~870°C で数分~30 分保持した上冷却します。Ms 点が 150°C 近辺であるため、常温で低炭素マルテンサイト相になり 300~330HV 位になっています。このため靱性はあるものの一般軟質材のような加工はできません。  
 (2) 標準的な時効硬化処理条件は 480°C 3h ですが、多少の温度・時間の組合せを変えることは可能です。  
 (3) 熱処理の雰囲気は、水素または AX ガスが適当です。  
 (4) 高合金鋼のため一見ステンレス鋼のように錆びにくい材料と思われがちですが、不銹成分であるクロムを含まないため、一般鉄鋼に準じた防錆処置が必要です。

14

# Mirror thermal noise

# Mirror and Coating Parameters

- Coating: silica/tantala (loss angle:  $3e-4$  /  $5e-4$ )

	ITM/ETM	BS	SRM/2/3	PRM/2/3
Material	Sapphire	Fused silica	Fused silica	Fused silica
Diameter	22 cm	37 cm	25 cm	25 cm
Thickness	15 cm	8 cm	10 cm	10 cm
Mass	22.8 kg	18.9 kg	10.8 kg	10.8 kg
Temperature	22 K	290 K	290 K	290 K
Substrate loss angle	$1e-8$	$1/(6.5e-12/thickness+7.6e-12*f^{0.77})$ <a href="#">Physics Letters A 352, 3 (2006)</a>		
Coating layers	22 / 40	<b>tantala/silica/tantala</b> (see p.10 of <a href="#">JGW-T1503347</a> )	<b>4 / 18 / 18</b>	<b>4 / 18 / 18</b>
Beam radius	3.5 cm	3.62 cm	0.43 / 0.43 / 3.67 cm	0.46 / 0.46 / 3.66 cm

Number of coating layers for fused silica mirrors are derived from calculation using reflectivity. Coating thermal noise of Type-B/Bp suspensions are not very important since quantum noises for auxiliary DOFs are quite high.

BS thermal noise is tricky ([LIGO-T0900209](#)) but not considered carefully here.

[JGW-T1707038](#)

[Classical and Quantum Gravity 34, 225001 \(2017\)](#)

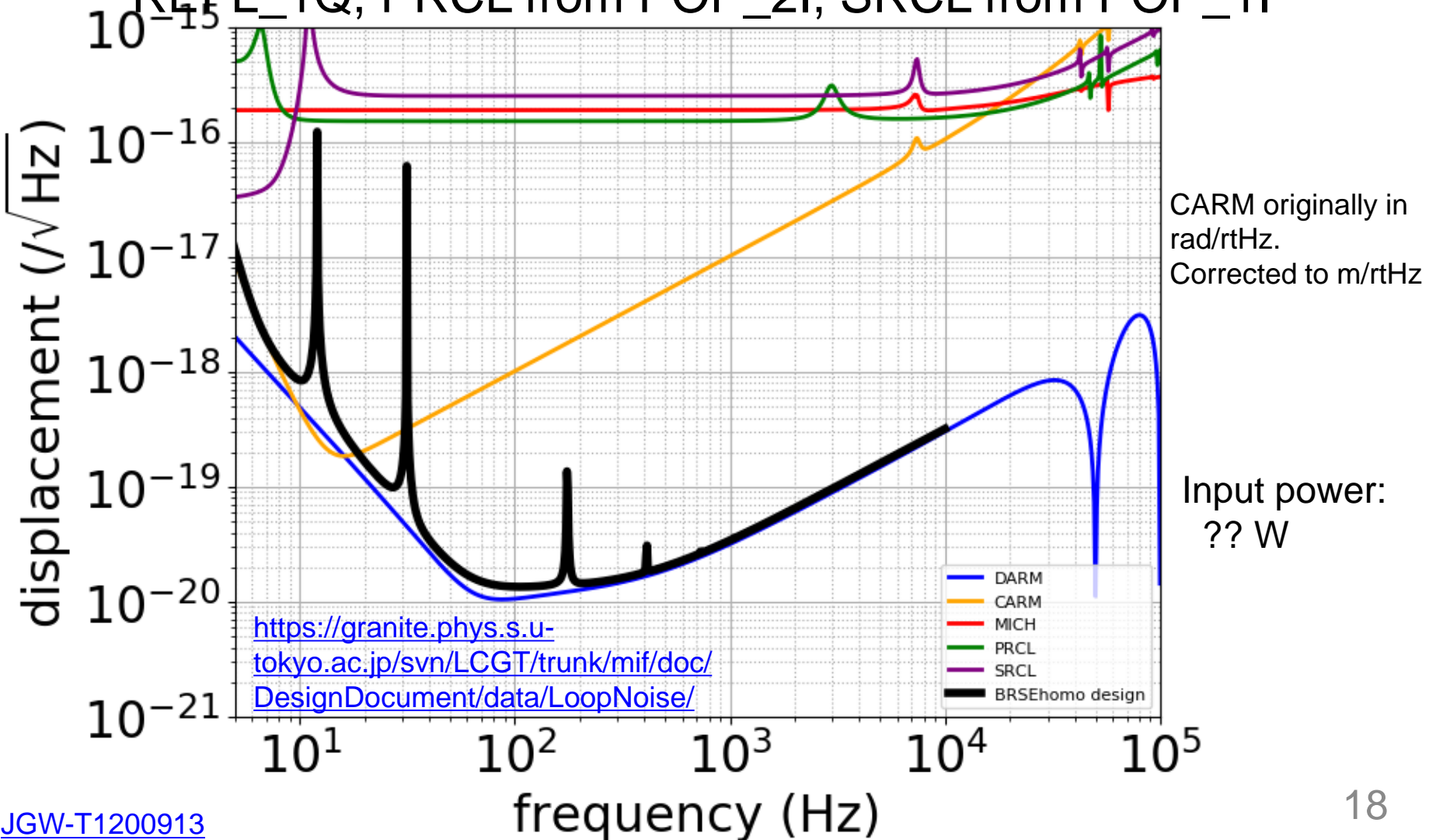
<http://gwwiki.icrr.u-tokyo.ac.jp/JGWwiki/LCGT/subgroup/ifo/MIF/OptParam>



# Quantum noise

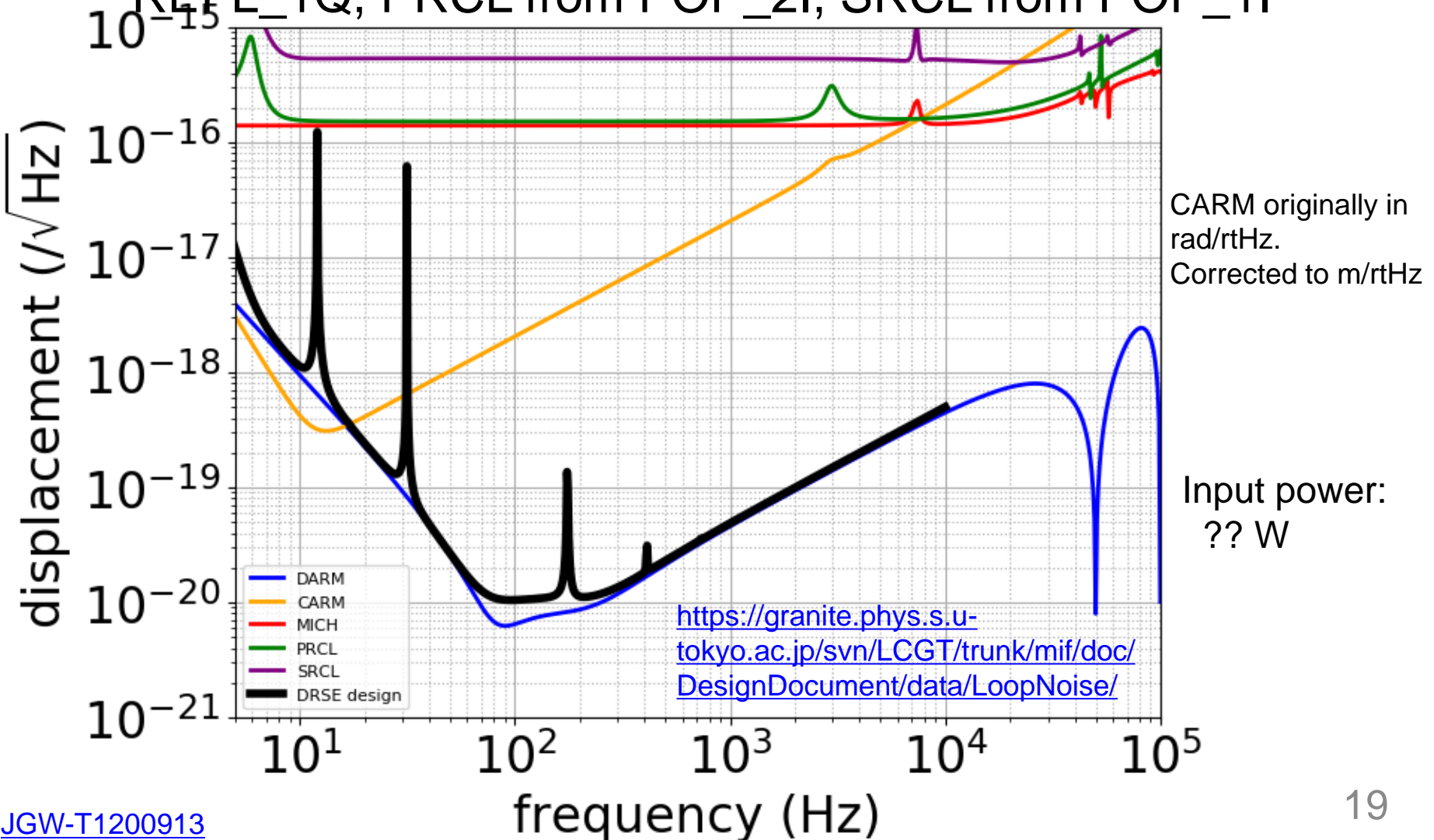
# Optickle Simulation (BRSE Aso)

- DARM from AS\_DC, CARM from REFL\_1I, MICH from REFL\_1Q, PRCL from POP\_2I, SRCL from POP\_1I



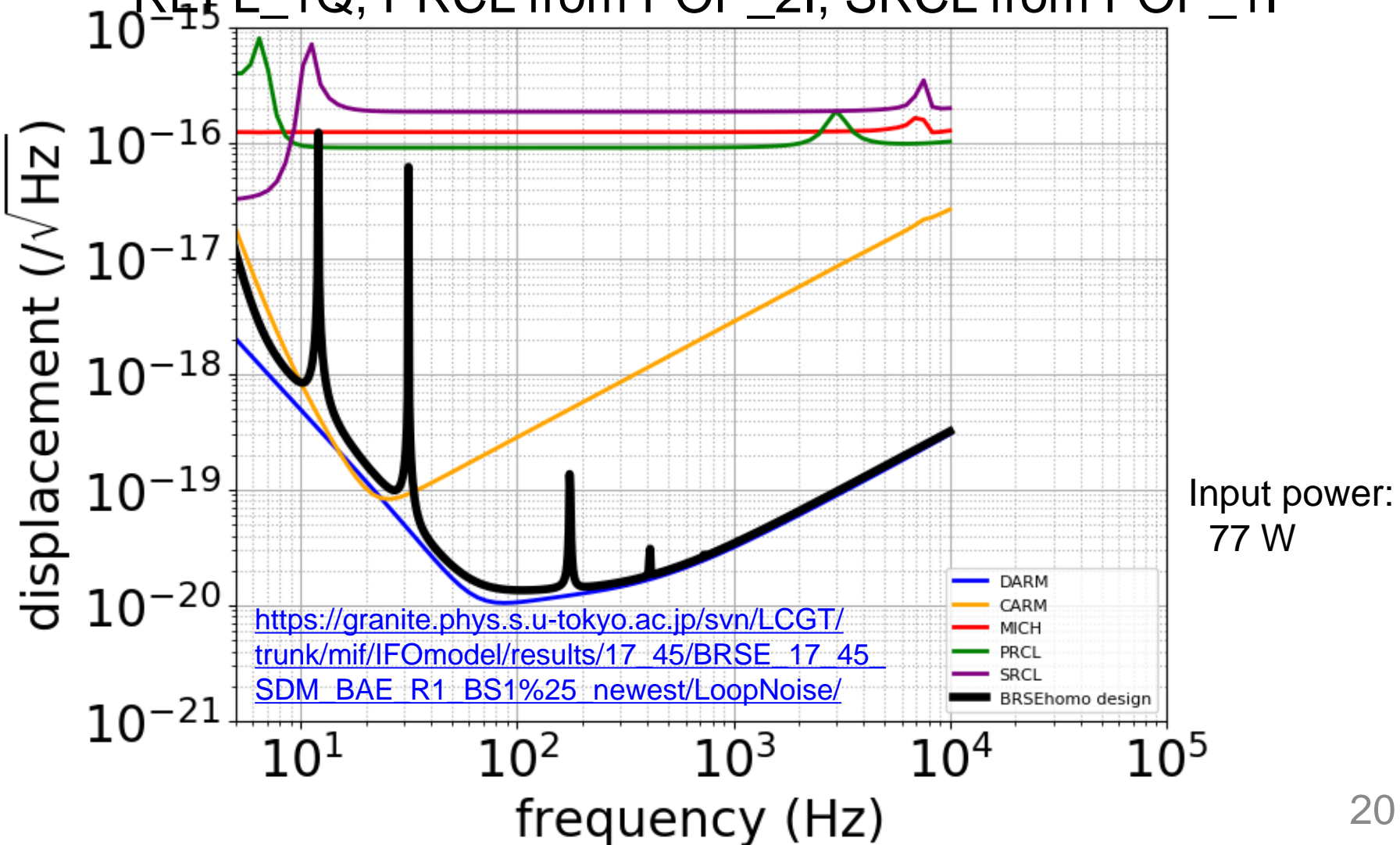
# Optickle Simulation (DRSE Aso)

- DARM from AS\_DC, CARM from REFL\_2I, MICH from REFL\_1Q, PRCL from POP\_2I, SRCL from POP\_1I



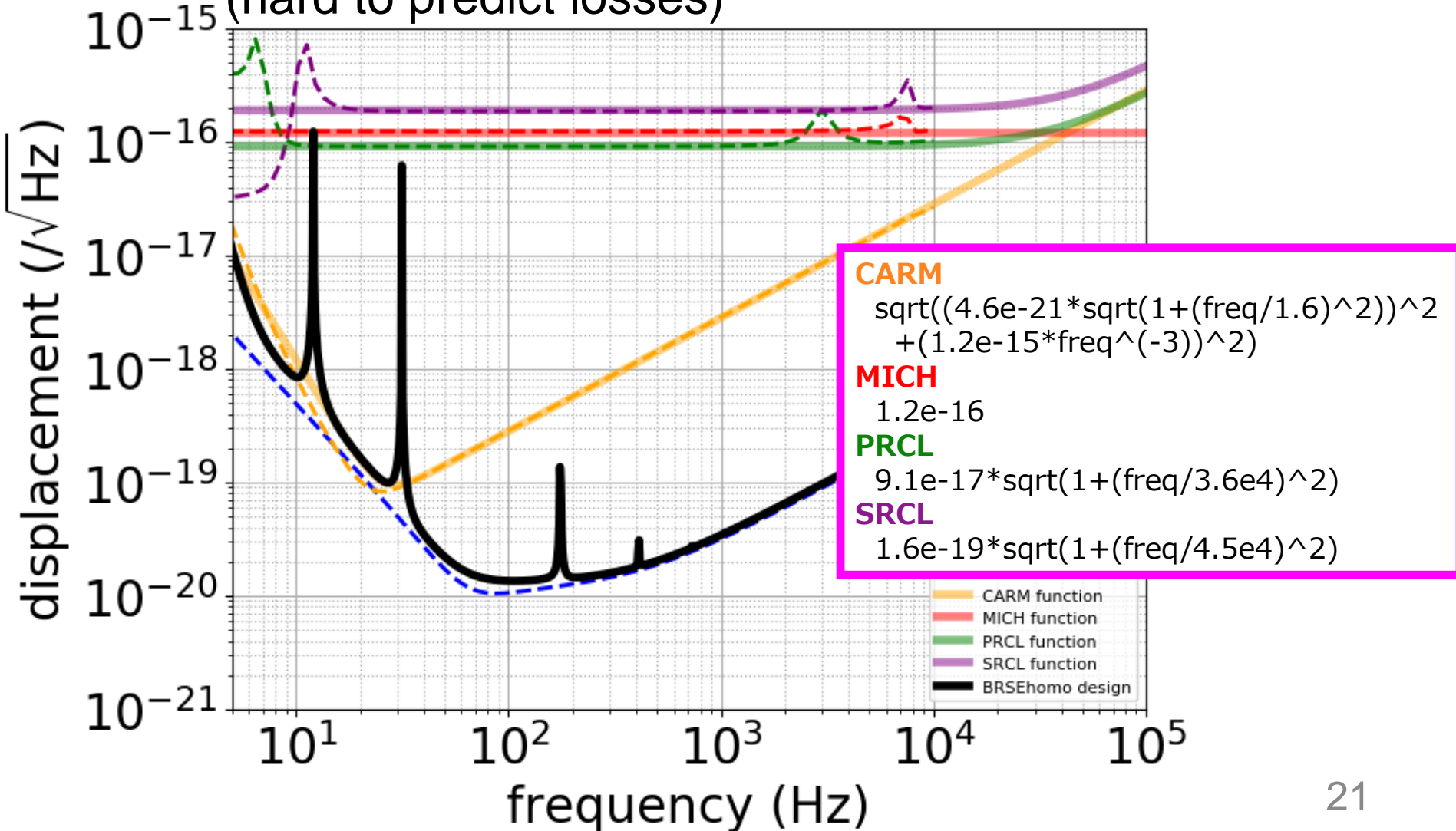
# Optickle Simulation (BRSE Enomoto)

- DARM from AS\_DC, CARM from REFL\_1I, MICH from REFL\_1Q, PRCL from POP\_2I, SRCL from POP\_1I



# Quantum Function

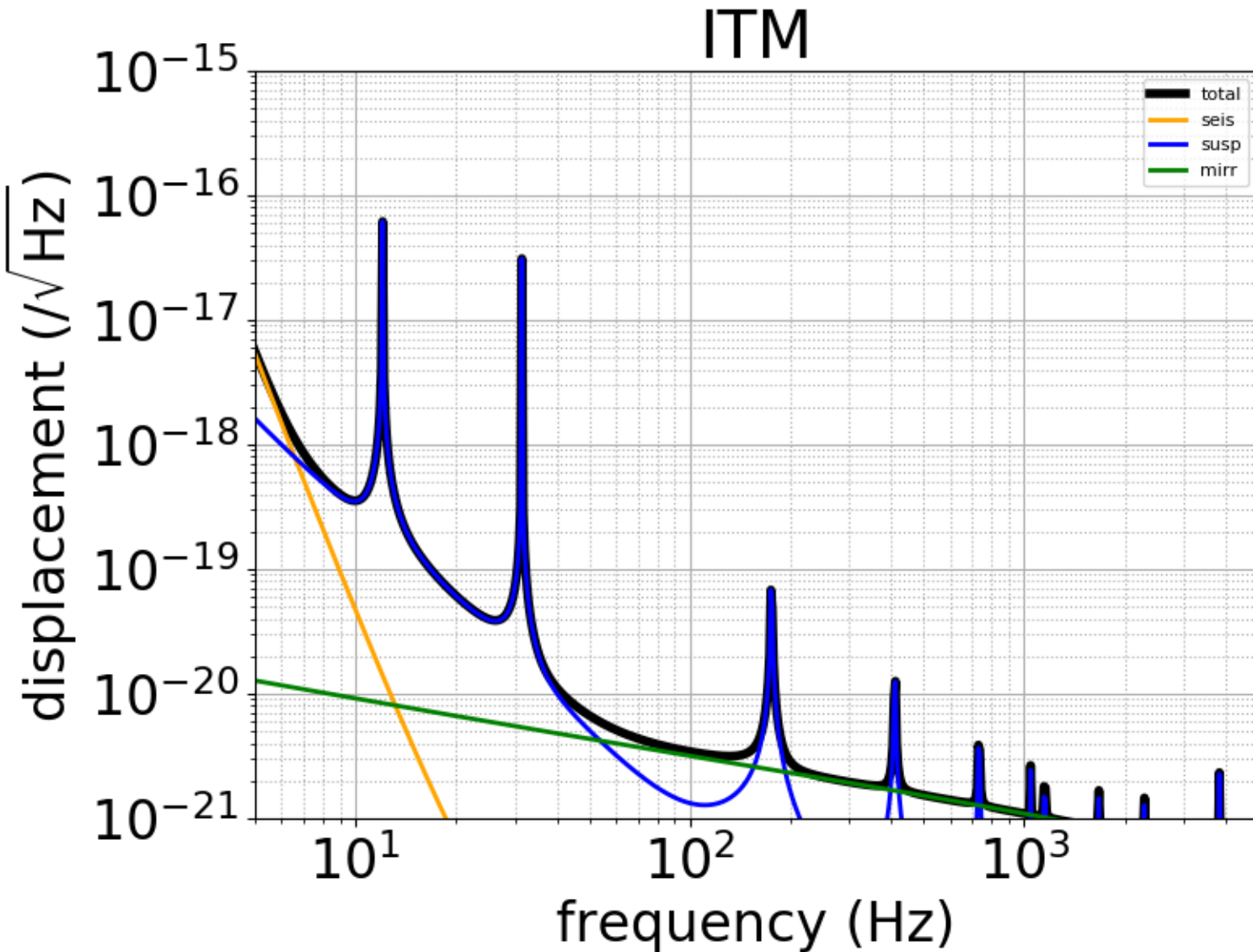
- Use fitted function instead of doing analytical calculation (hard to predict losses)



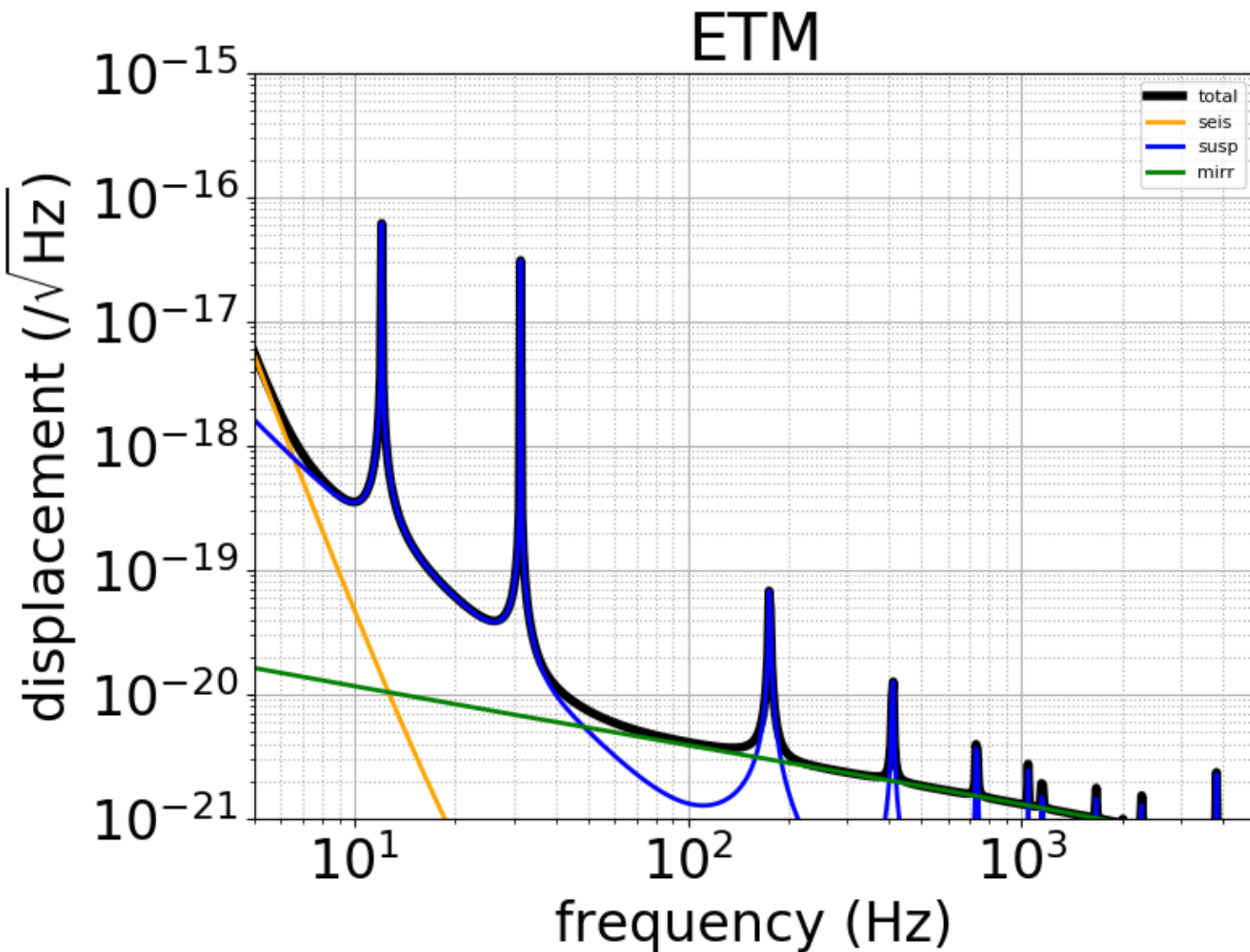
# Displacement sensitivity

Codes for plotting these sensitivity curves lives in the zip file of [JGW-T2011755](#)

# Displacement Noise: ITM

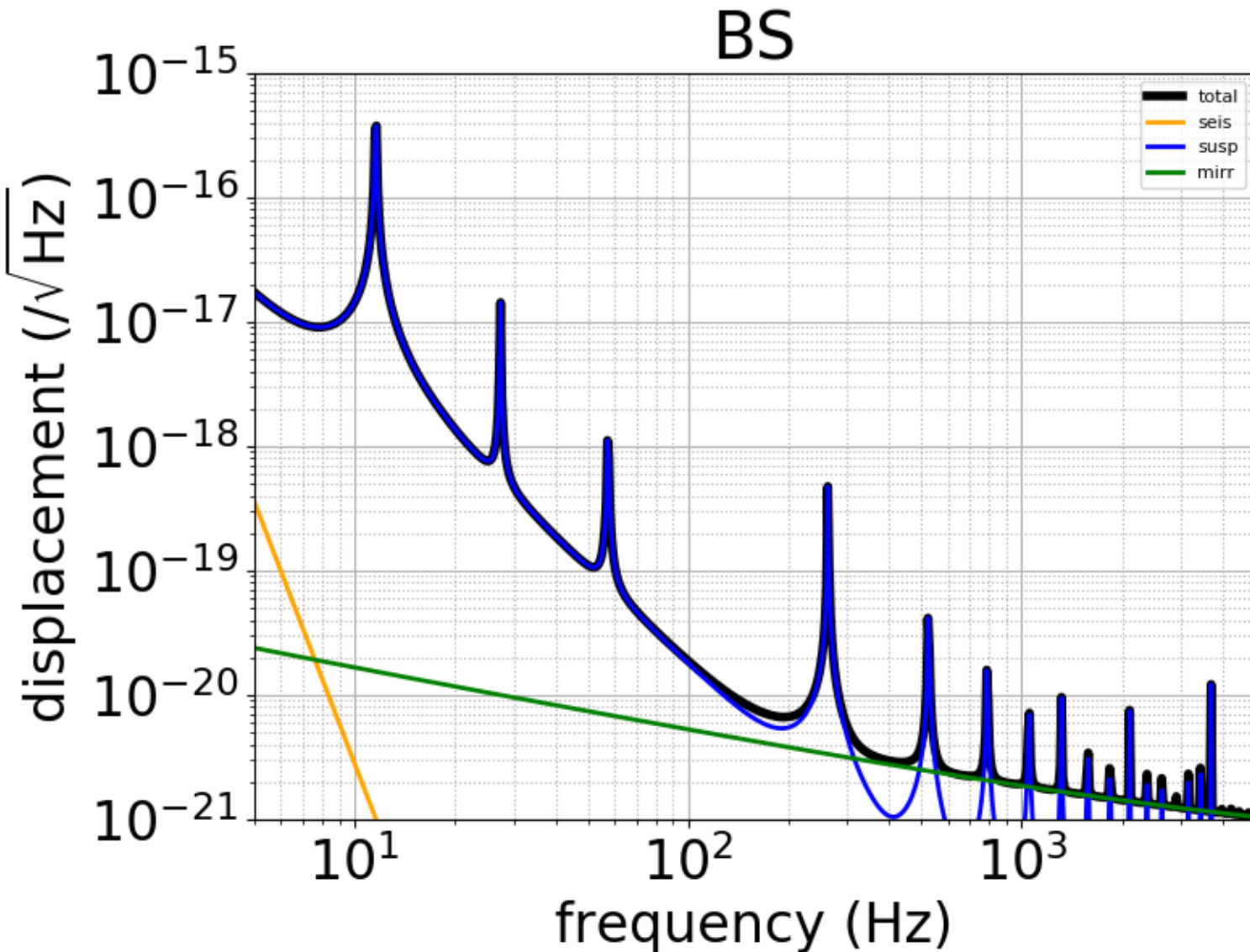


# Displacement Noise: ETM

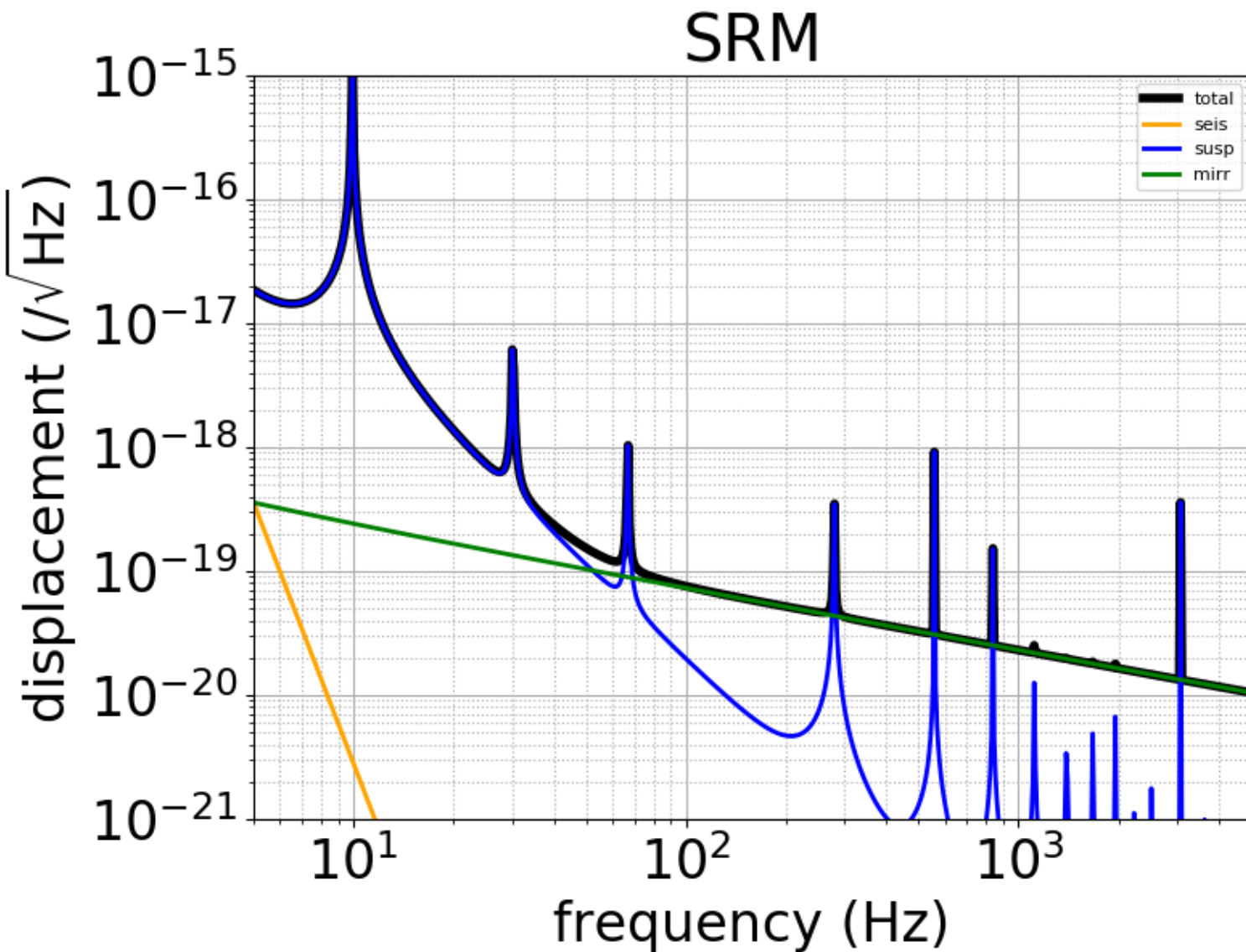




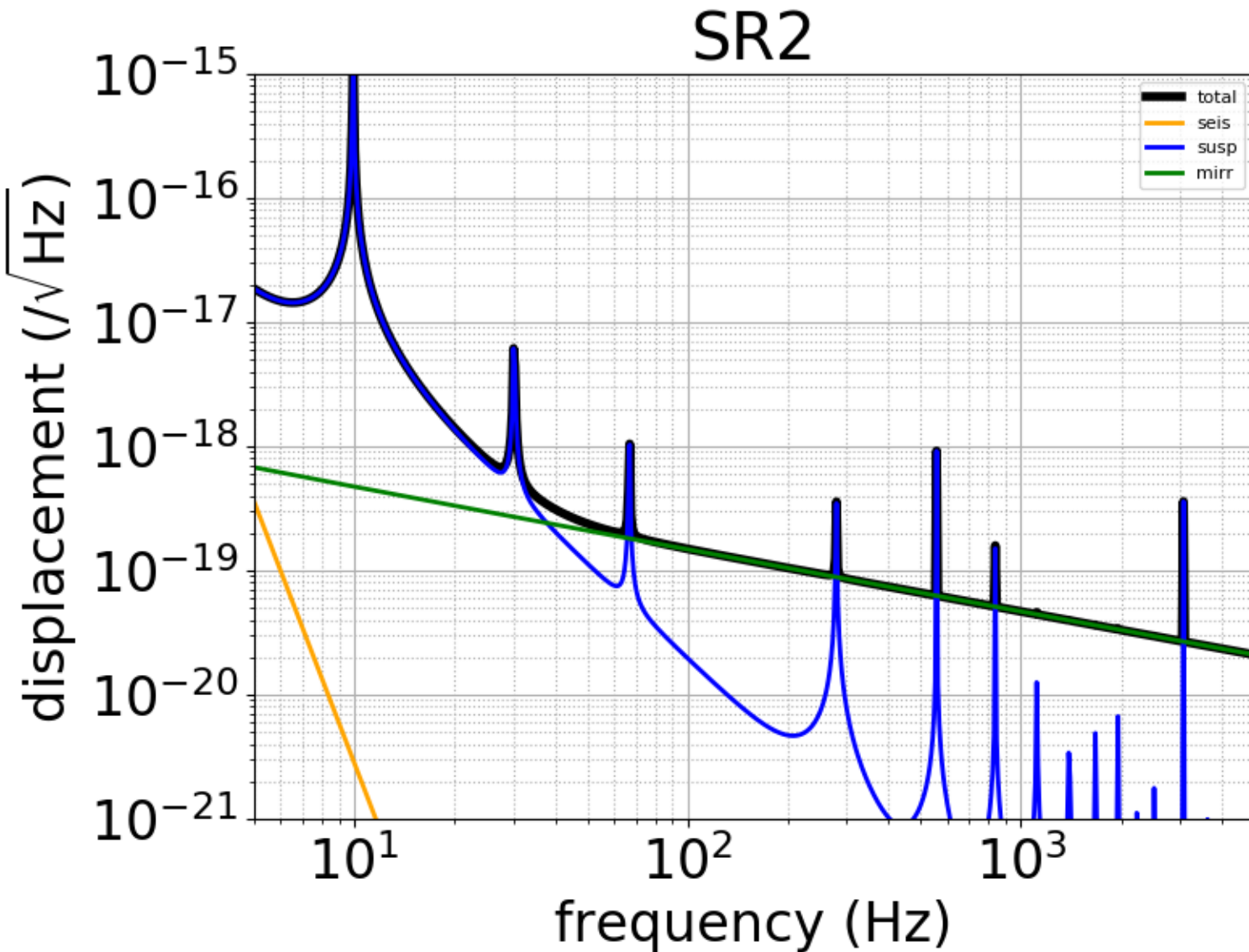
# Displacement Noise: BS



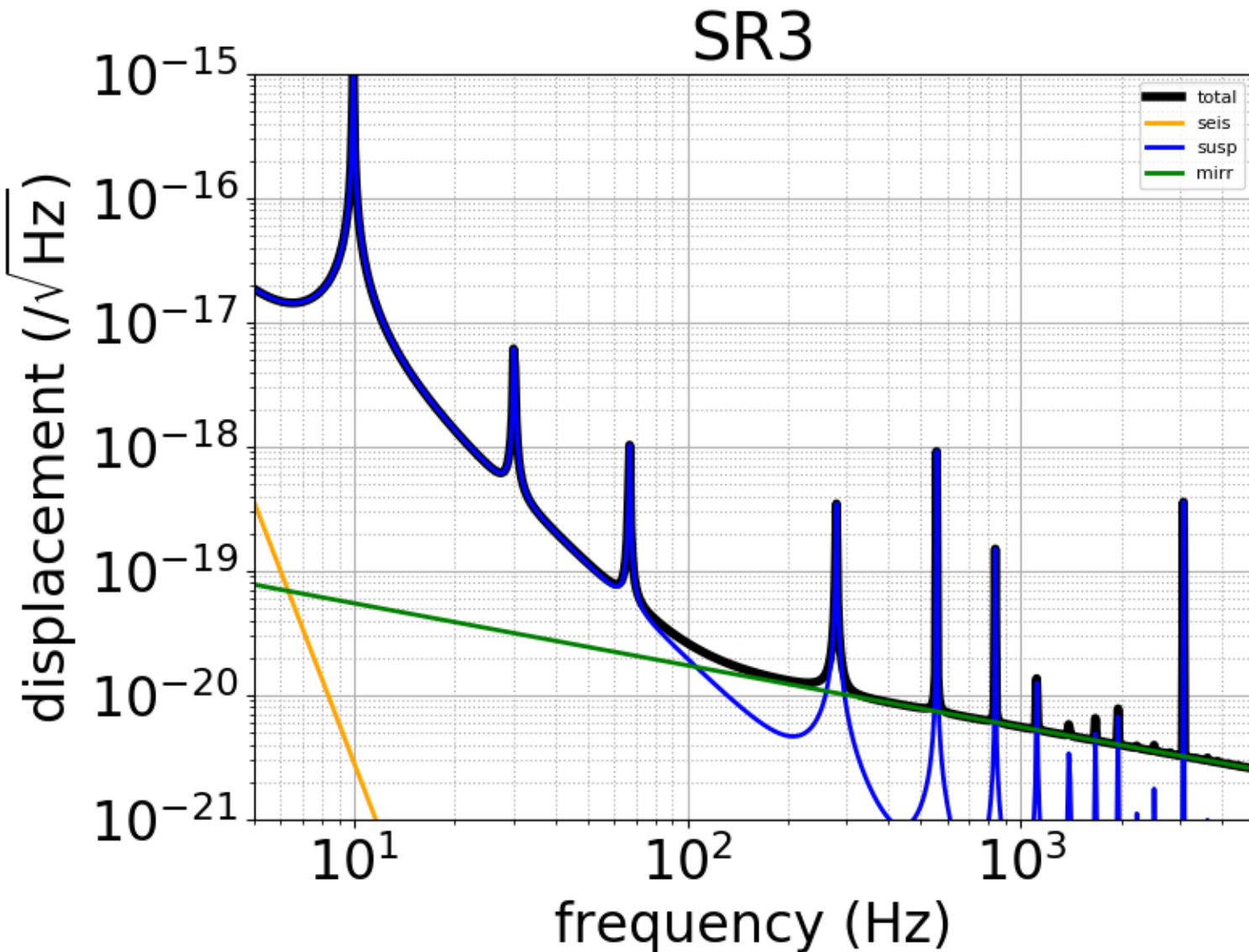
# Displacement Noise: SRM



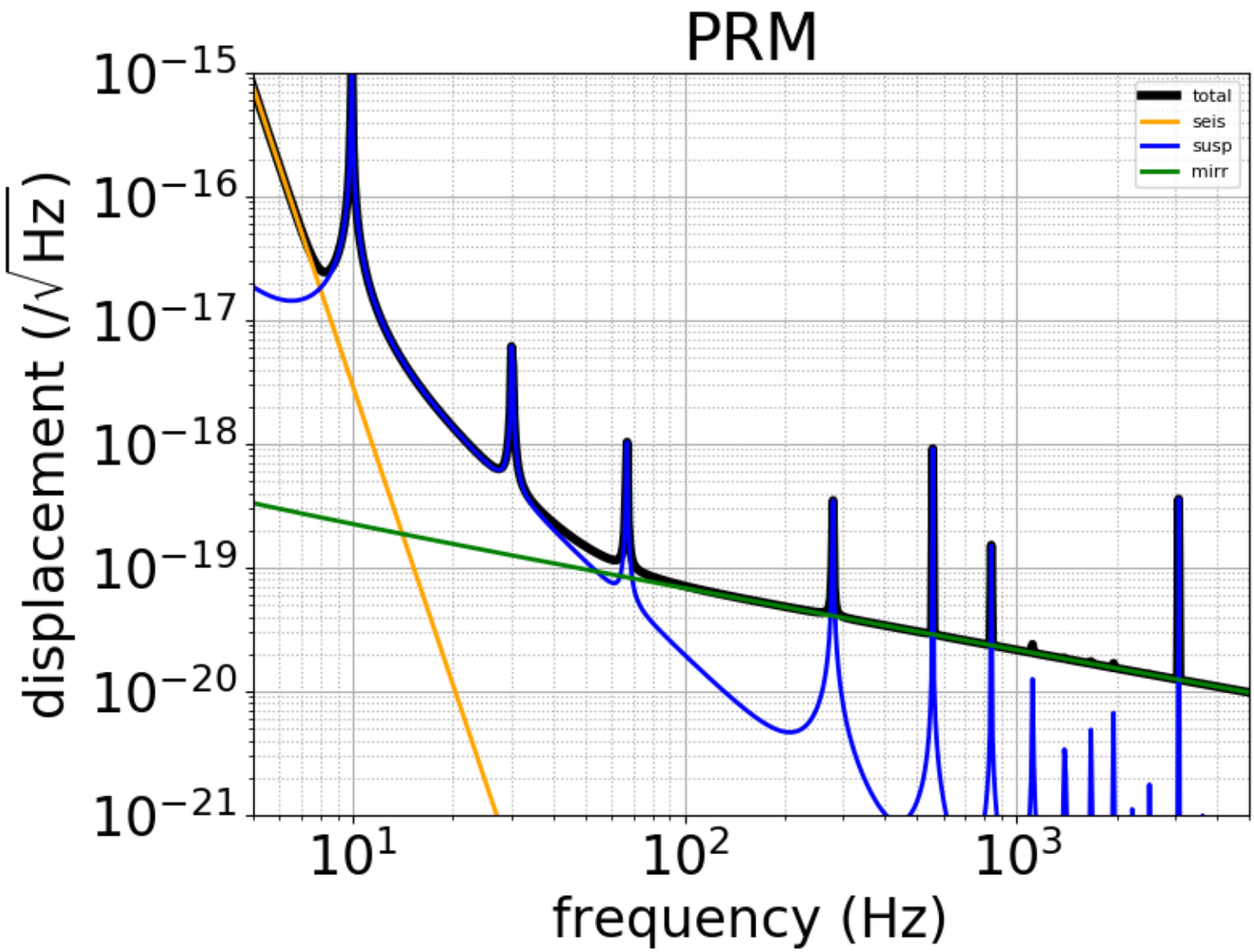
# Displacement Noise: SR2



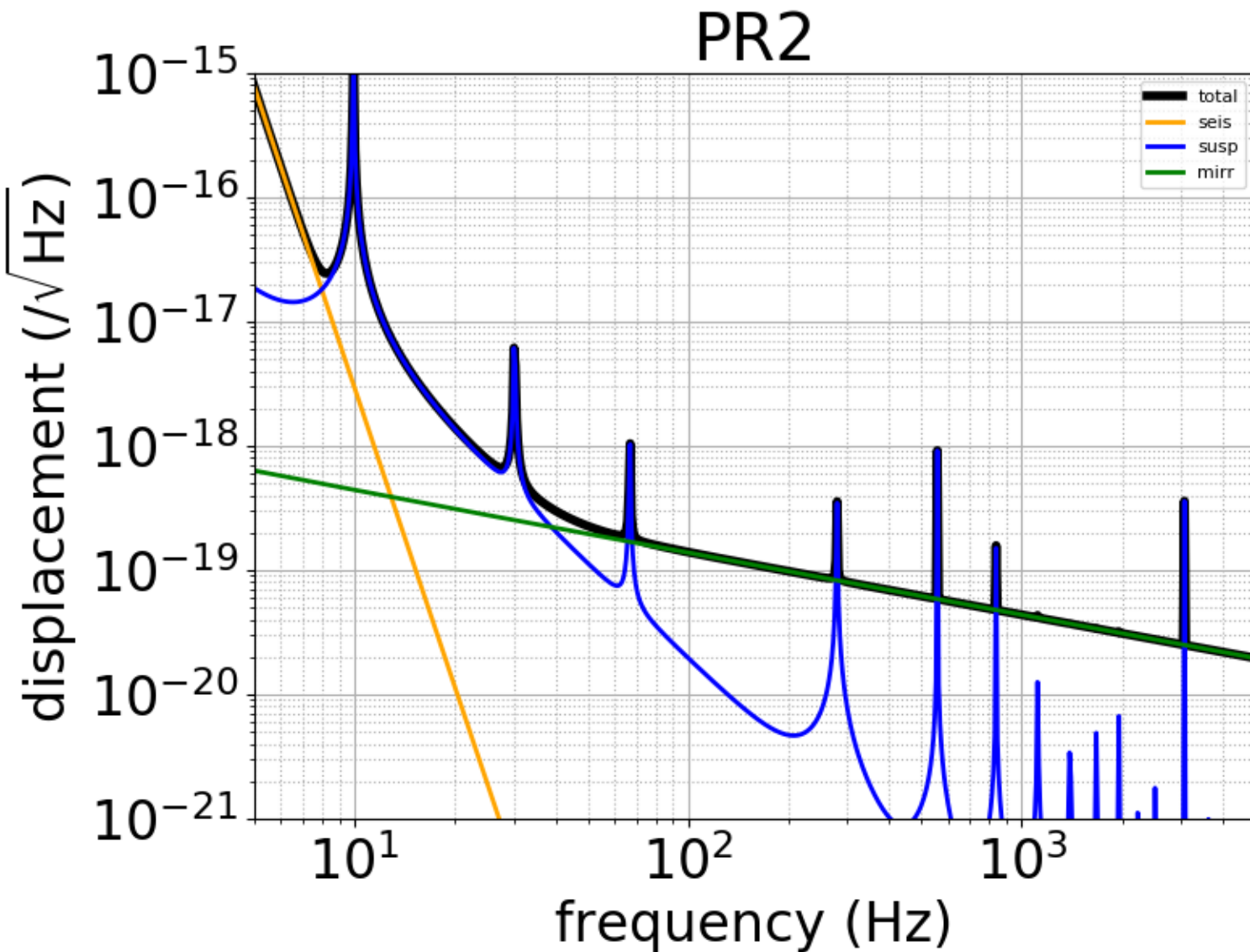
# Displacement Noise: SR3



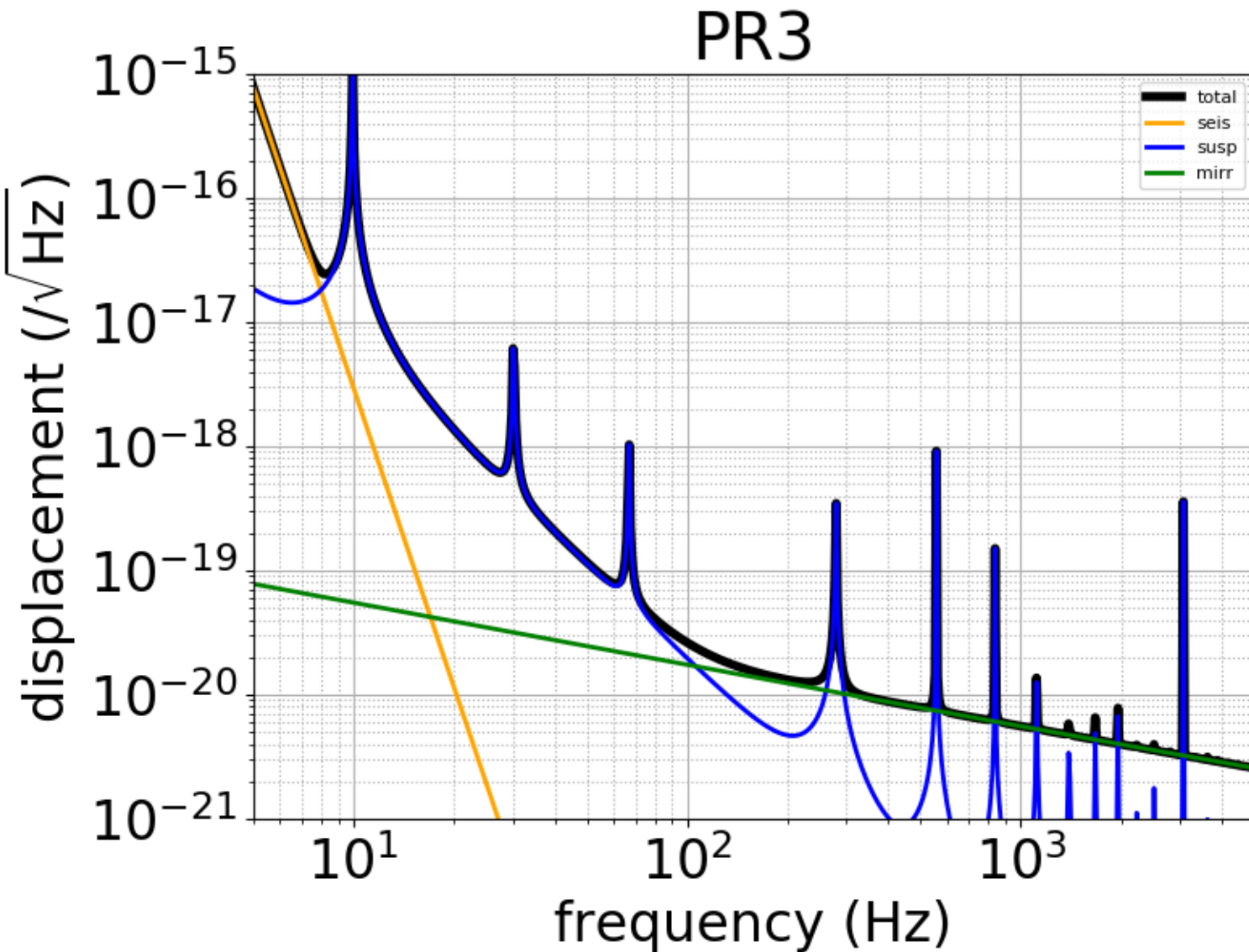
# Displacement Noise: PRM



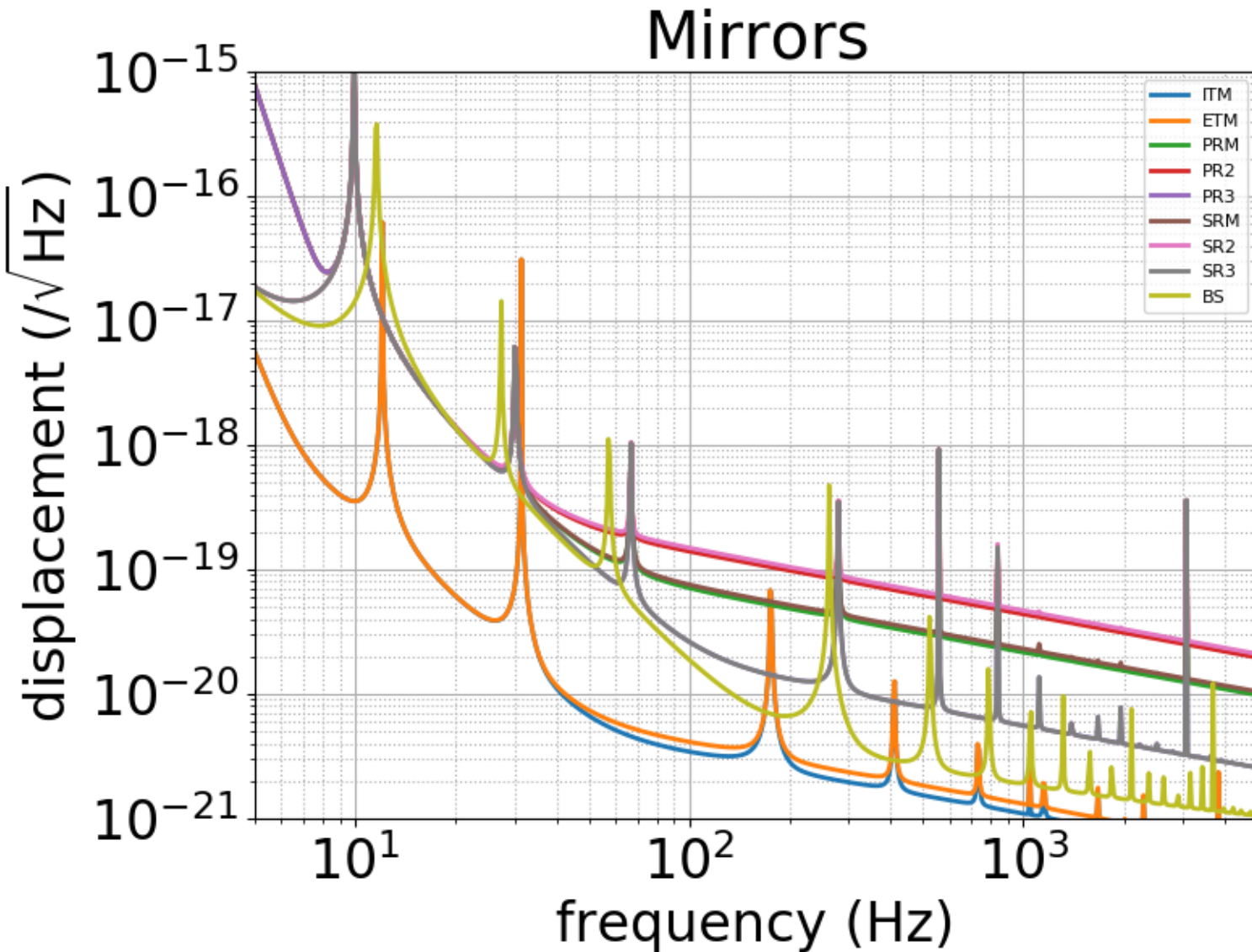
# Displacement Noise: PR2



# Displacement Noise: PR3

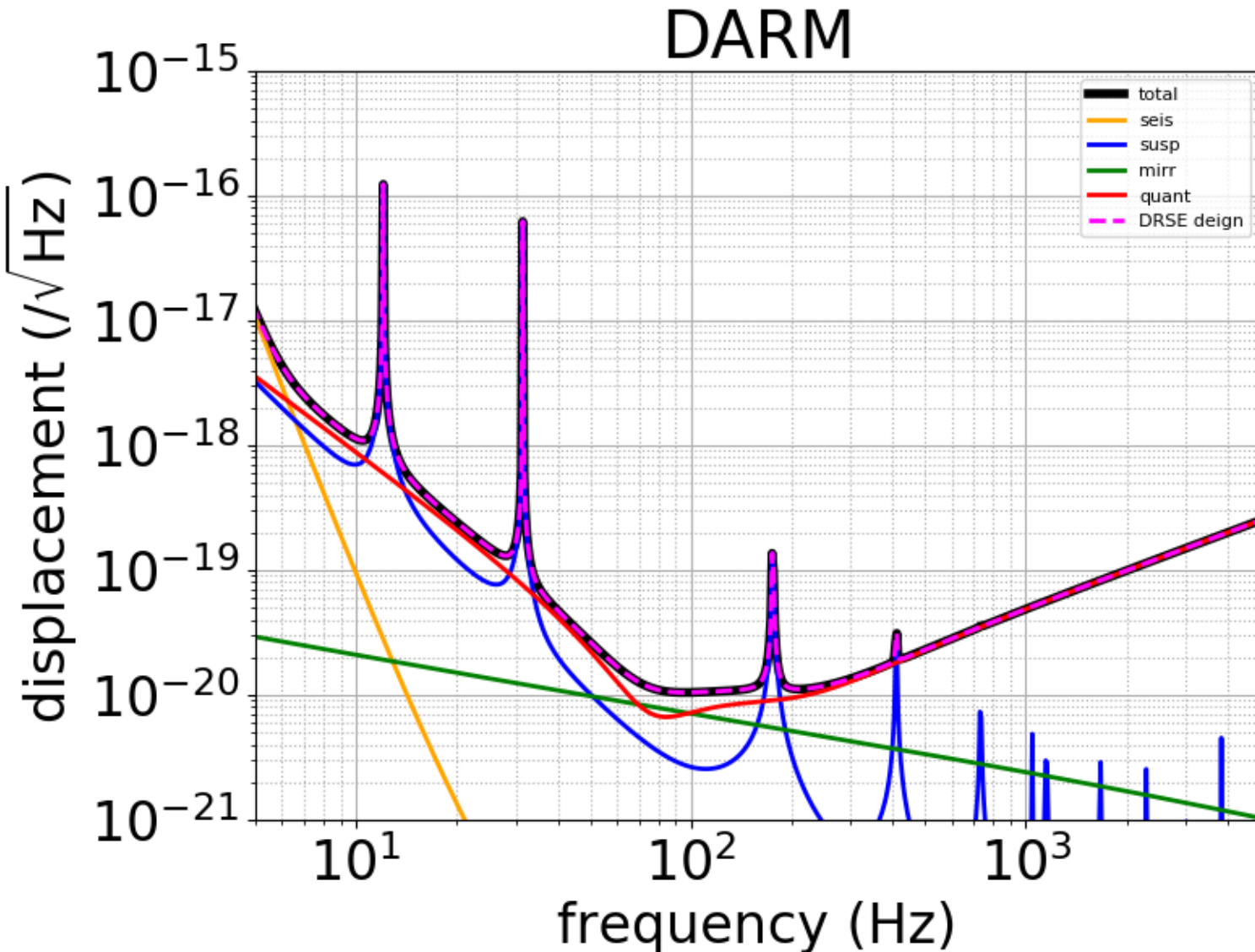


# Mirrors Summary



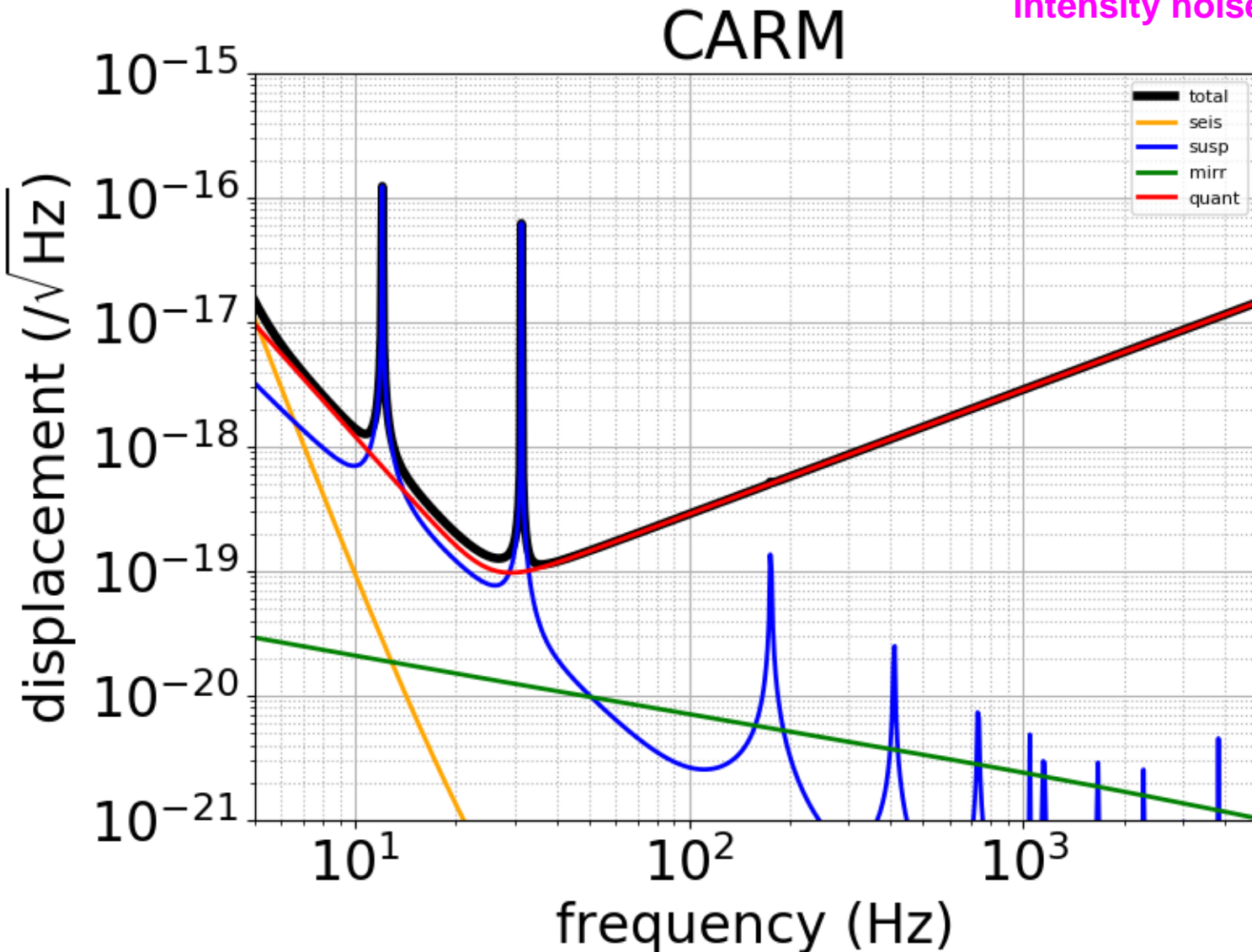


# Displacement Sensitivity: DARM

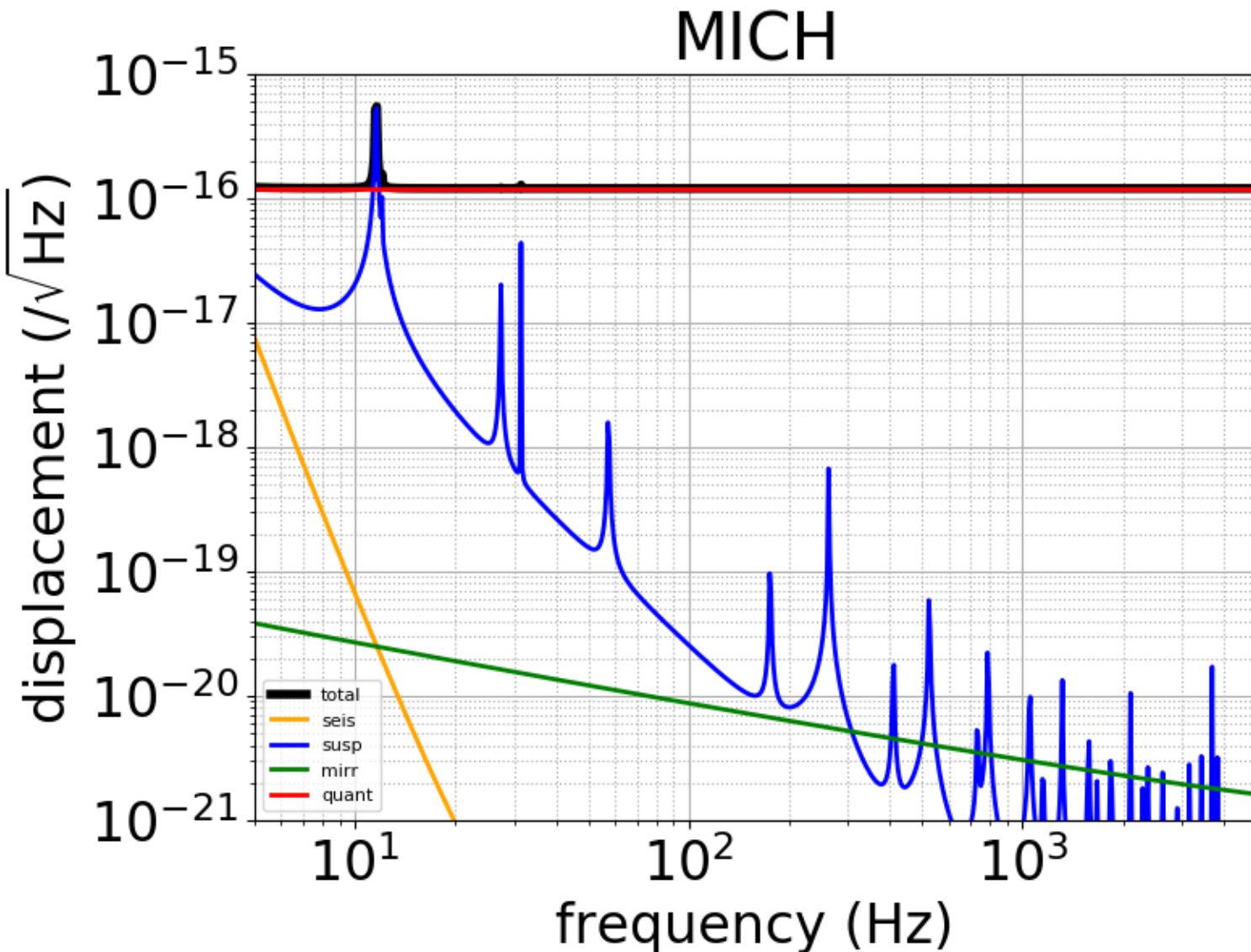


# Displacement Sensitivity: CARM

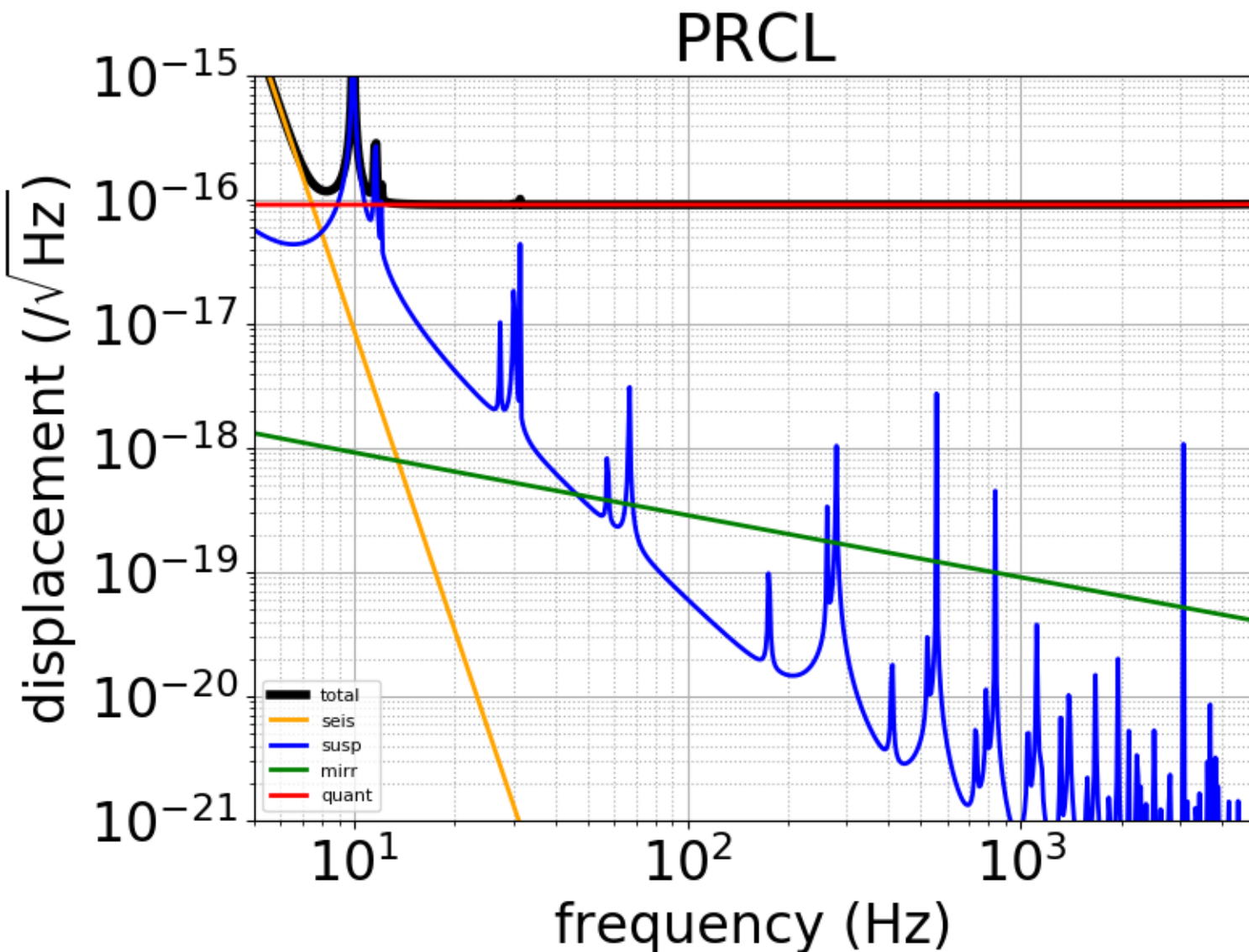
NOTE: frequency noise and intensity noise not considered



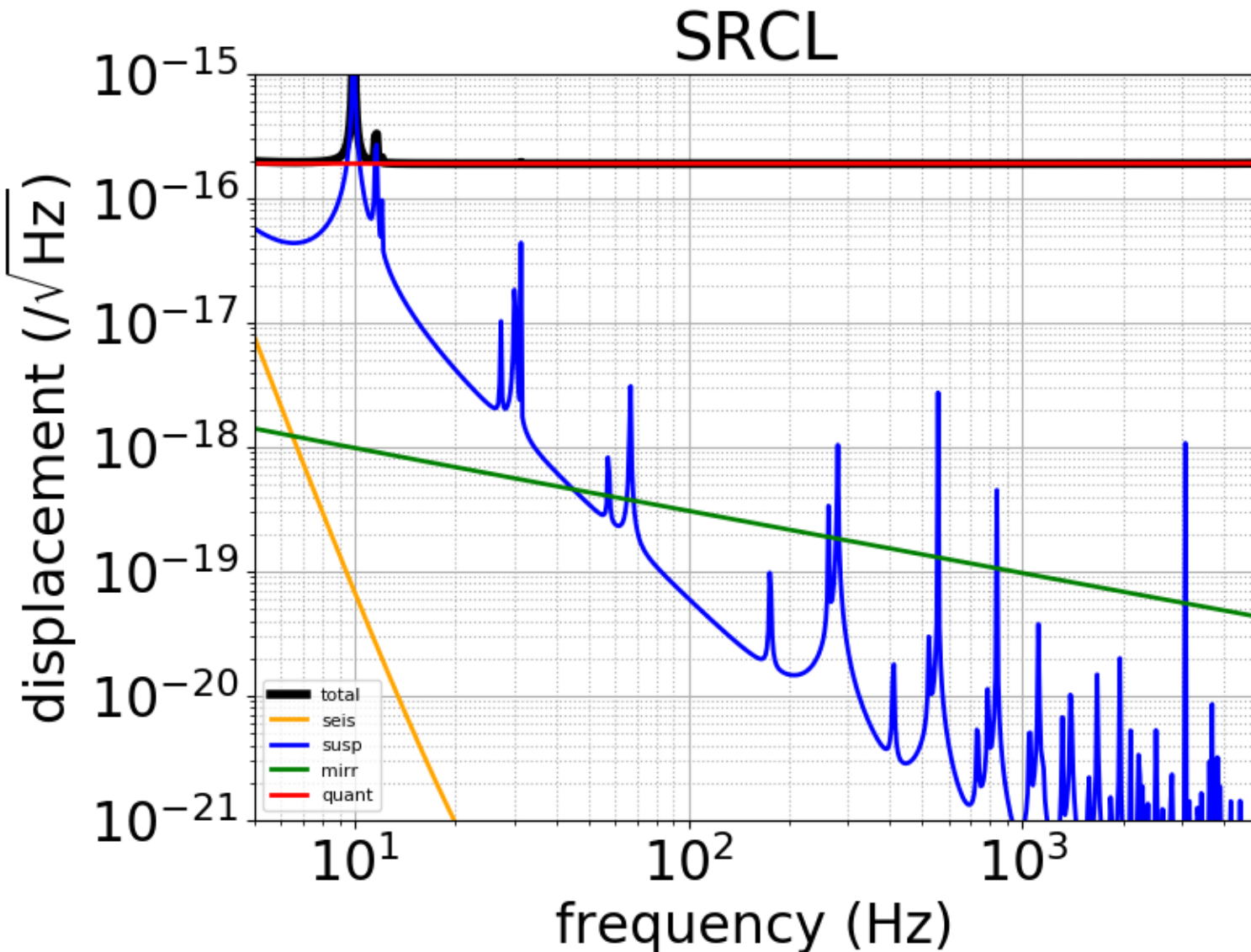
# Displacement Sensitivity: MICH



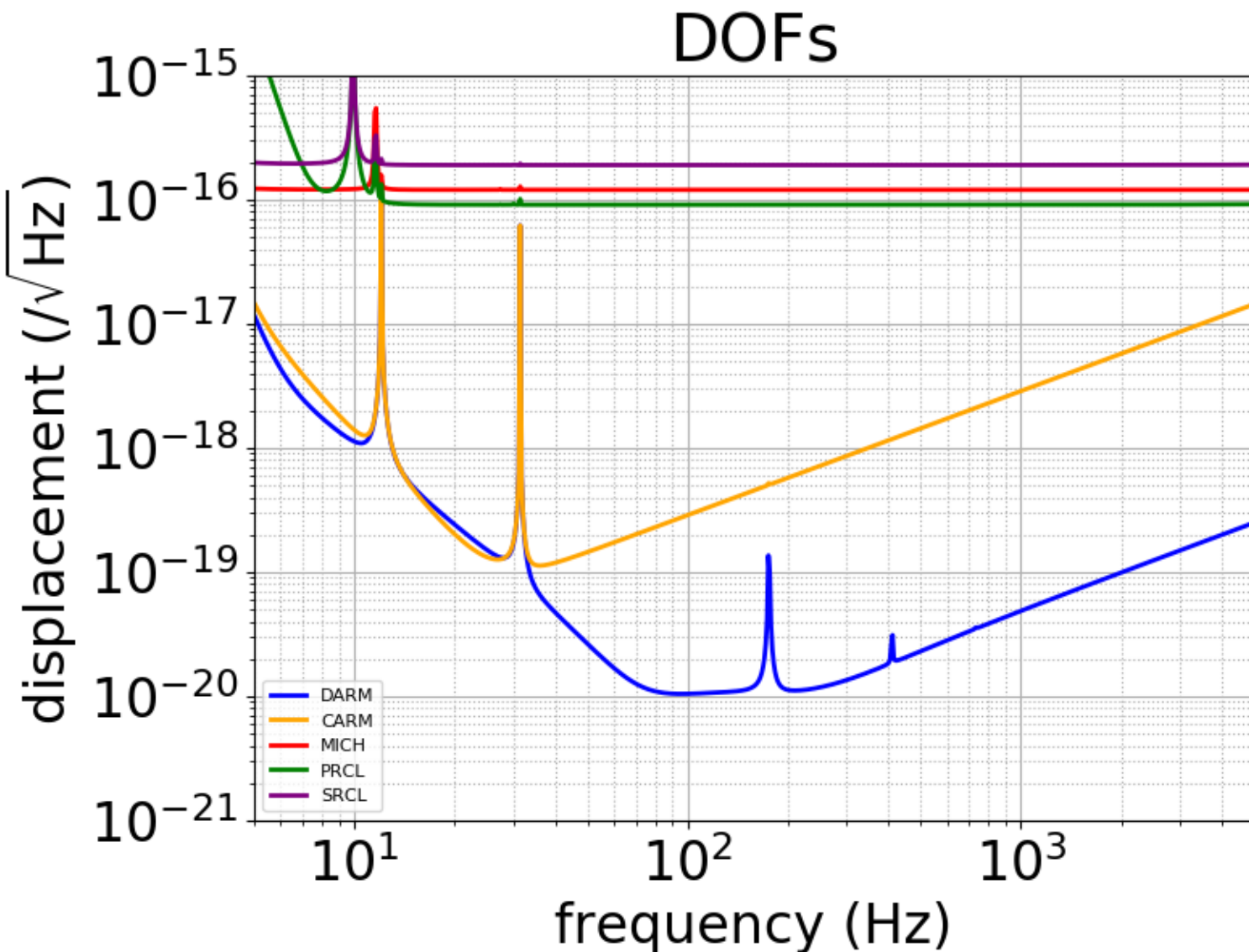
# Displacement Sensitivity: PRCL



# Displacement Sensitivity: SRCL



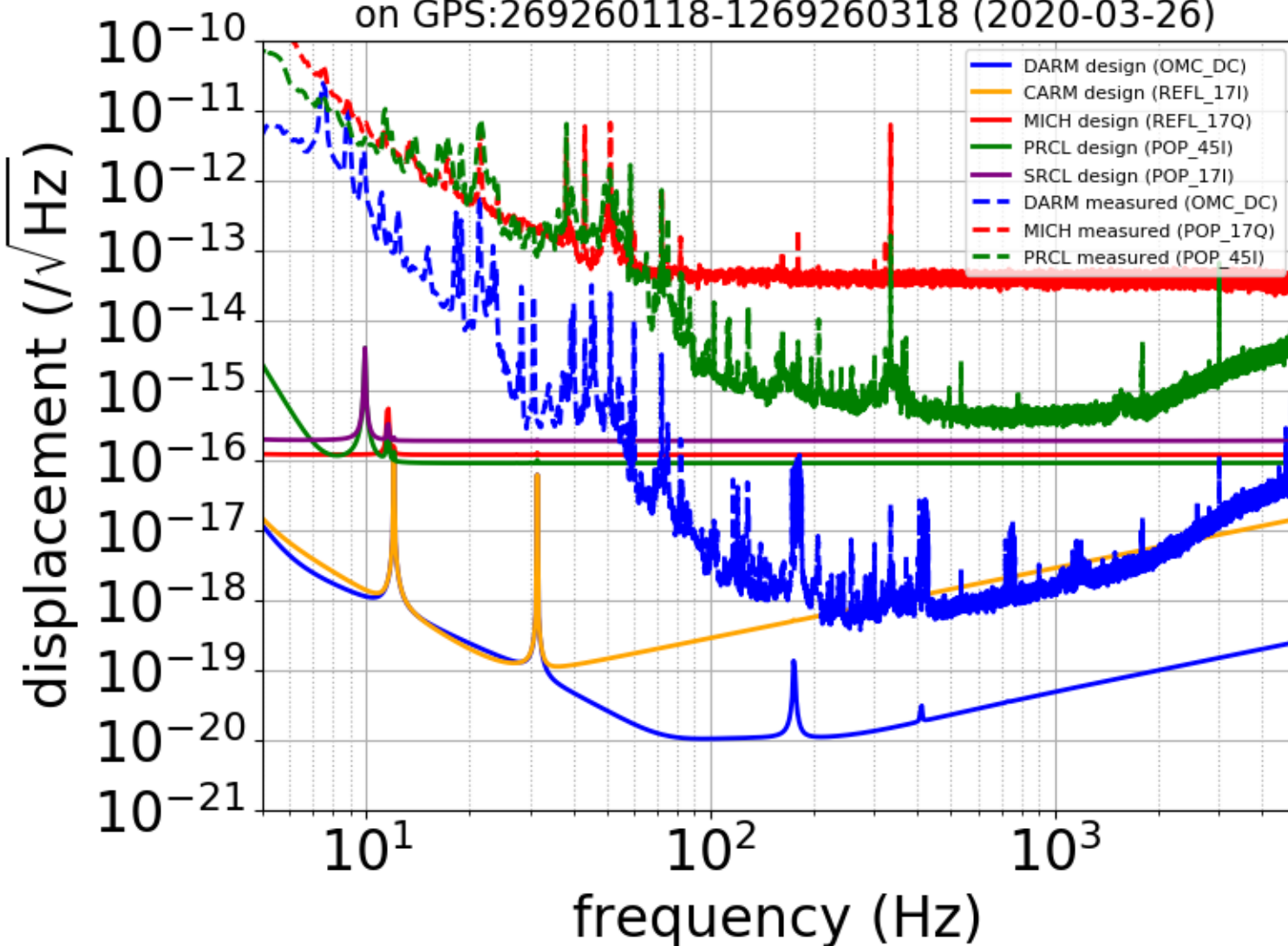
# Displacement Sensitivity Summary



NOTE: frequency noise and intensity noise not considered for CARM

# Mar 26, 2020 Sensitivity

Designed vs measured sensitivity  
on GPS:269260118-1269260318 (2020-03-26)



MICH and PRCL calibrated offline (see [klog #14556](#))