Improving the sensitivity of KAGRA gravitational wave detector

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Cryogenic cooling of test mass mirrors adds more complexity to the sensitivity design of interferometric gravitational wave detectors. This is because the heat extraction design affects both suspension thermal noise and quantum noise [1]. Here, we present the prospects for improving the sensitivity of KAGRA from O3 to O5. We show that it is likely that binary neutron star range of KAGRA will be only a few Mpc in O3 and about 80 Mpc in O4 at most optimistic cases, with current birefringent sapphire input test masses. We also show that the sensitivity can be improved upto 180 Mpc in O5, with improved test masses and frequency dependent squeezing, without increasing the inout laser power from the originally designed value. Detector parameters critical for the sensitivity calculation are also explained.

Designed Sensitivity

KAGRA has smaller coating thermal noise than other detectors owing to cryogenic \mathbb{P} . cooling, but has larger suspension thermal noise due to thick and short suspension fibers to extract heat from test mass mirrors. Reducing or increasing the input laser power improves the sensitivity in low or high frequency bands [2].

IMC TRANS

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arXiv:1906.02866

[3] KAGRA Collab.,

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arXiv:1909.12033

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PRD 97, 122003 (2018)

PTEP 2018, 013F01 (2018)

CQG 36, 165008 (2019)

PRD 97, 102001 (2018)

PRD 93, 082004 (2016)

150 Mpc in BNS 10^{-21} range with detuned configuration 10⁻²²± 7 10⁻²³ ★ 10^{-24} 10¹ 10^2 10^{3} frequency (Hz)

Arm cavity parameters gives bandwidth of quantum noise

- ITM transmission: 0.4 %

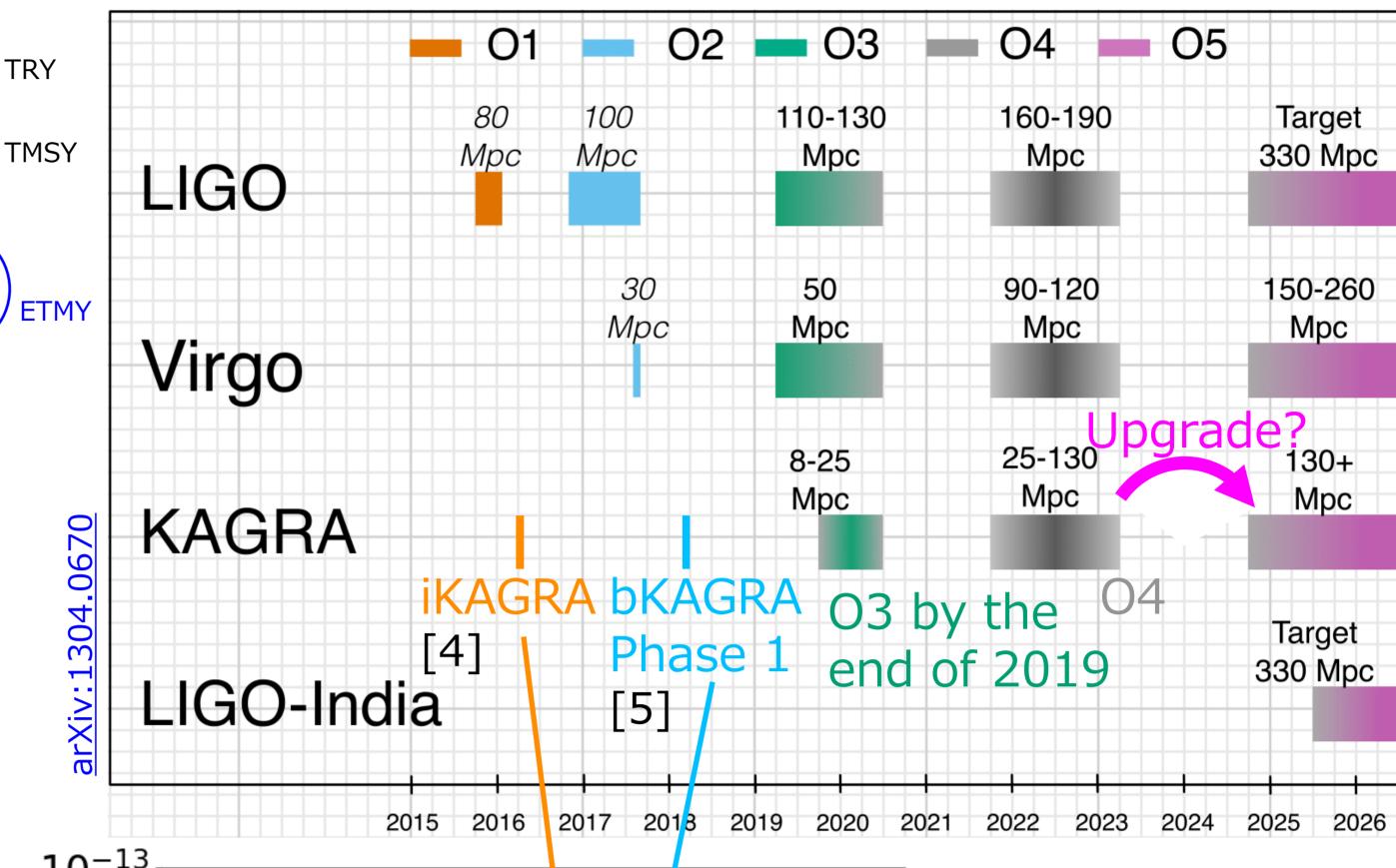
- Finesse: 1530

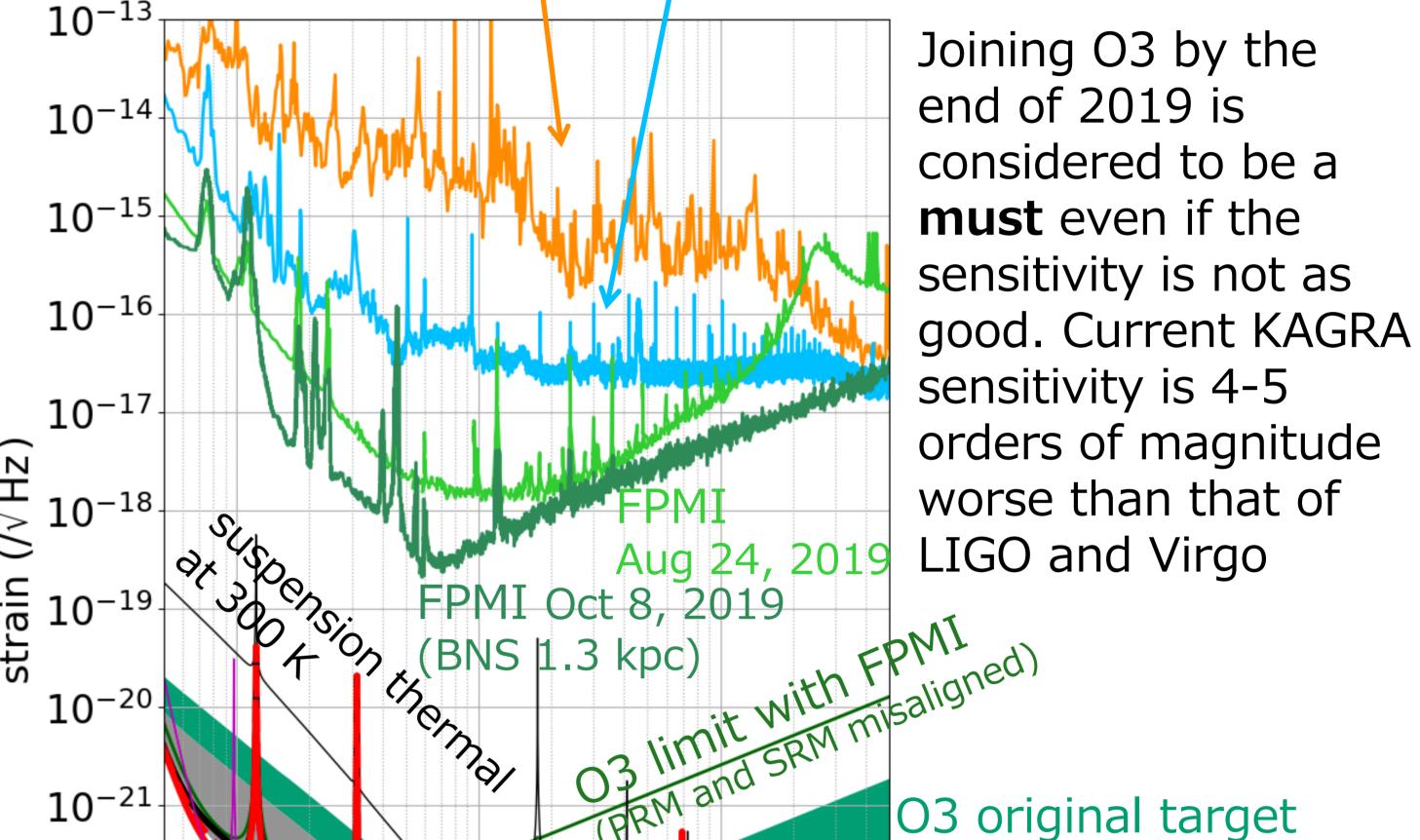
Mirror Birefringence Further Reading

Unexpectedly large and inhomogeneous birefringence of sapphire input test masses (ITMs) was found. Birefringence creates unwanted polarization in the reflection of ITMs. The optical losses are as high as several %, and power and signal recycling cavities cannot be locked stably until now.

Shape of unwanted polarization component of reflected beam from X-arm

Observing Scenario





O4 original target 10-22+ 10⁻²³ O4 limit with DRFPMI (BNS ~80 Mpc; with optical 10^{-24} losses in power and signal 10^3 10^2 10^{1} recycling cavities) frequency (Hz) O5 plan with mirrors replaced

Significant vertical thermal noise comes from blade springs and CuBe fibers suspending the intermediate mass (IM)

- Blade spring resonance: 14.5 Hz vertical

2 kHz horizontal (lower the better)

- Blade spring loss angle: 7e-7

- CuBe fiber loss angle: 5e-6

- IM temperature: 16 K

60 m filter cavity assumed) Blade spring CuBe fiber bounce Horizontal Vertical suspension Ref. [6] 10⁻²⁶ thermal

and frequency dependent

squeezing (BNS ~180 Mpc;

X-arm cavity

IMC REFL

IMMT1

Increasing input laser power reduces quantum noise at high frequencies but increases at low frequencies.

- Power at BS:

1 W for O3 due to no power recycling? 200 W for O4 due to reduced recycling gain from birefringence? 673 W for O5?

Signal recycling cavity parameters changes the

will be injected from here to reduce quantum noise in broad

- Filter cavity length: 60 m in O5?

- Injected squeezing: 10 dB

band [7]

suspending the test mass is critical for suspension thermal noise and heat extraction calculations.

- length: 35 cm

- diameter:

1.6 mm in design, 1.4 mm for O5??

- loss angle: 2e-7

- thermal conductivity: 5800 W/m/K

Mirror parameters are critical for calculating coating and substrate thermal noises

Parameters for sapphire fibers

- size: 22 cm dia. 15 cm thick

- mass: 22.8 kg

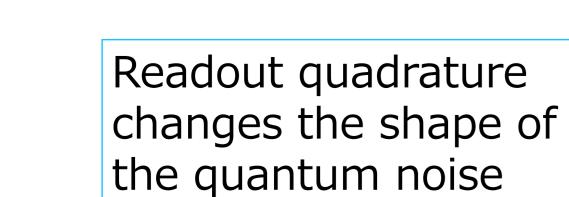
- temperature: 22 K

- loss angle: 1e-8

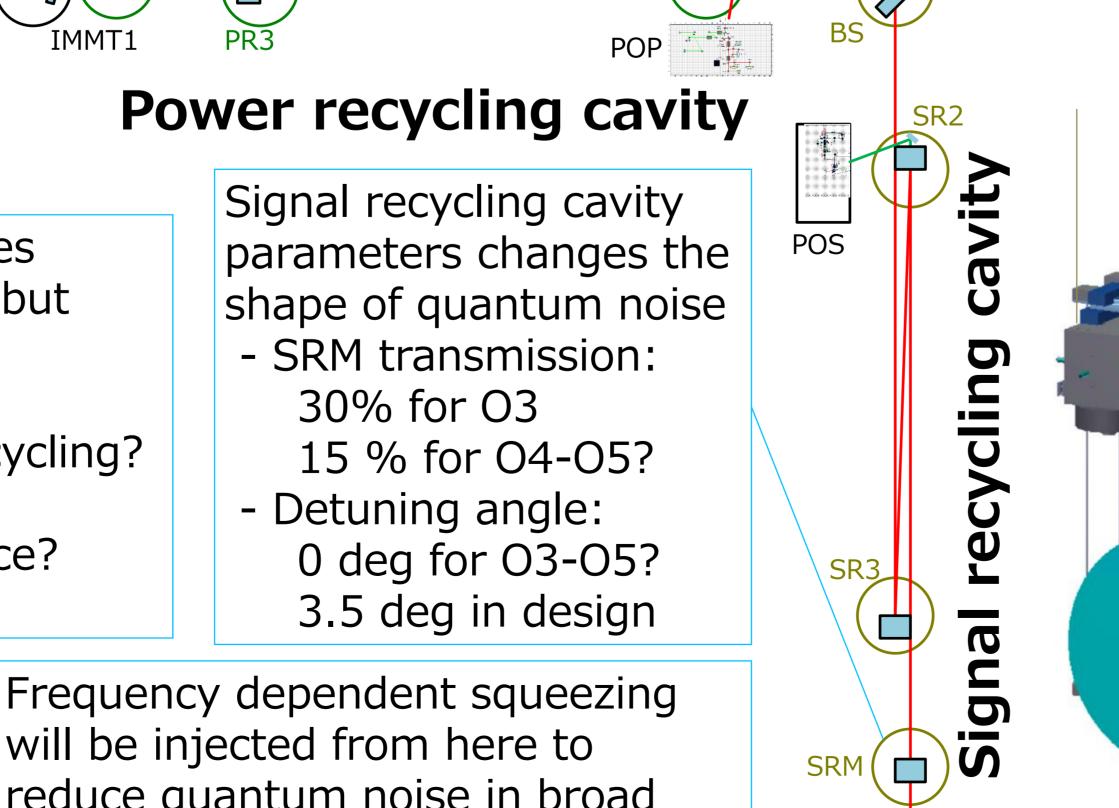
- substrate absorption: 50 ppm/cm in design

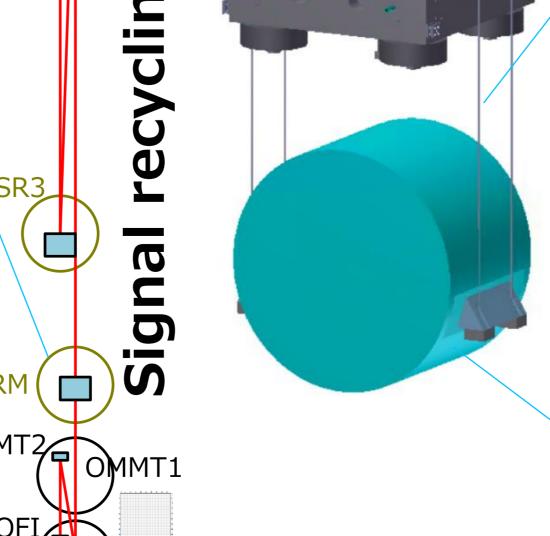
25 ppm/cm for 05??

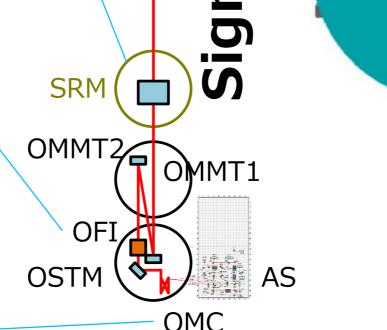
- coating loss angle: 3e-4 / 5e-4 - coating absorption: 0.5 ppm



- Homodyne angle: 90 deg for O3-O5? 135.1 deg in design







ITMY