

# On the effect of arm cavity finesse asymmetry to O3 sensitivity

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# Background

- Transmission measured to be  
ITMX: 0.444 % ITMY: 0.479% ([JGW-T1809173](#))
- So the asymmetry was 0.076 although MIF requirement was  $2 \cdot |(T1-T2)/(T1+T2)| < 0.01$  ([wiki](#))
- Arm cavity finesse recently measured to be  
Xarm 1440(10) at cryo 1411(2) at room temp.  
klog [9215](#), [9156](#), [9097](#), [9052](#), [9033](#), [9014](#), [8999](#) and [7307](#)  
Yarm 1300(20) at cryo  
klog [9211](#), [9169](#), [9052](#), [9047](#), [9040](#), [9023](#), [9014](#), [8995](#)
- ITMs also have inhomogeneity issues as studied in, for example, [JGW-G1909955](#)

# Finesse and ITM transmission

- Xarm 1440(10) [1411(2)] means  
ITMX transmission + losses = 0.436(3) %  
0.444 % according to [JGW-T1809173](#) [0.445(1) %]
- Yarm 1300(20) means  
ITMY transmission + losses = 0.483(7) %  
0.479 % according to [JGW-T1809173](#)
- Yarm sounds reasonable but Xarm finesse seems to be too high
  - could be due to finesse measurement at cryogenic temperatures
  - could be due to some systematic errors

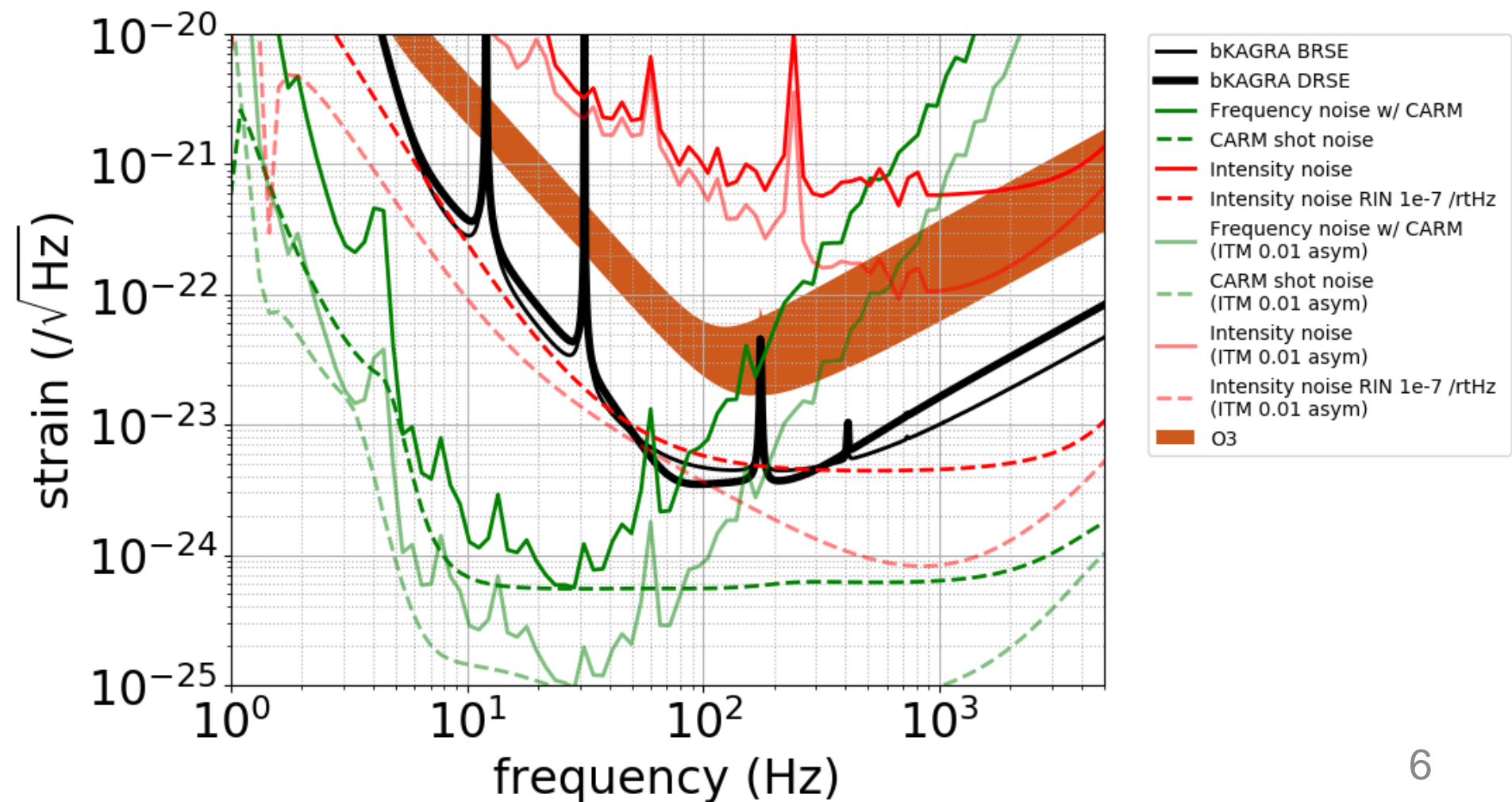
# Effects of Finesse Asymmetry

- Larger laser frequency noise
  - Larger laser intensity noise
  - These effects are presented below
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- Note that these effects will be even larger with ITM inhomogeneity
  - With ITM inhomogeneity, shot noise will be worse due to larger HOMs but the effect would be small (~14 % increase according to [JGW-G1909955](#))

# Method for Calculations

- Simulate frequency/intensity noise coupling with Optickle ([JGW-T1910341](#))
  - Note that it gives transfer function from laser frequency noise **without** CARM suppression to strain sensitivity (CARM openloop gain assumed)
  - Used power at BS 10 W, ITMX 0.44% ITMY 0.479 % case (ITMX 0.44% ITMY 0.4445% as comparison)
- Multiply the coupling factor to frequency noise and intensity noise of IMC transmitted beam
  - frequency noise: 1 Hz/rtHz @ 100 Hz ([klog #9291](#))
  - intensity noise:  $2e-5$  /rtHz @ 100 Hz **without** intensity stabilization ([klog #9259](#))

# Result

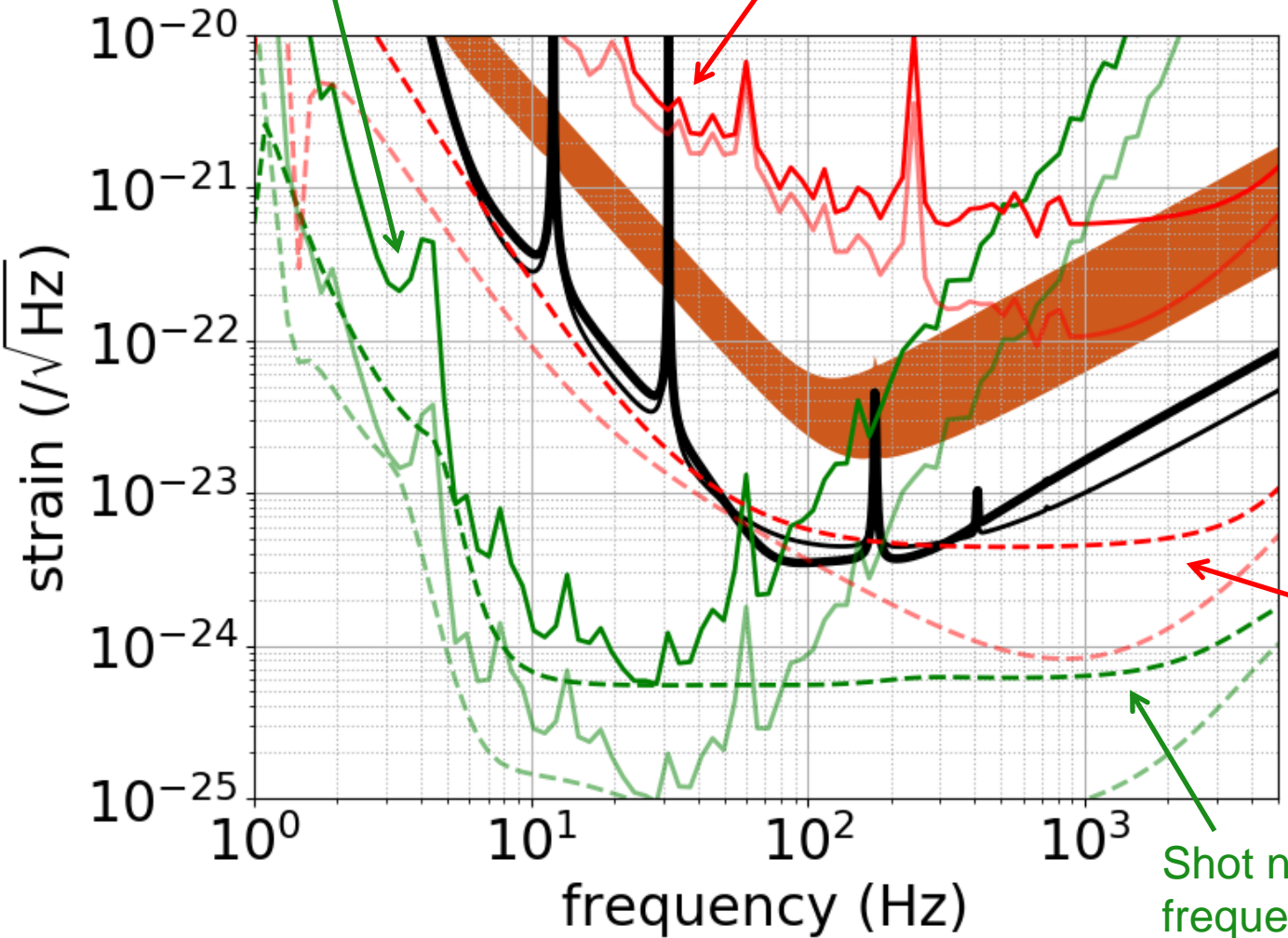


Frequency noise coupling estimated with current measured frequency noise; CARM loop turned on (could be limited by measurement noise at high frequencies)

# Result

Intensity noise coupling estimated with current measured intensity noise (stabilization servo not on yet)

Dim lines represent same curves when ITM transmission asymmetry was 0.01



- bKAGRA BRSE
- bKAGRA DRSE
- Frequency noise w/ CARM
- - CARM shot noise
- Intensity noise
- - Intensity noise RIN 1e-7 /rtHz
- Frequency noise w/ CARM (ITM 0.01 asym)
- - CARM shot noise (ITM 0.01 asym)
- Intensity noise (ITM 0.01 asym)
- - Intensity noise RIN 1e-7 /rtHz (ITM 0.01 asym)
- O3

Intensity noise coupling when RIN = 1e-7 /rtHz (as was the case in klog #7177)

Shot noise limit of frequency noise stabilization

# Implications for O3

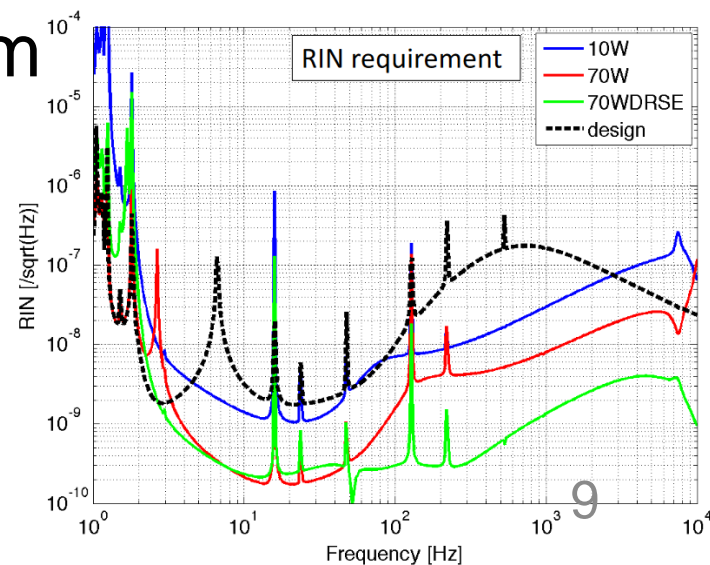
- Current frequency noise and intensity noise do not meet the requirement
- The situation don't change much even if ITM transmission asymmetry was 0.01
- As for the frequency noise, we should identify the noise at high frequencies
- As for the intensity noise, we should wait for intensity stabilization result. If relative intensity noise reaches  $1e-7$  /rtHz, intensity noise won't be a problem.



# Implications for O4 (designed sensitivity)

- Frequency noise seem to be OK with ITM transmission asymmetry if frequency stabilization servo work fine (if frequency noise reach CARM shot noise limit)
- But frequency noise is probably not OK considering ITM inhomogeneity (requirement will be an order of magnitude tougher at ~kHz)
- Intensity noise will be a problem since RIN requirement will be  $\sim 2e-10 / \sqrt{\text{rtHz}}$  @ 10 Hz (with safety factor of 10)

[JGW-T1707565](#)



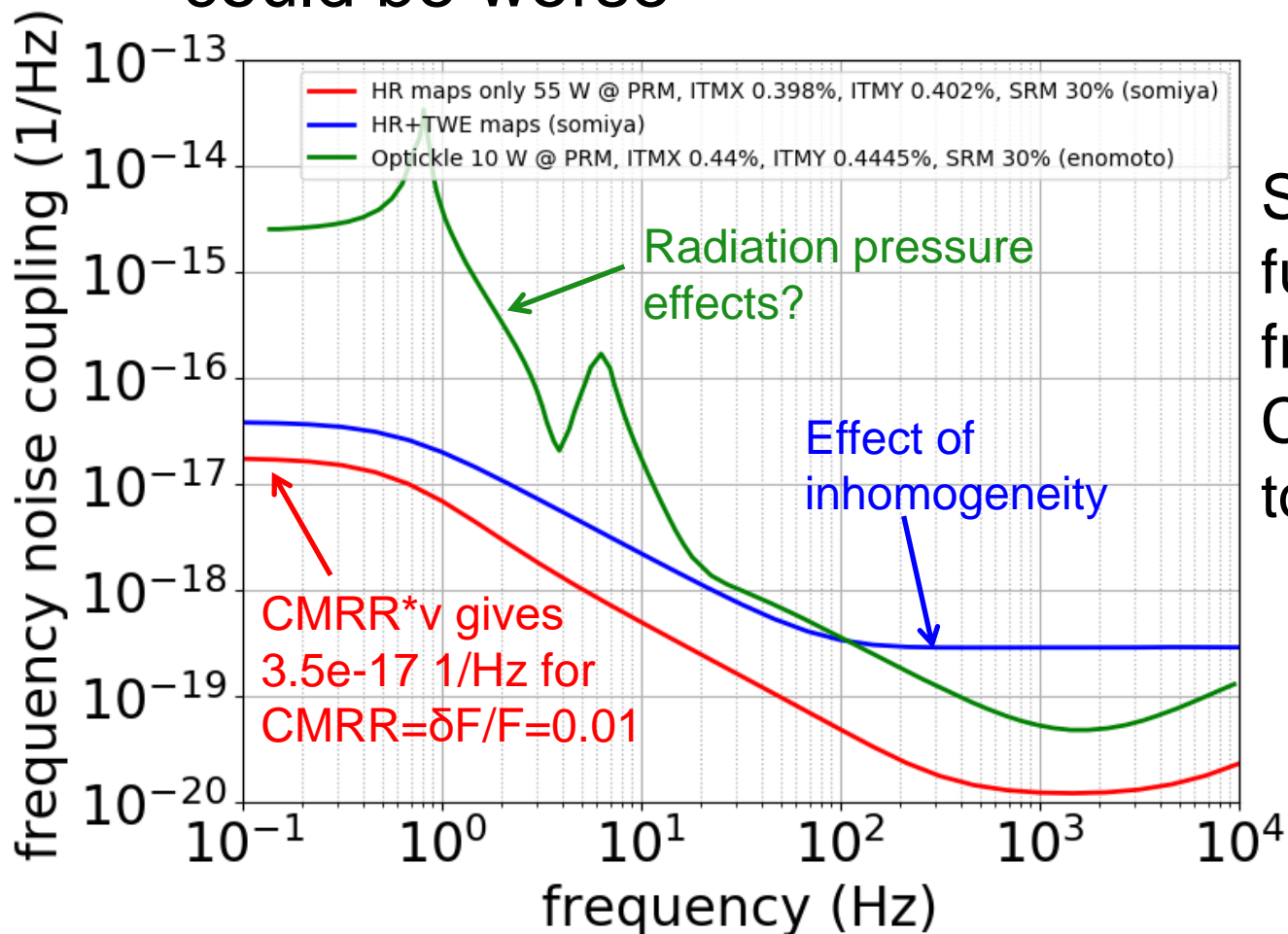
# Conclusions

- Measured arm cavity finesse asymmetry can be basically explained by ITM transmission asymmetry but we cannot say that ITM transmission asymmetry is the only reason
- We cannot say much if current finesse asymmetry is acceptable for O3 or not since frequency noise and intensity noise is bad at this moment.
- Frequency noise do not meet the O3 requirement at high frequencies. We should identify the noise at high frequencies and try to reduce it.
- Intensity noise without stabilization do not meet the O3 requirement. We need to wait for the stabilization result.
- This finesse asymmetry and ITM inhomogeneity will likely to be an issue for achieving the design sensitivity.

# Some More Details

# Optickle vs FINESSE

- Optickle calculation do not include ITM HR maps and inhomogeneity; Frequency noise coupling could be worse

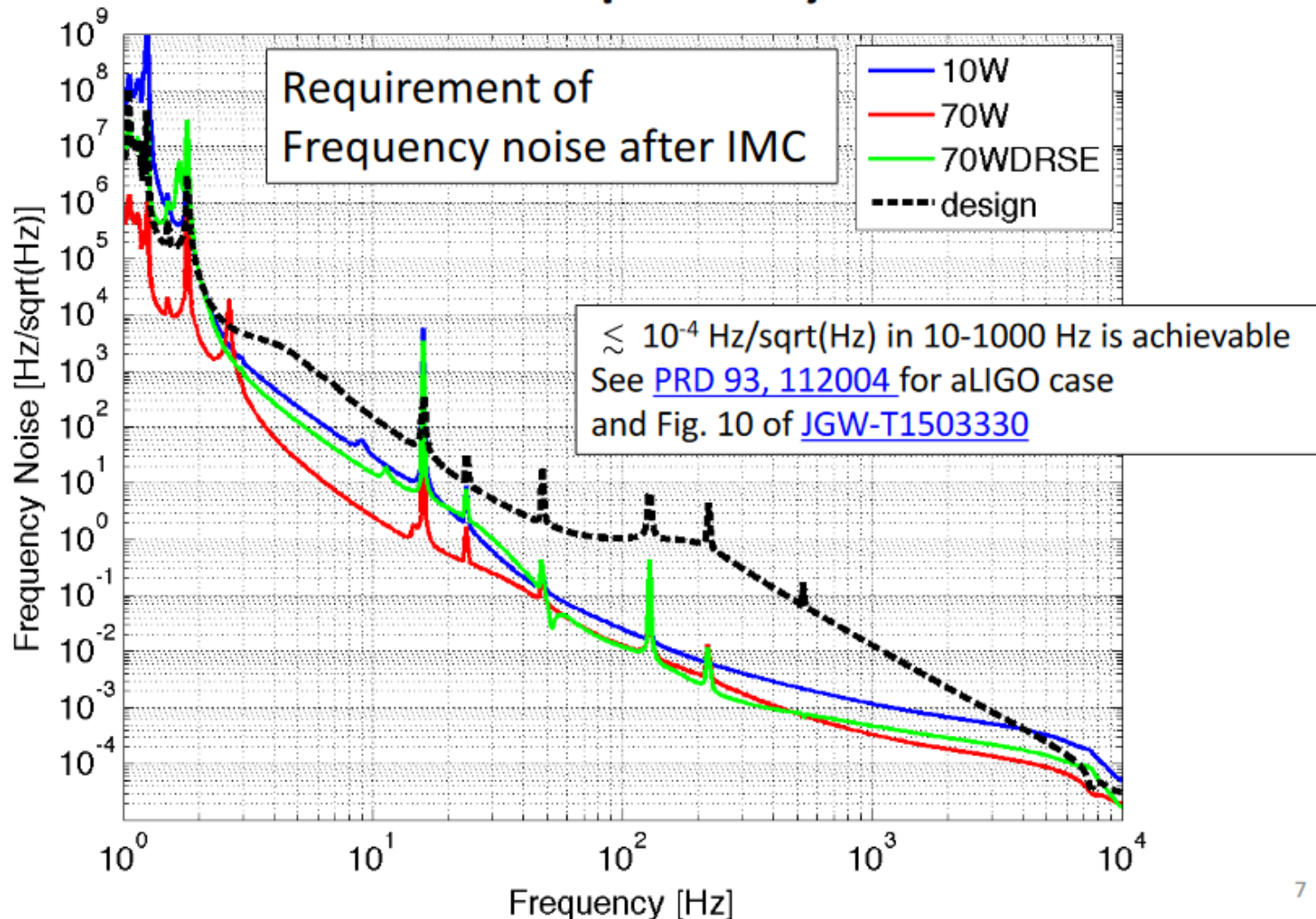


Simulated transfer functions from frequency noise **with** CARM suppression to strain sensitivity

# Frequency Noise Requirements

- See [JGW-T1707565](#) (ITM 0.4% and 0.5%, SRM 30%)

## Results: Frequency noise



# Frequency Noise Requirements

- Compared with measurements ([klog #9256](#))

## Results: Frequency noise

