Development of
Power Recycling Seismic Attenuation System for KAGRA

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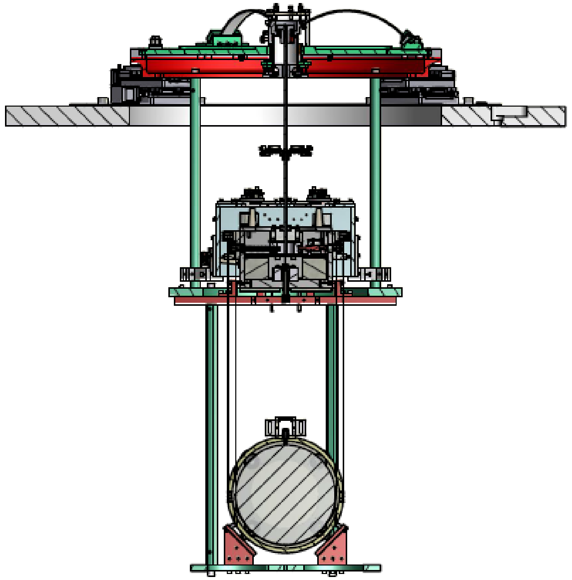
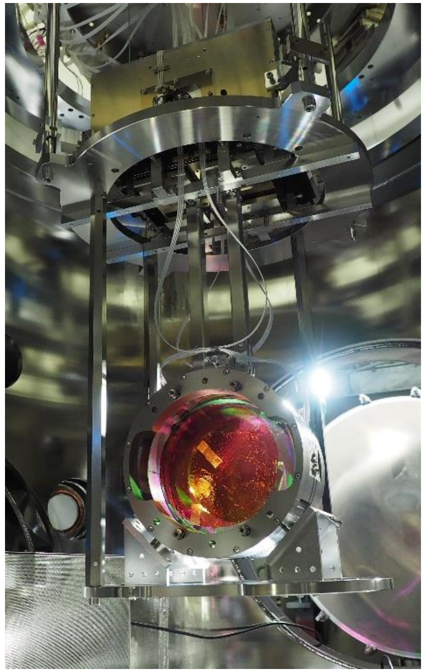
from VIS, NAOJ

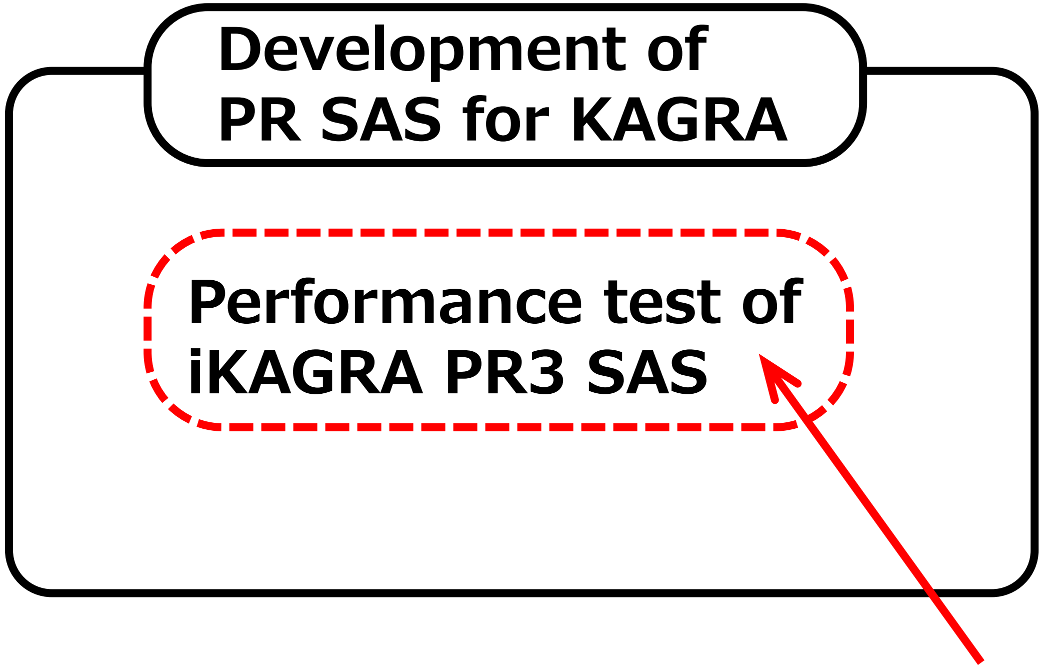




Contents

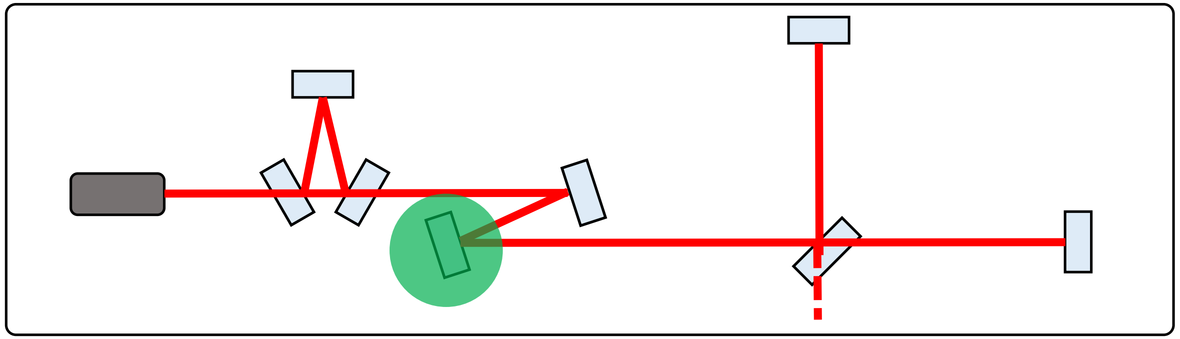
Performance test of iKAGRA PR3 SAS at Kamioka

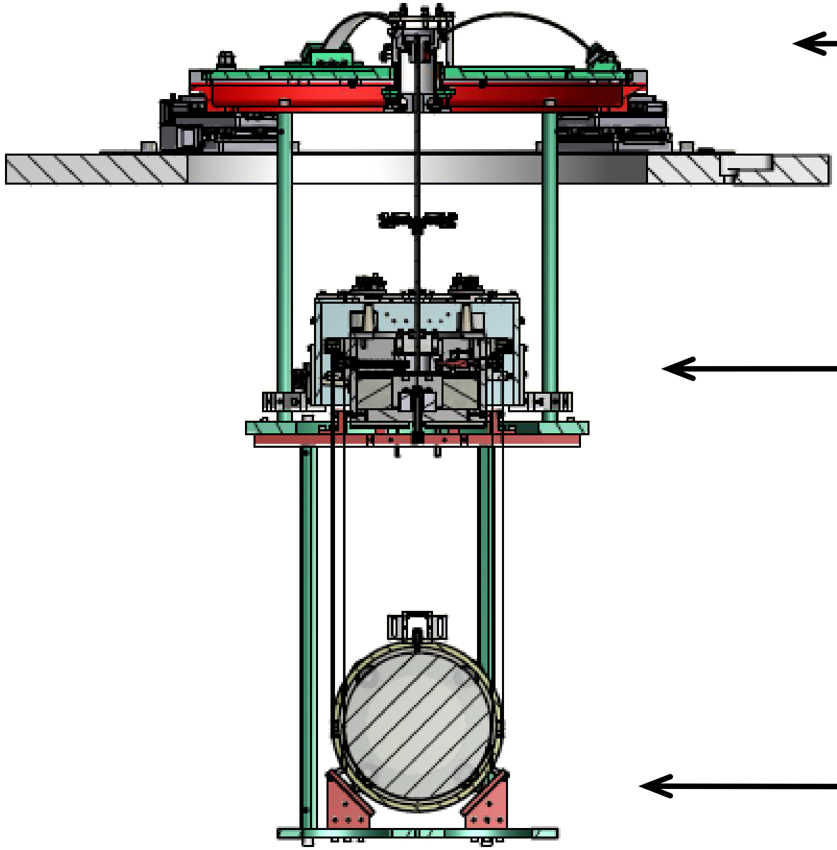
1. Introduction
2. Performance test
   2-1. Damping performance test
   2-2. Residual vibration
3. Summary



1. Introduction

iKAGRA PR3 SAS (= Type-Bpp SAS)





Bottom GAS filter (BF)

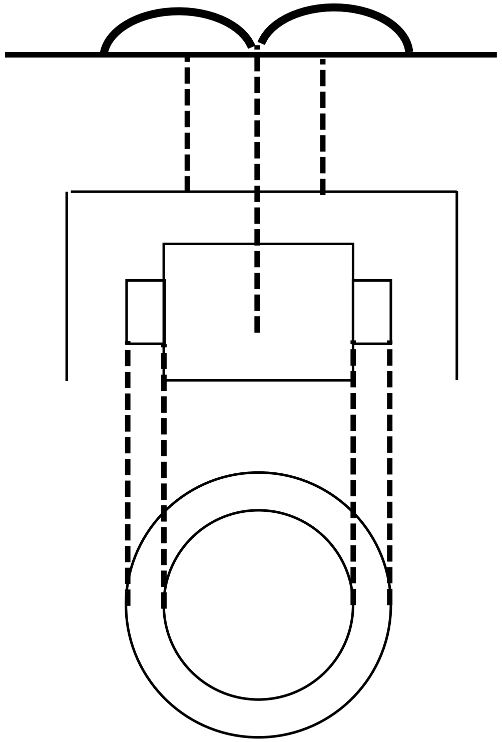
Traverser

Intermediate mass (IM)

Intermediate recoil mass (IR)

Test Mass (TM)

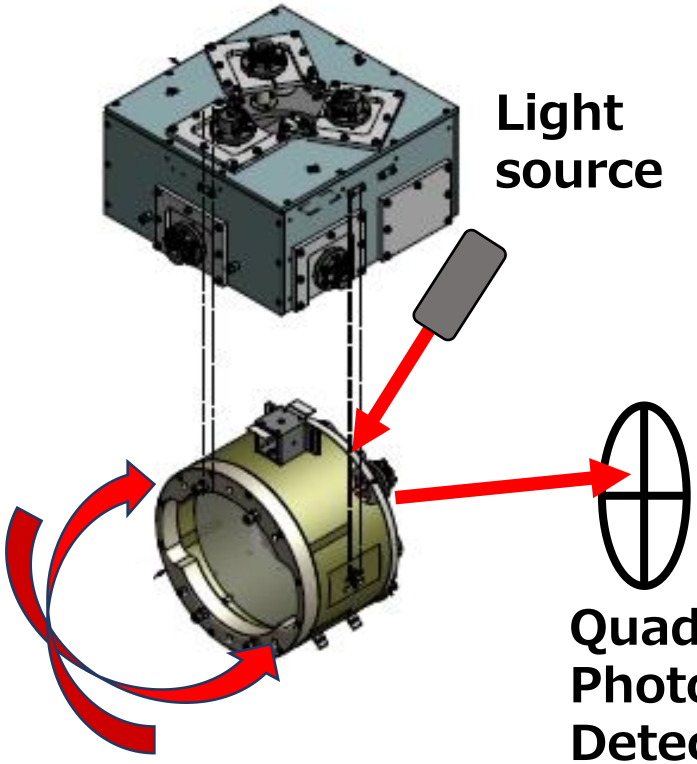
Recoil mass (RM)



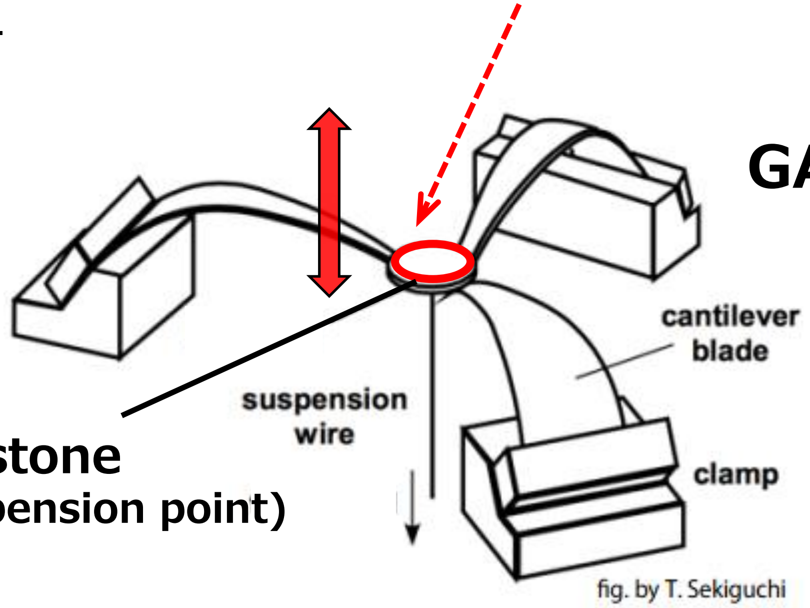
Sensors & actuators for active control (in iKAGRA)

Optical Lever (Oplev)

→ senses angular motion of the optic



Linear Variable Differential Transducer (LVDT)

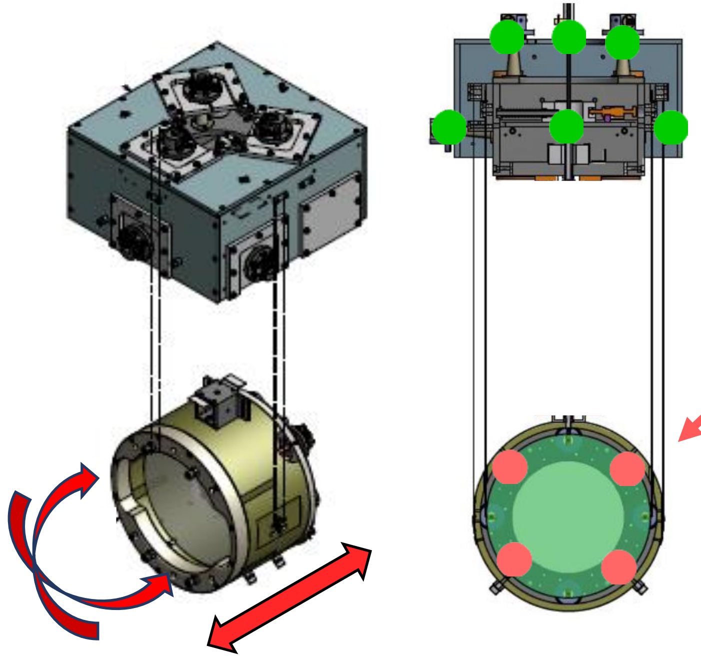


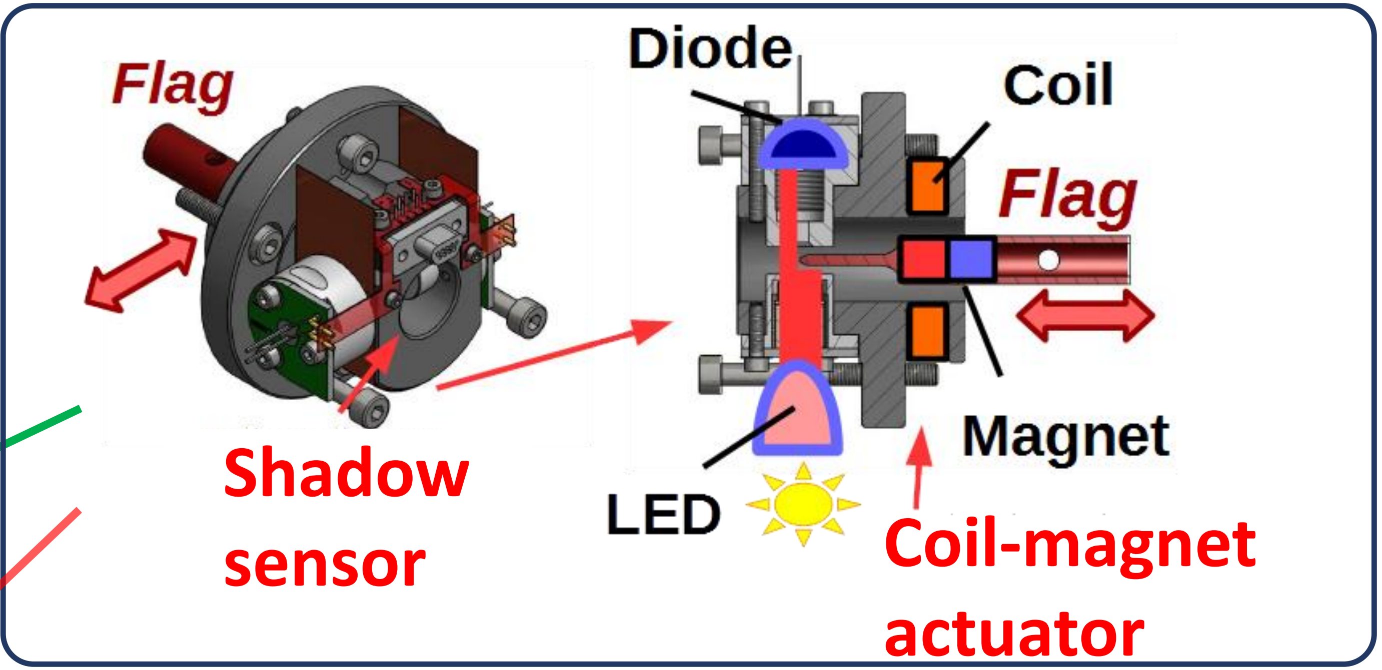
→ senses & actuates position of keystone

Sensors & actuators for active control (in iKAGRA)

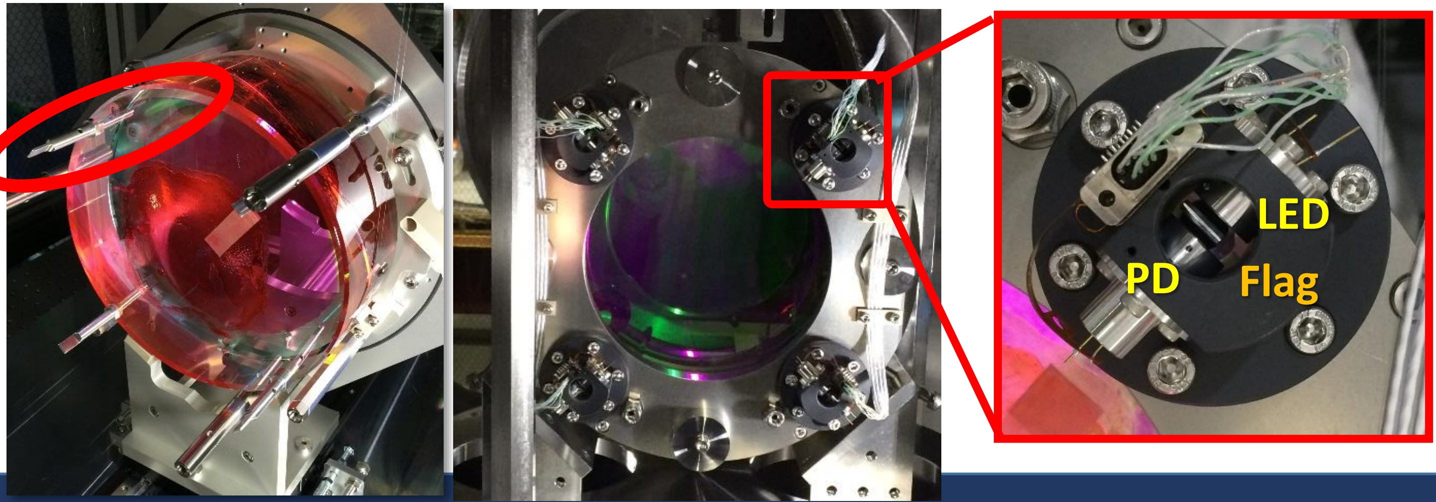
Optical Sensor and Electro-Magnetic actuator (OSEM)

→ senses & actuates relativemotion of mass and recoil mass





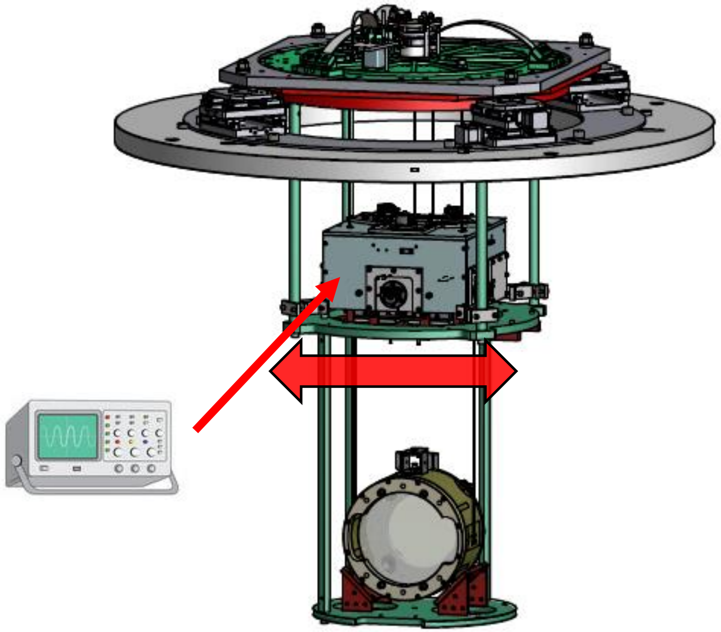
Flag

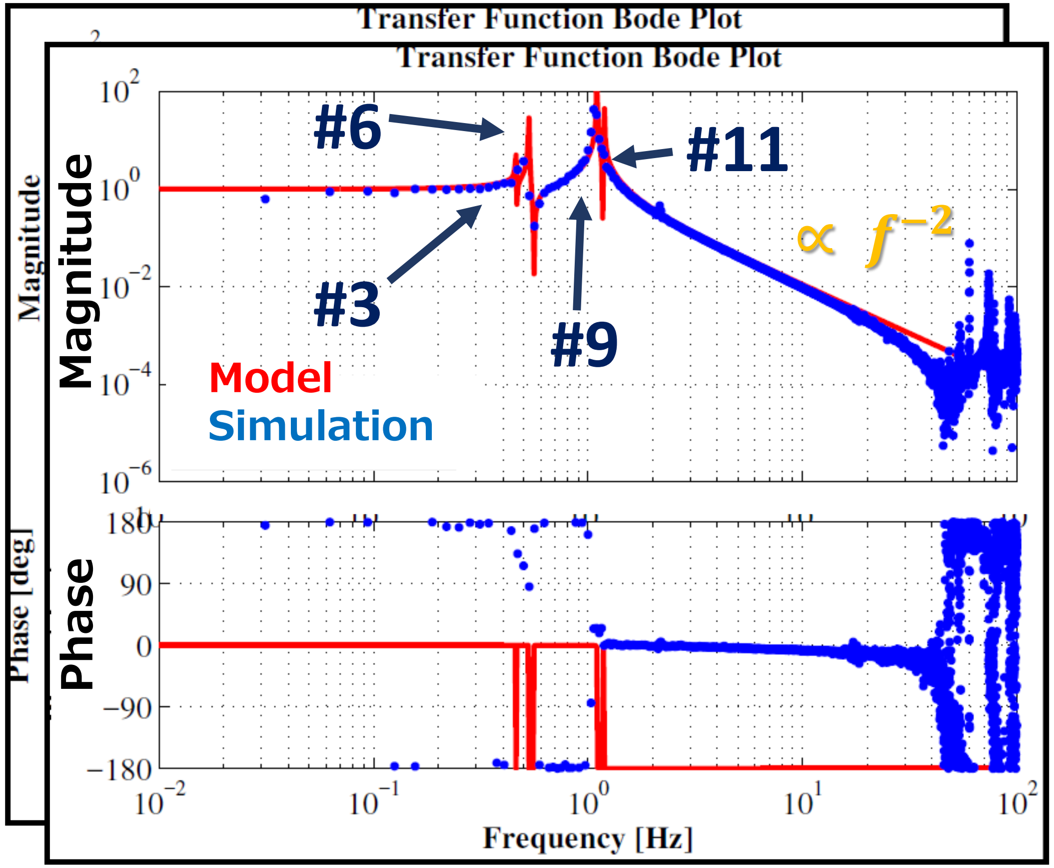


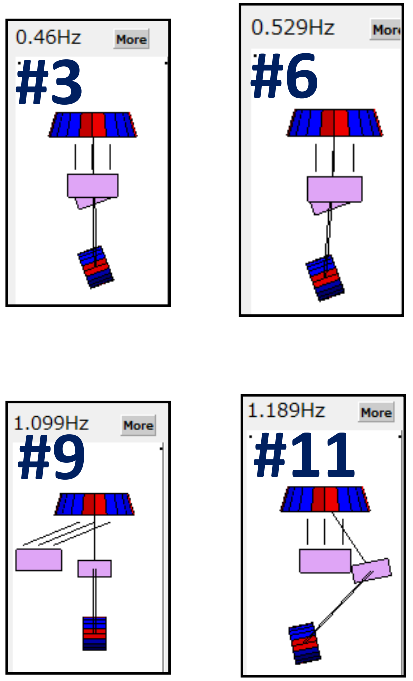
Assembly

October 2015 - February 2016 (test hanging & installation at Kamioka)

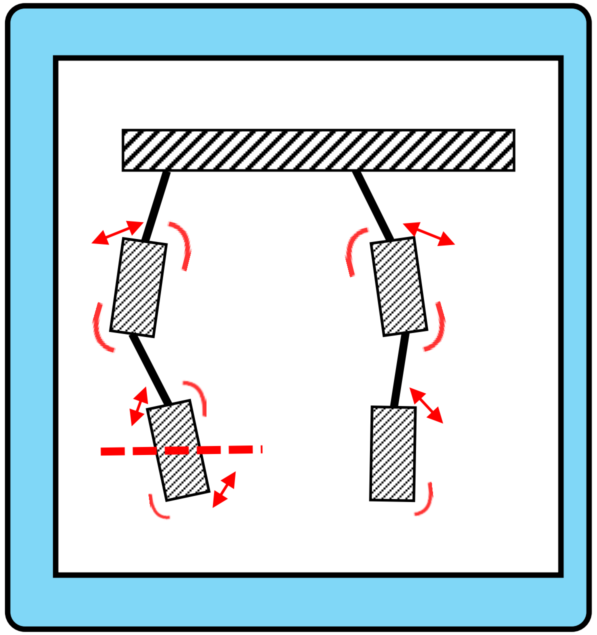
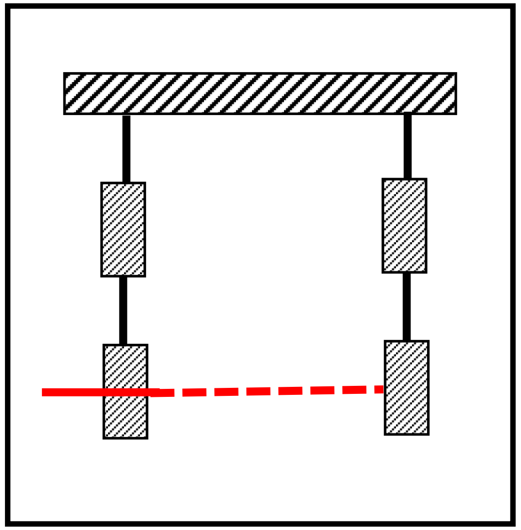
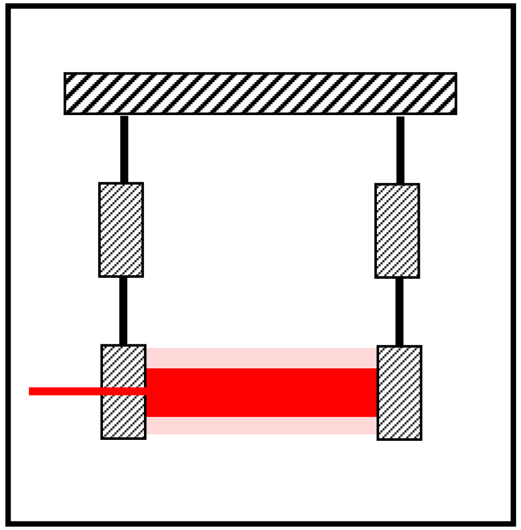
Frequency response is get along with the simulation?







2. Performance test (conducted in vacuum on 23-25, May, 2016)

Damping phase → **Lock acquisition phase** → **Observation phase**

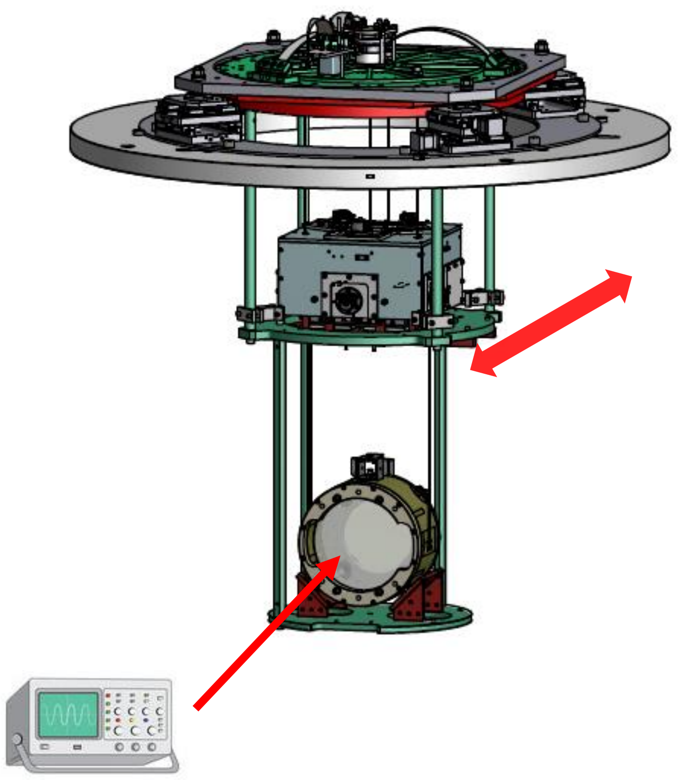
Suppress large disturbance

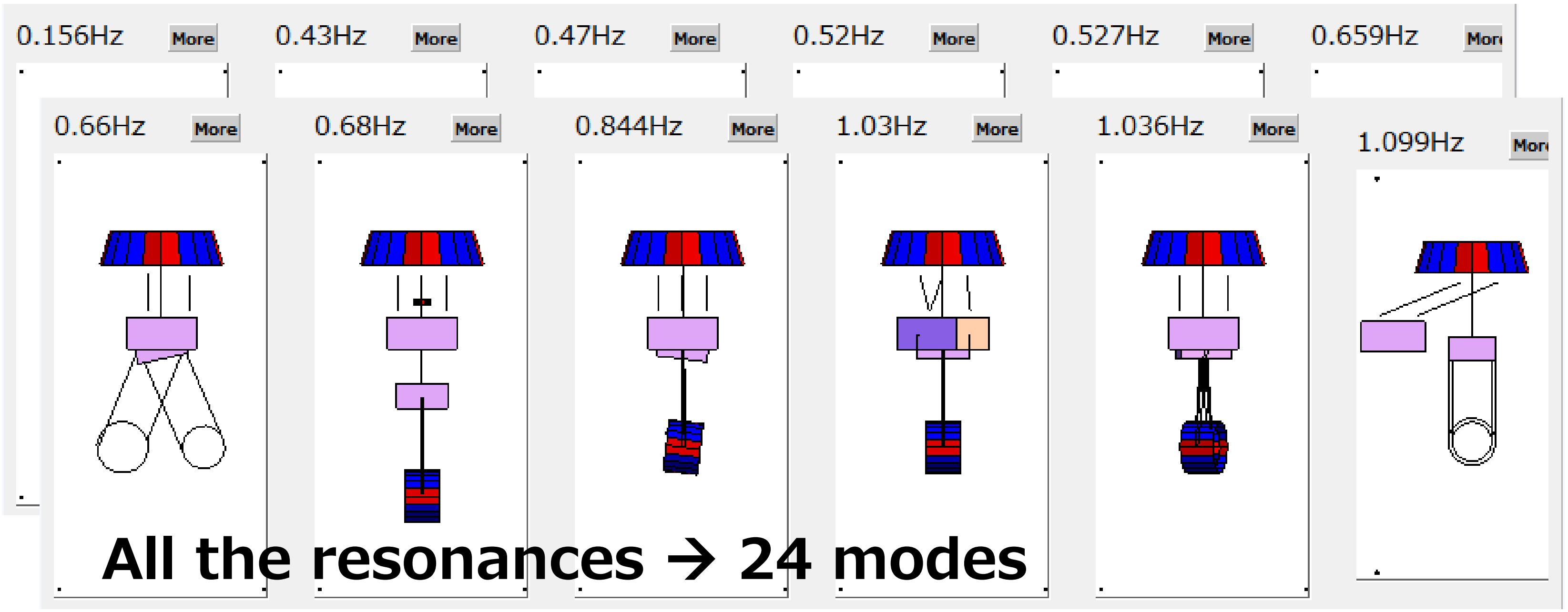
Manage lock-acq

Keep position with low noise control

2-1. Damping performance test

All the resonances can be damped within a short time with active control ?

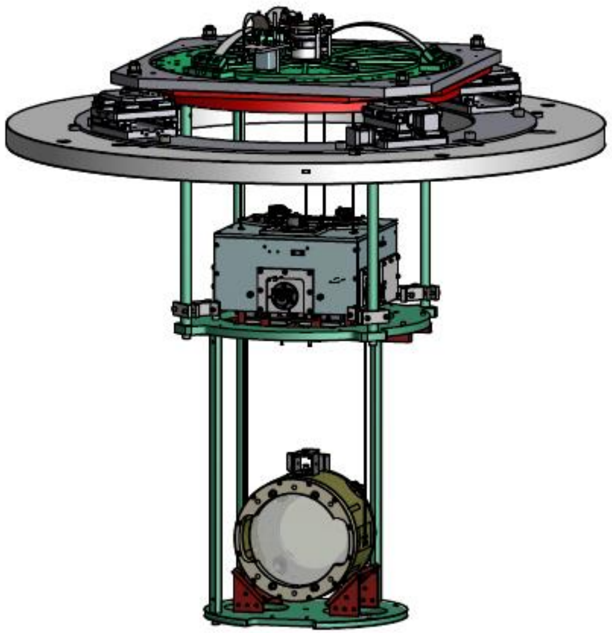


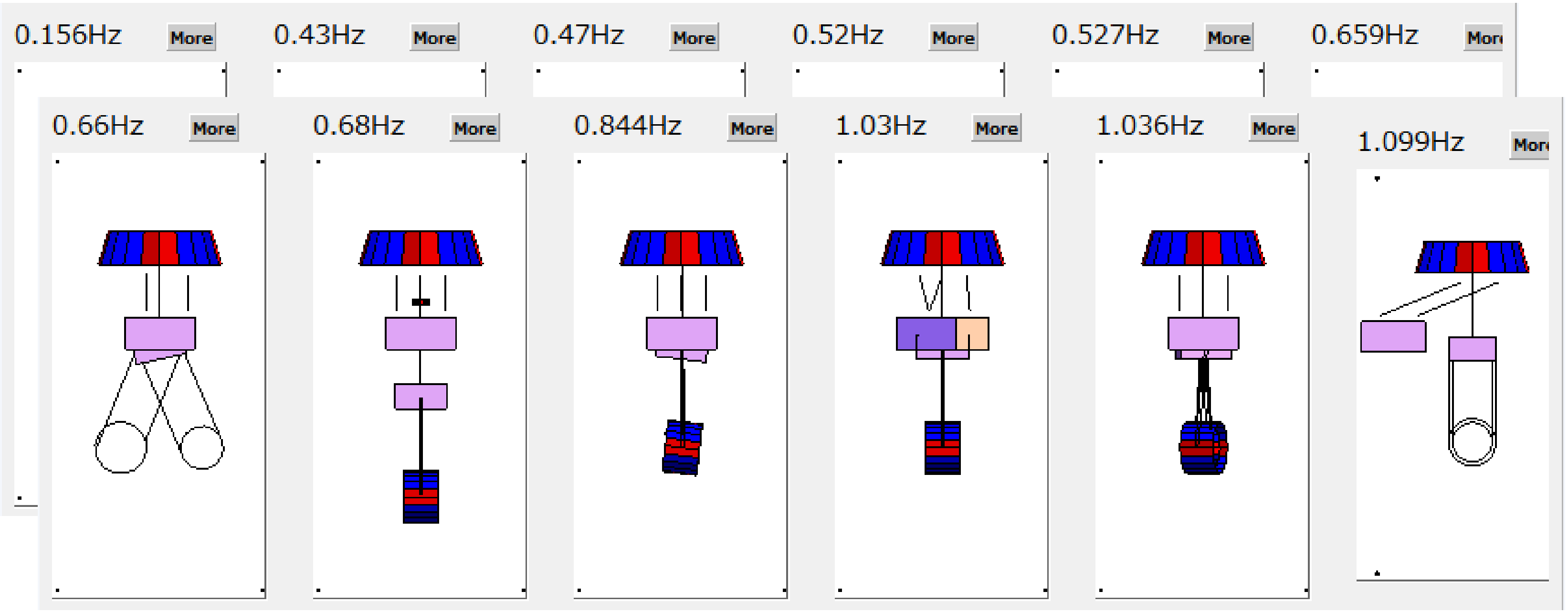


All the resonances → 24 modes

2-1. Damping performance test

All the resonances can be damped within a short time with active control ?

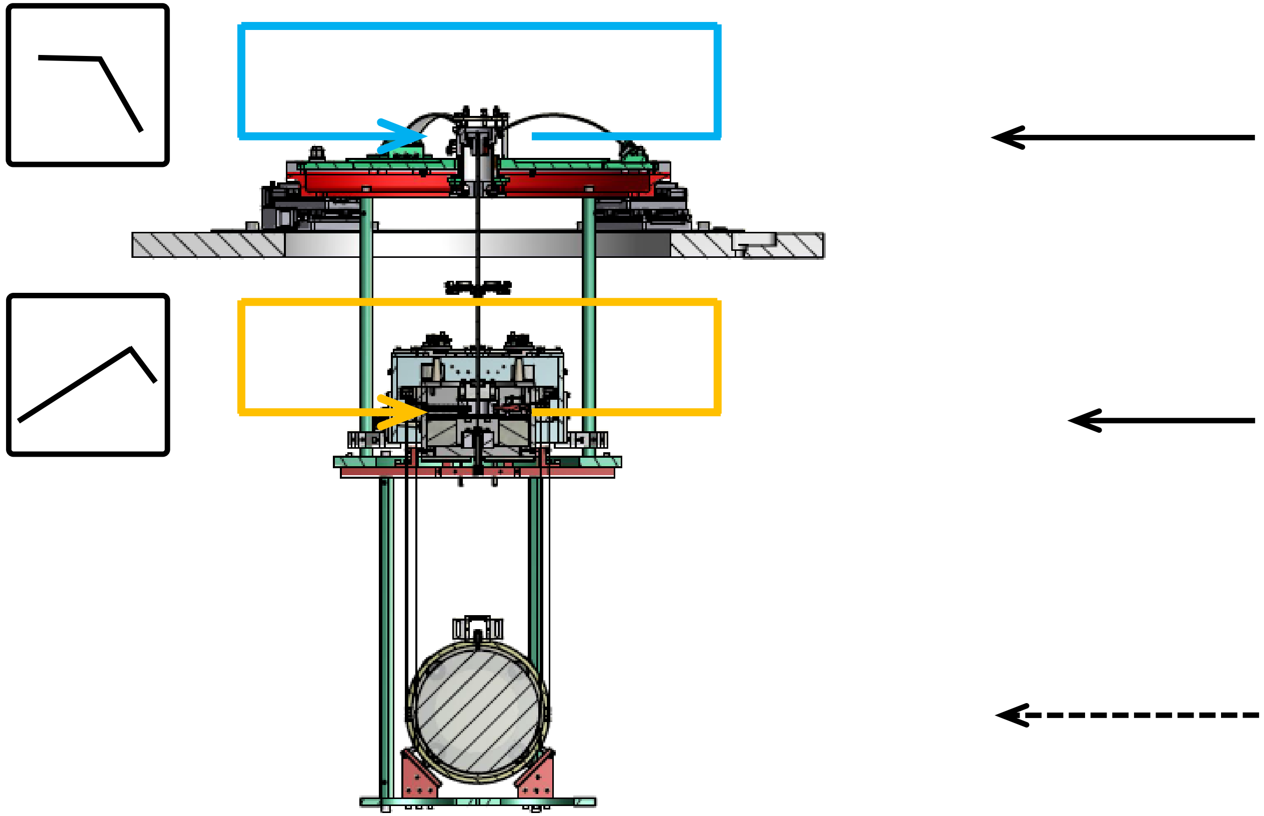




Resonances to be taken care (< 20 Hz) → 19 modes

Requirement in this test : 1/e decay time < 1 min.

Implemented control loops

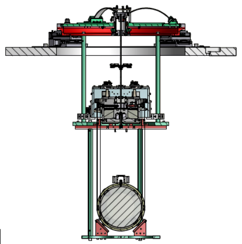


GAS :
DC control, with LVDT

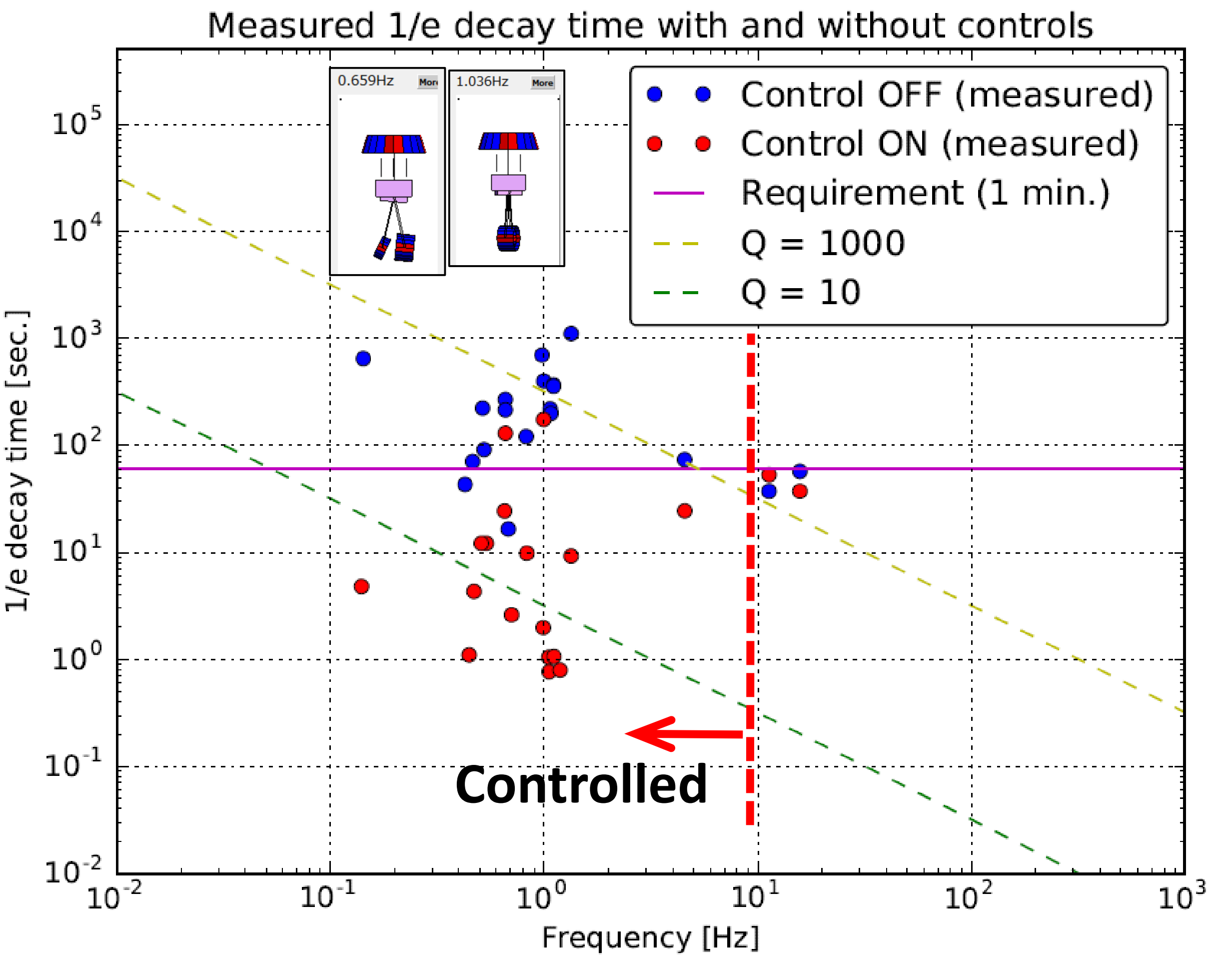
IM – IR :
Damping control, with OSEMs
(~ 10 Hz cutoff)

TM – RM :
Freely suspended

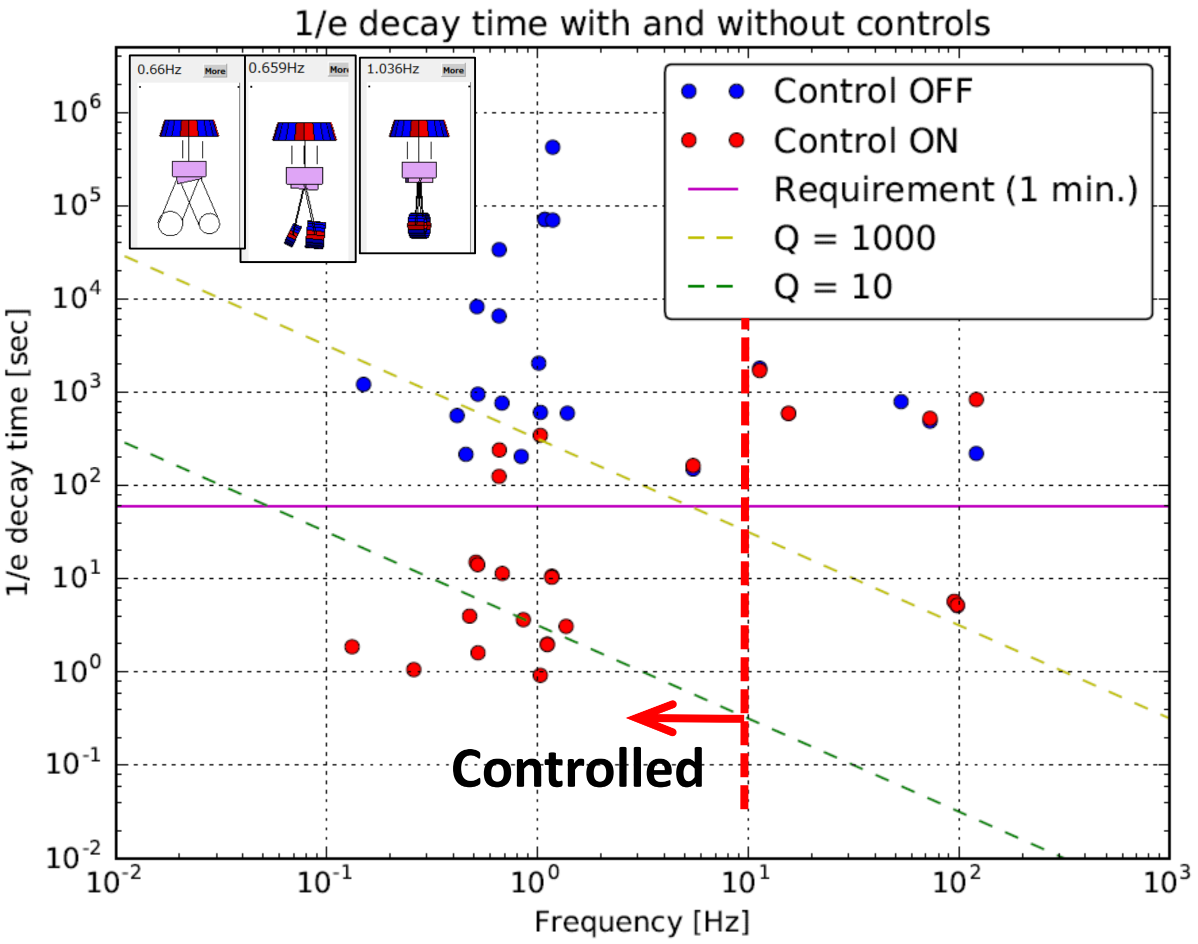
Measured damping time: Control OFF vs. Control ON



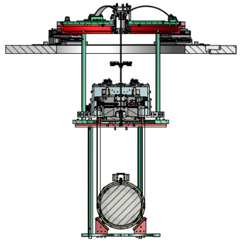
Measured



Simulated



Measured damping time: Control OFF vs. Control ON

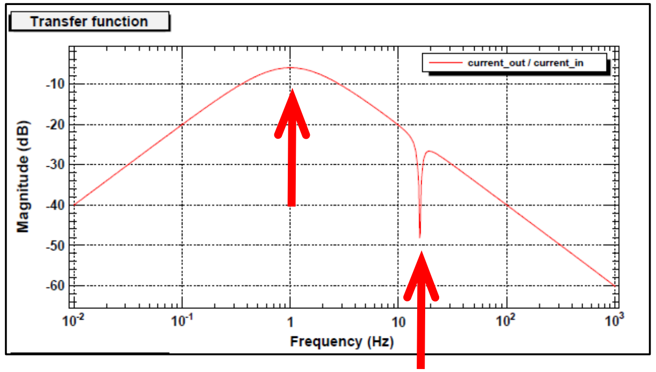


What the result says:

1. Simulation tends to tell larger natural Q factors than the actual ones.

→ Actual feedback filters can be different from the simulated ones, depending on actual Q factors.

→ notch? damping control cut-off frequency? ..
→ Filter tuning at the site would be needed.



Typical damping filter shape

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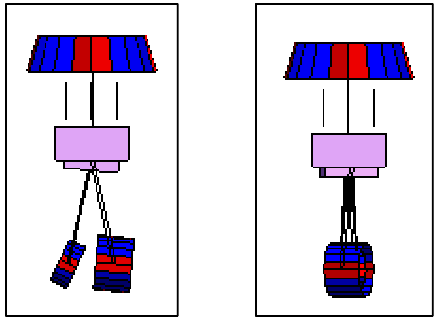
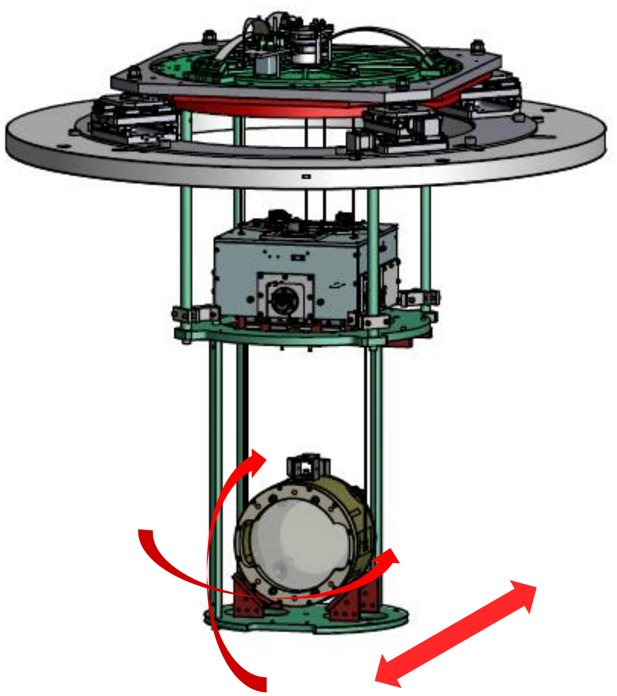
2. To damp optic & recoil mass motion, sensing the optic motion is needed.

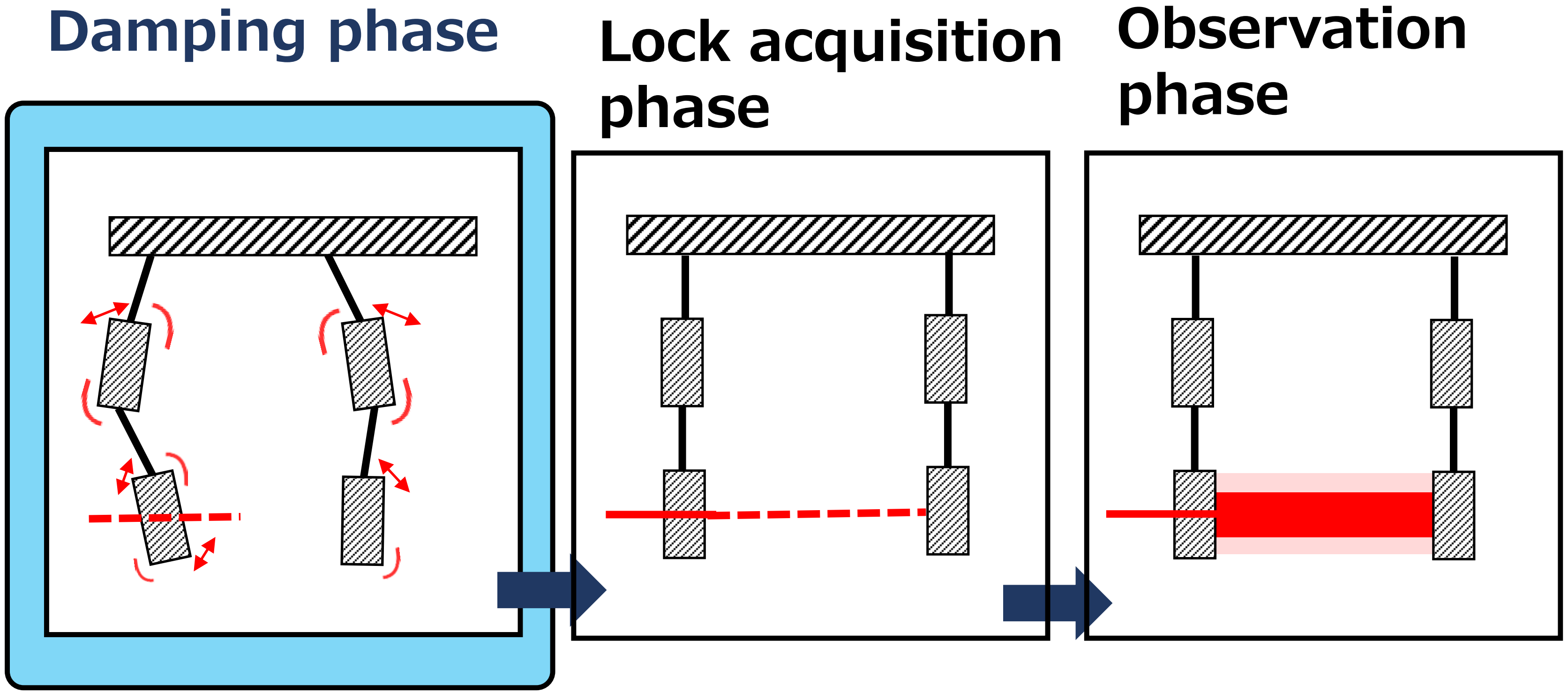


More than 2, 3 min (IM Ctrl-ON)

To be investigated:
→ Is oplev available even just after large disturbances ?

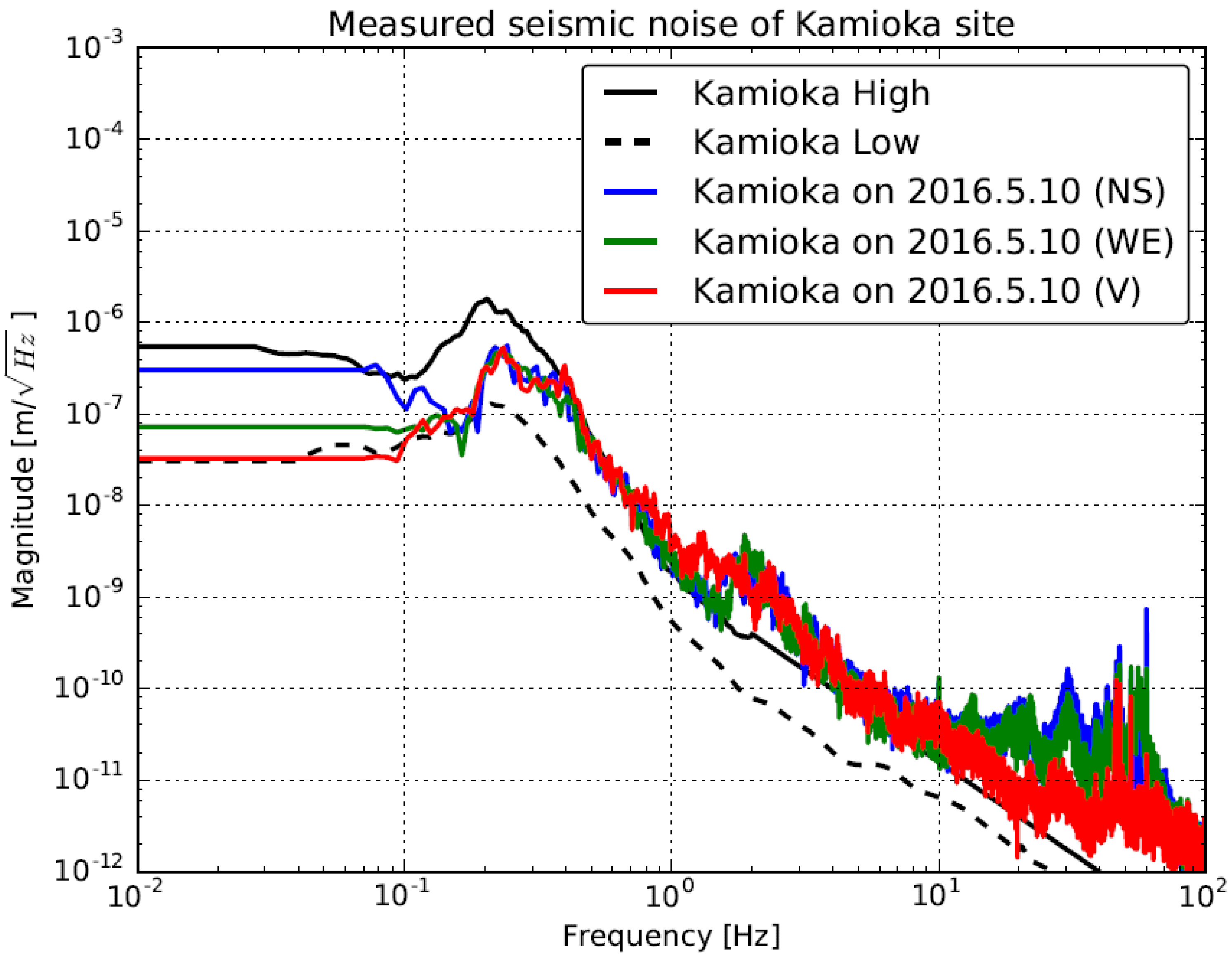
2-2. Residual vibration





Model vs. Measurement

Seismic noise of Kamioka (on 2016.5.10)

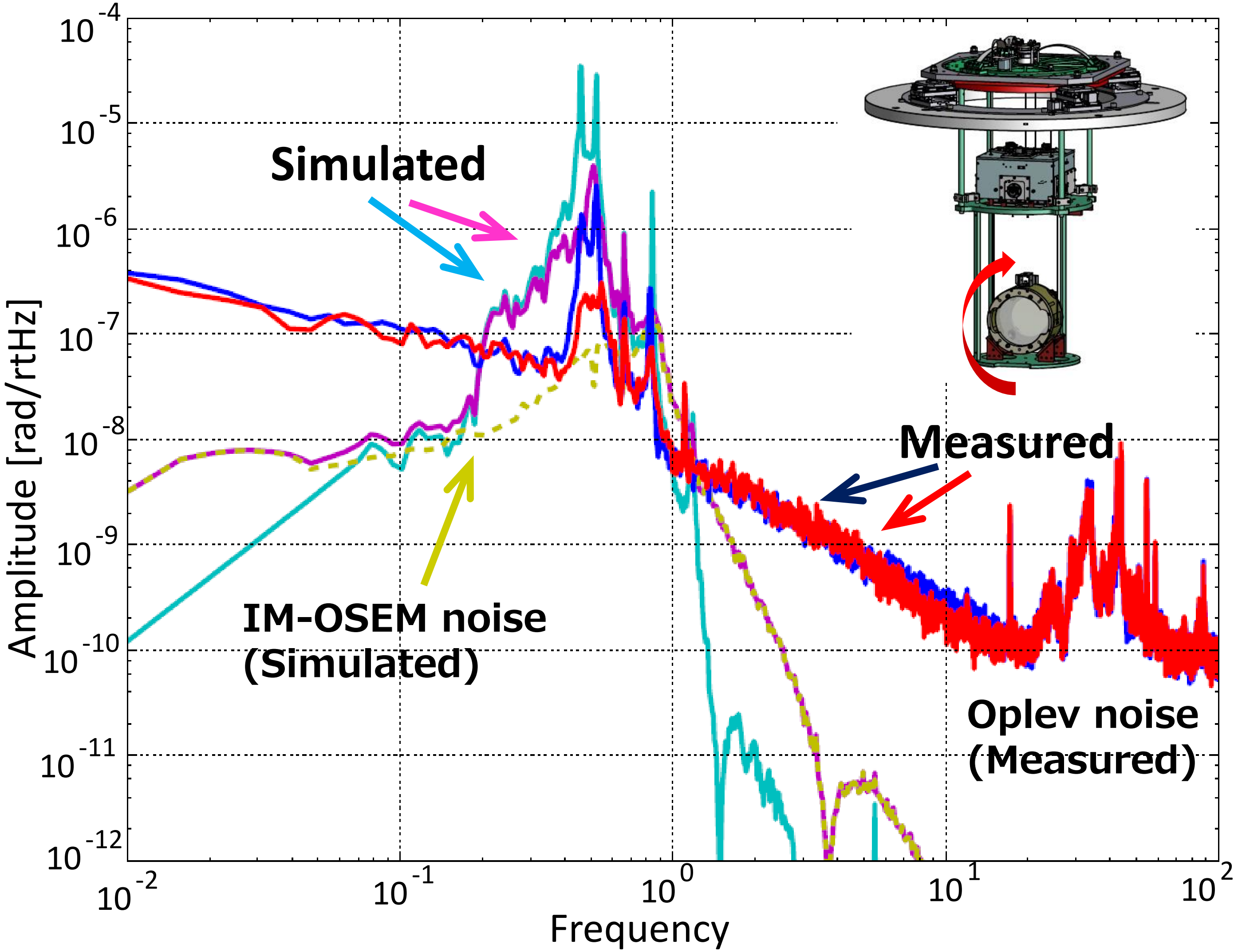


In following calculation, seismic noise measured on 2016.5.10 is considered (blue one).

cf.)
Following measurement was done on 2016.5.24.

Angular fluctuation of the optic (Pitch)

Model (based on 2016.5.10) vs. Measured (on 2016.5.24)



○ Resonance frequency

× Q factor, without control
→ lack of modeling (Actual < Model)

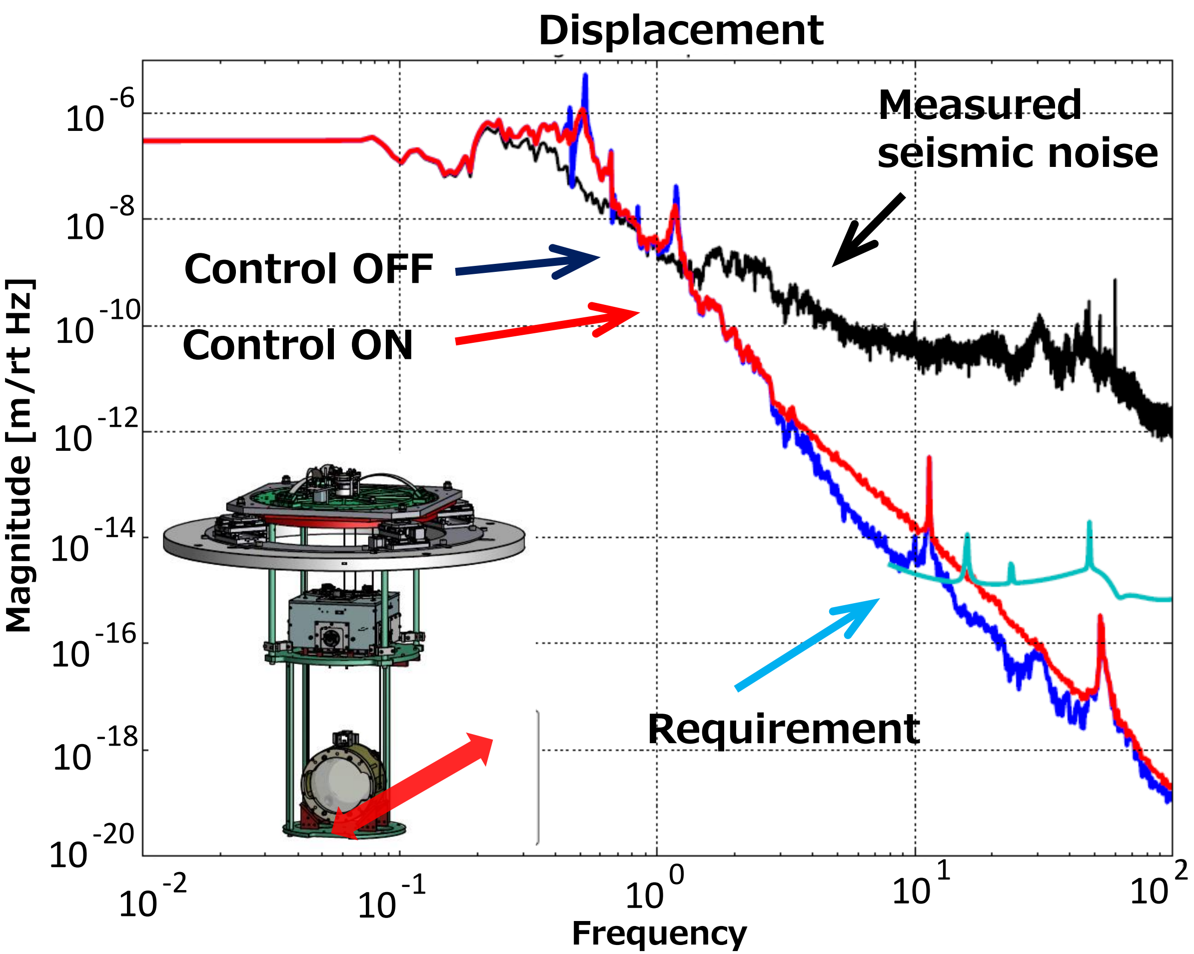
× 0.2 ~ 0.4 Hz structure
→For this prediction, to be considered:
→ seismic noise,
→ hanging condition..

RMS values
Control OFF (Model) : 4.4 um
Control ON (Model) : 0.7 um

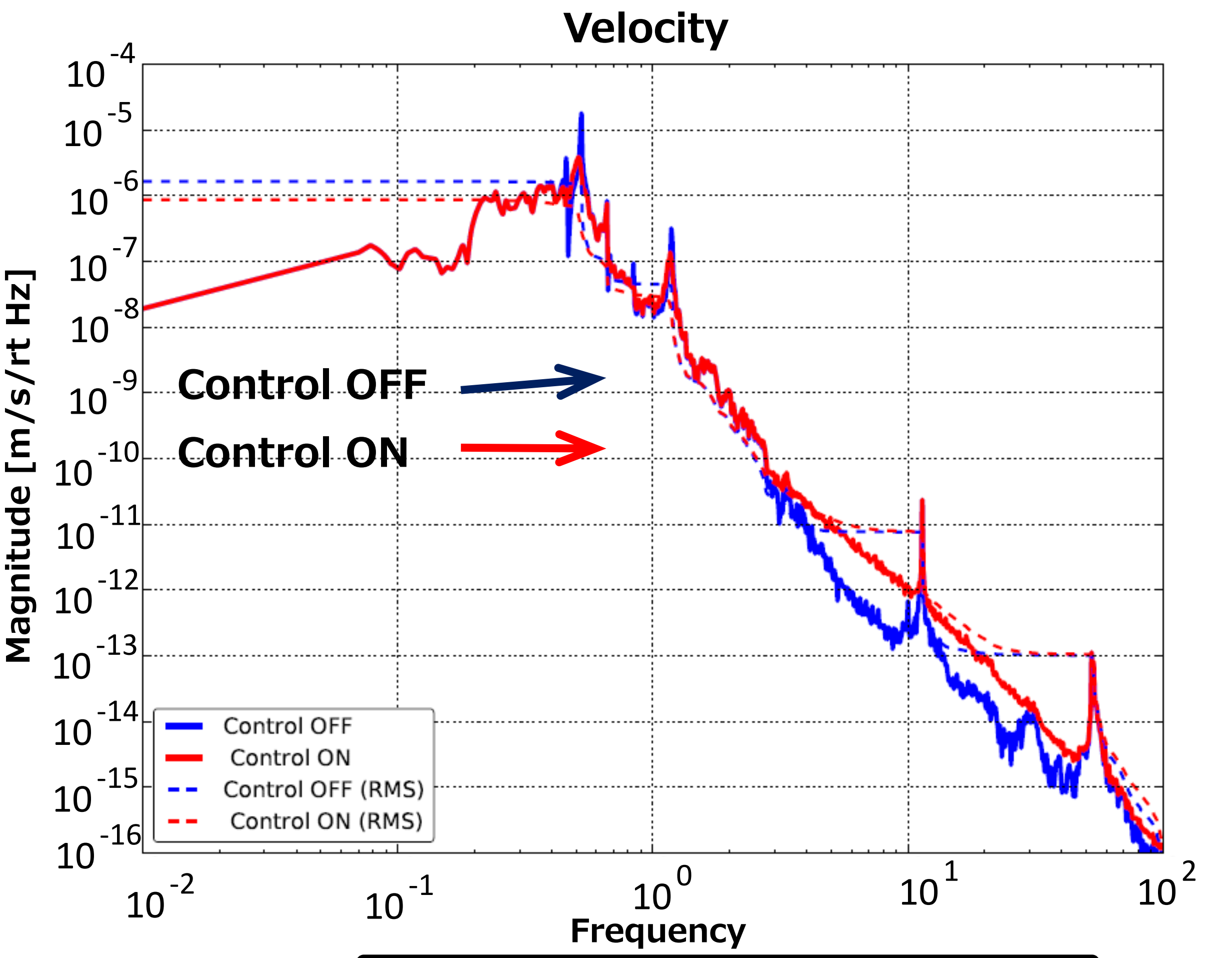
Control OFF (Measured) : 0.4 um
Control ON (Measured) : 0.1 um

→ *Simulation gives reasonable prediction.*

Expected fluctuation of the optic



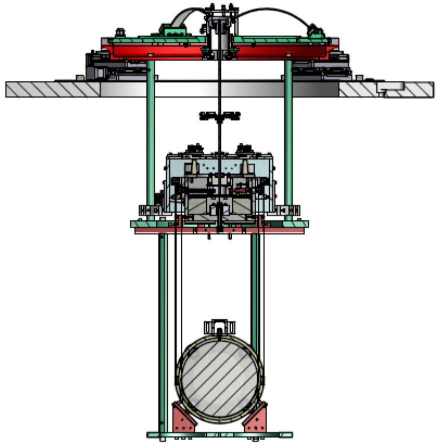
Control OFF : 0.5 um (RMS)
Control ON : 0.3 um (RMS)



Control OFF : 1.7 um/s (RMS)
Control ON : 0.8 um/s (RMS)

Summary of performance test

Measurement vs. Model



KEEP IN MIND:

1. Actual Q factors < predicted Q factors (of free swinging)
   → Some simulated servo filters can be modified at the site.
2. Sensing TM motion is needed, in damping phase.
   → should be investigated if oplev is available in the damping phase.

GOOD NEWS:

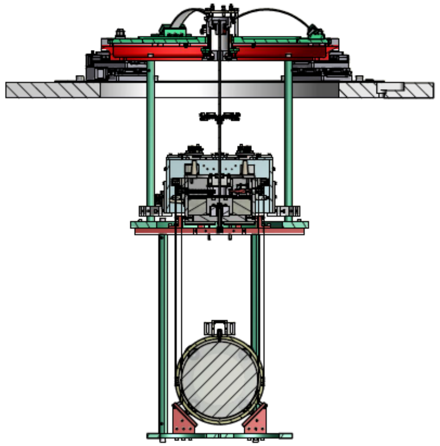
3. Our simulation has some uncertainties though, it tells reasonable prediction.

Using another sensors would be useful for more detailed characterization..
(Seismometers, length sensor for Longitudinal motion of the optic, etc.)

→ Updates would come soon. Type-Bp, B SAS would tell us much more information.

“iKAGRA data”, which I’d like to include:

→ Data for characterization of the iKAGRA PR3 SAS.

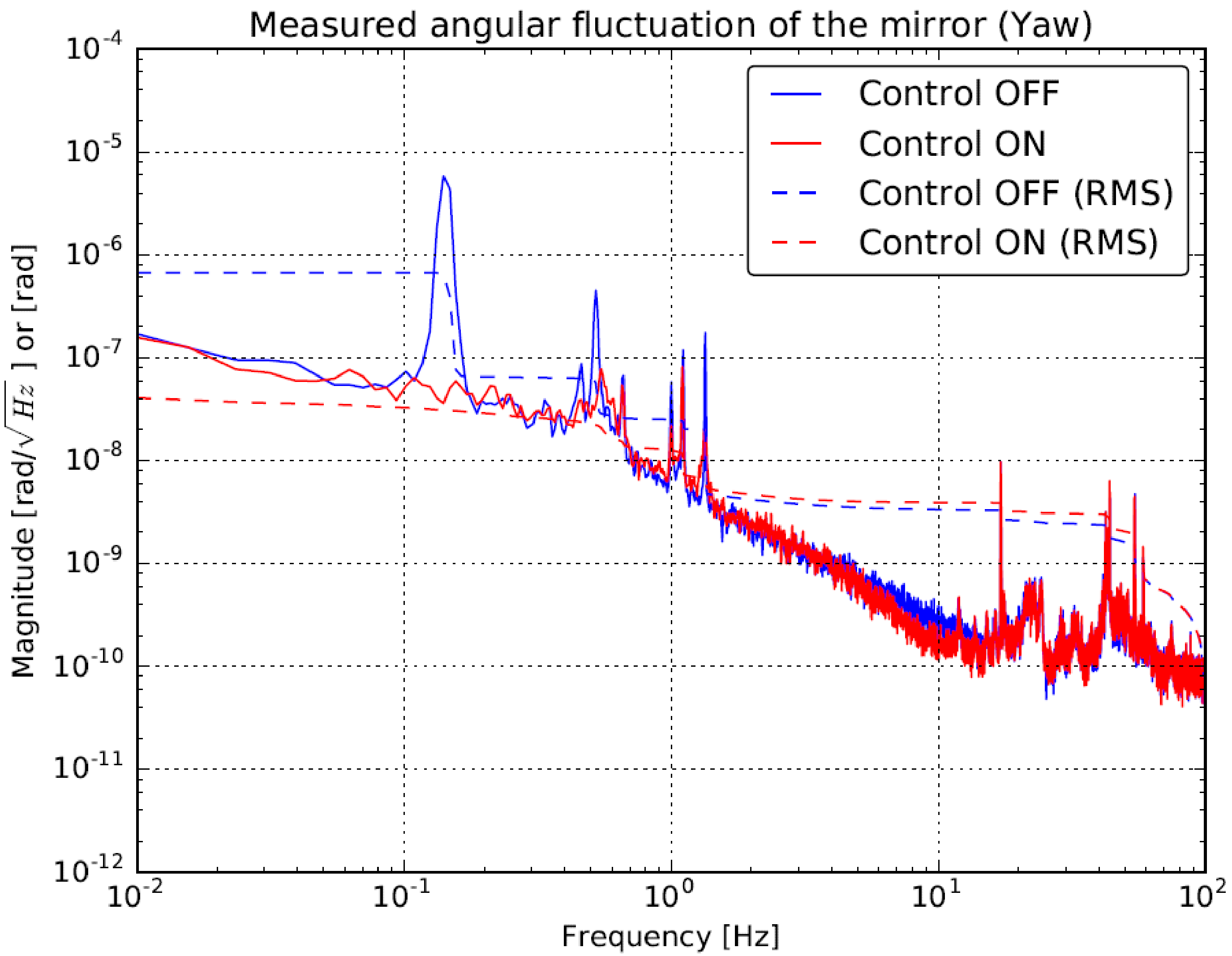


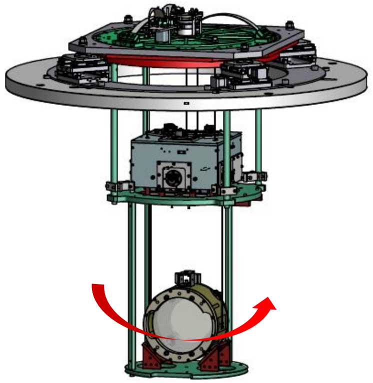
Back up

Other Type-Bpp measurement

Angular fluctuation of the mirror (Yaw)

Measured





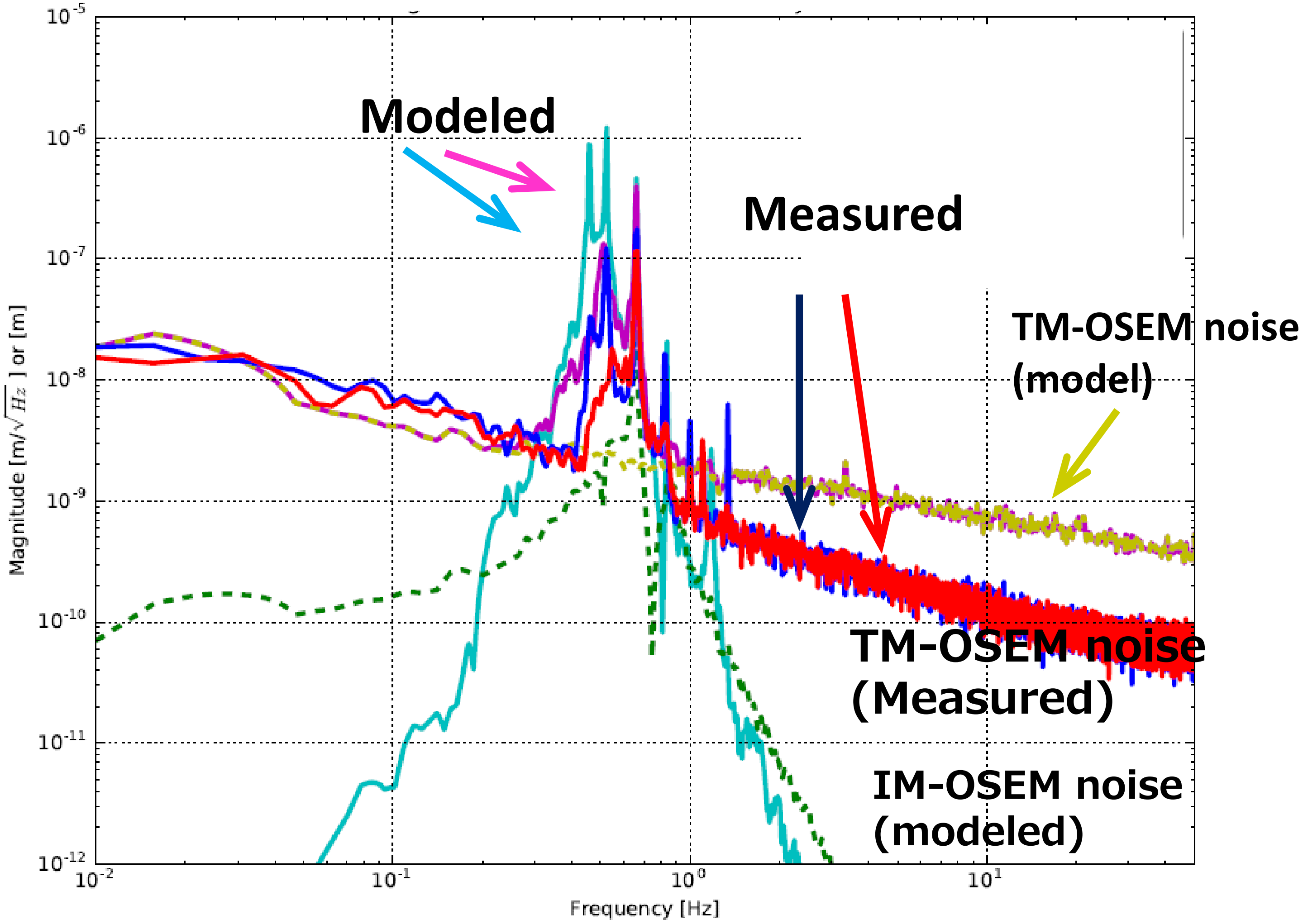
RMS values

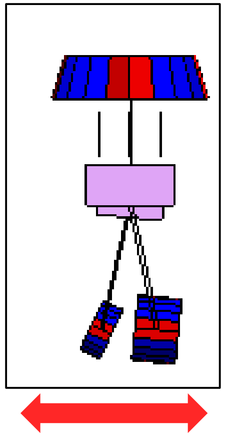
Control OFF (Model) : --- urad
Control ON (Model) : --- urad

Control OFF (Measured) : 0.63 urad
Control ON (Measured) : 0.040 urad

Displacement fluctuation measured by TM-OSEM (Longitudinal)

Model vs. Measured





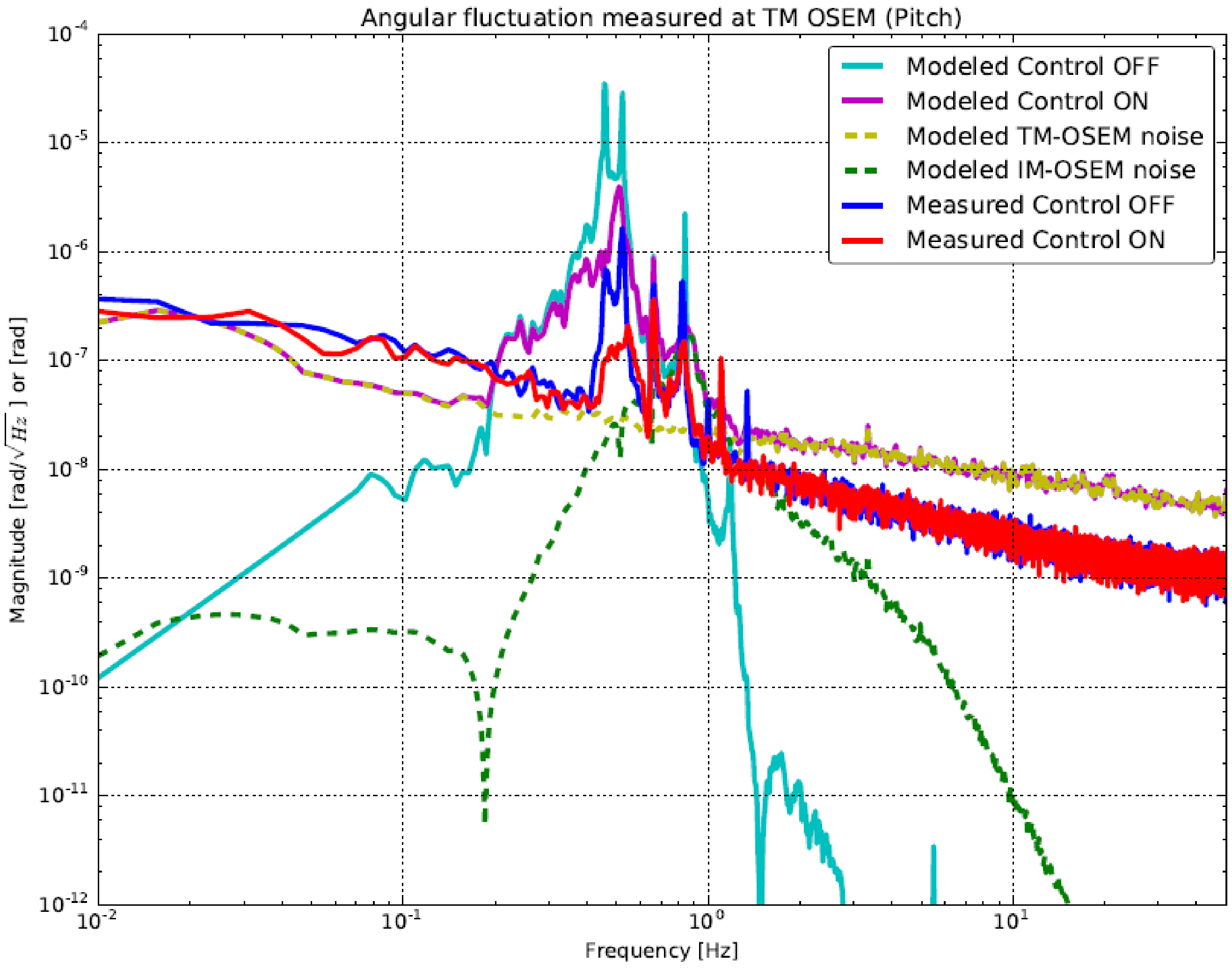
RMS values

Control OFF (Model) : 0.27 um
Control ON (Model) : 0.049 um

Control OFF (Measured) : 0.027 um
Control ON (Measured) : 0.016 um

Angular fluctuation measured by TM-OSEM (Pitch)

Model vs. Measured



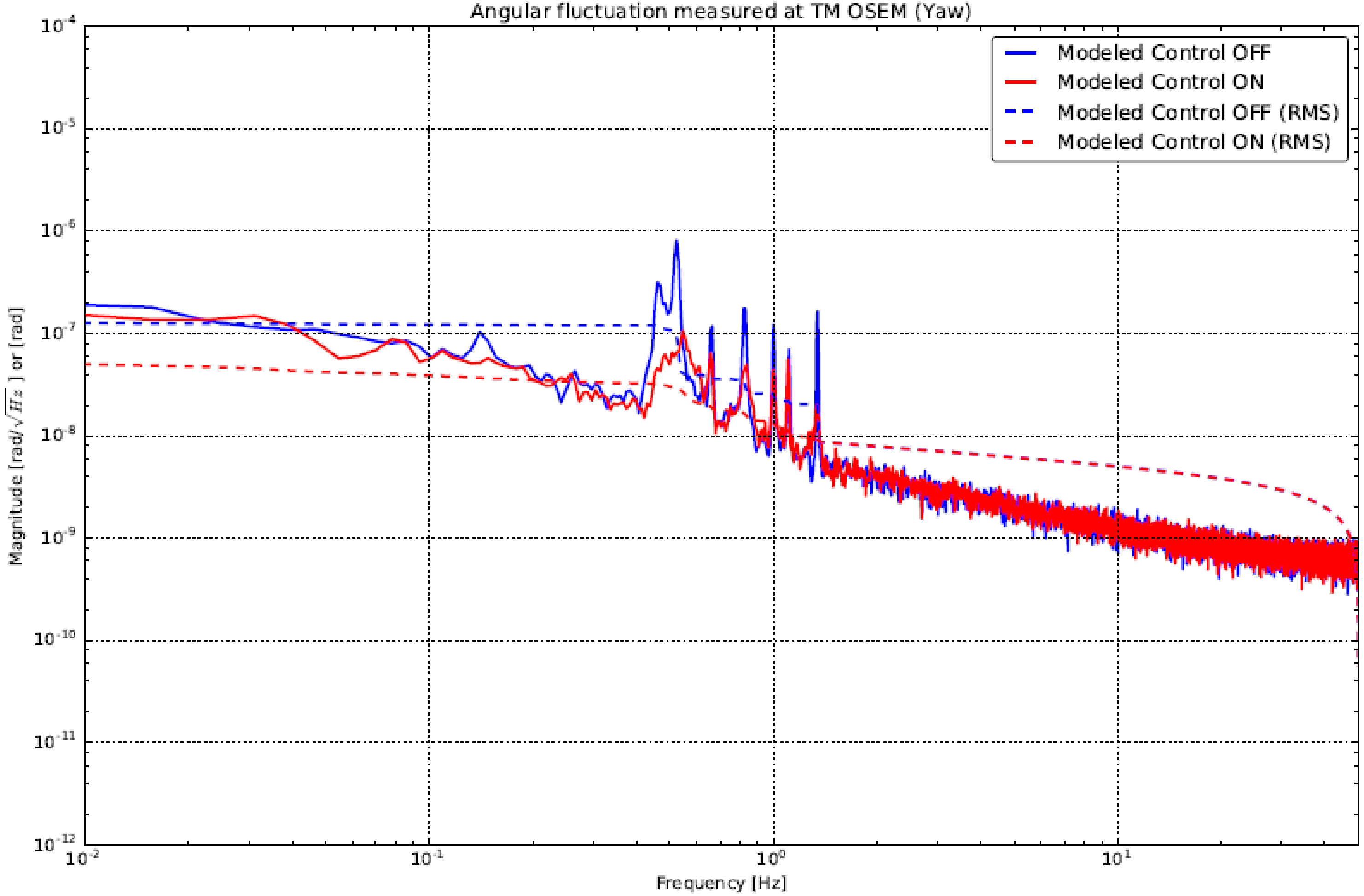
RMS values

Control OFF (Model) : 7.2 urad
Control ON (Model) : 1.1 urad

Control OFF (Measured) : 0.29 urad
Control ON (Measured) : 0.11 urad

Angular fluctuation measured by TM-OSEM (Yaw)

Measured

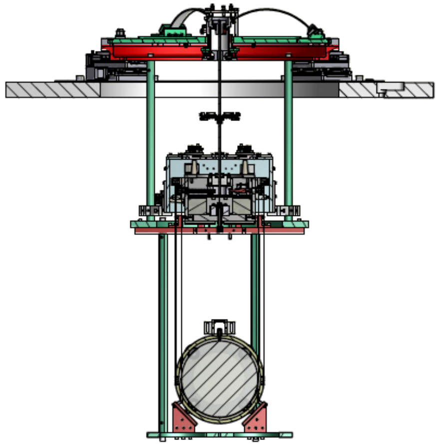


RMS values

Control OFF (Model) : ---
Control ON (Model) : ---

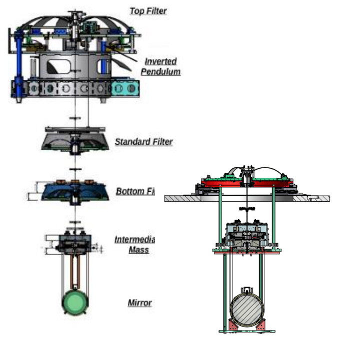
Control OFF (Measured) : 0.13 urad
Control ON (Measured) : 0.052 urad

2-3. Type-Bpp at Kamioka
vs. Type-B1proto at Tokyo Mitaka

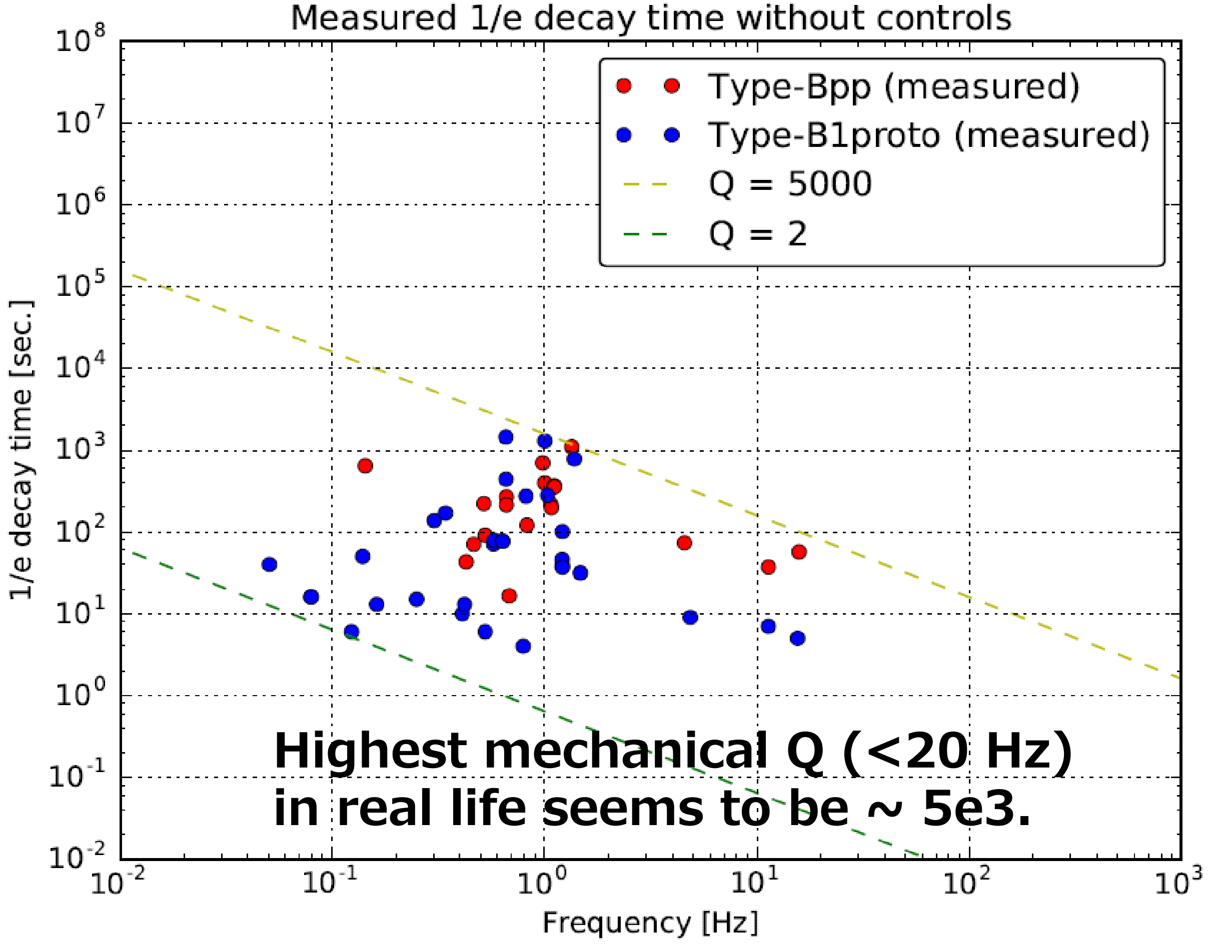


vs.

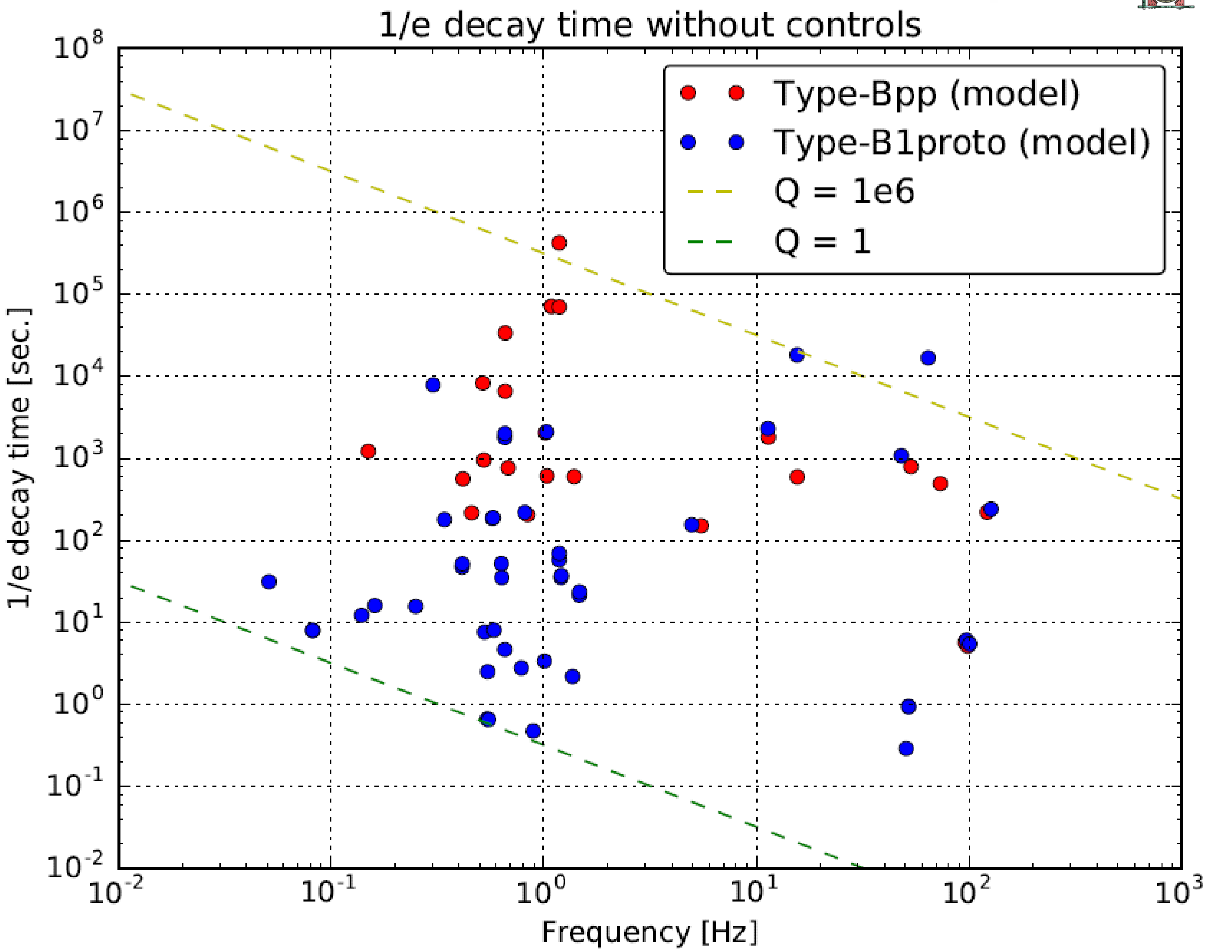
Mechanical Q factor of free swinging : Type-B1proto vs. Type-Bpp



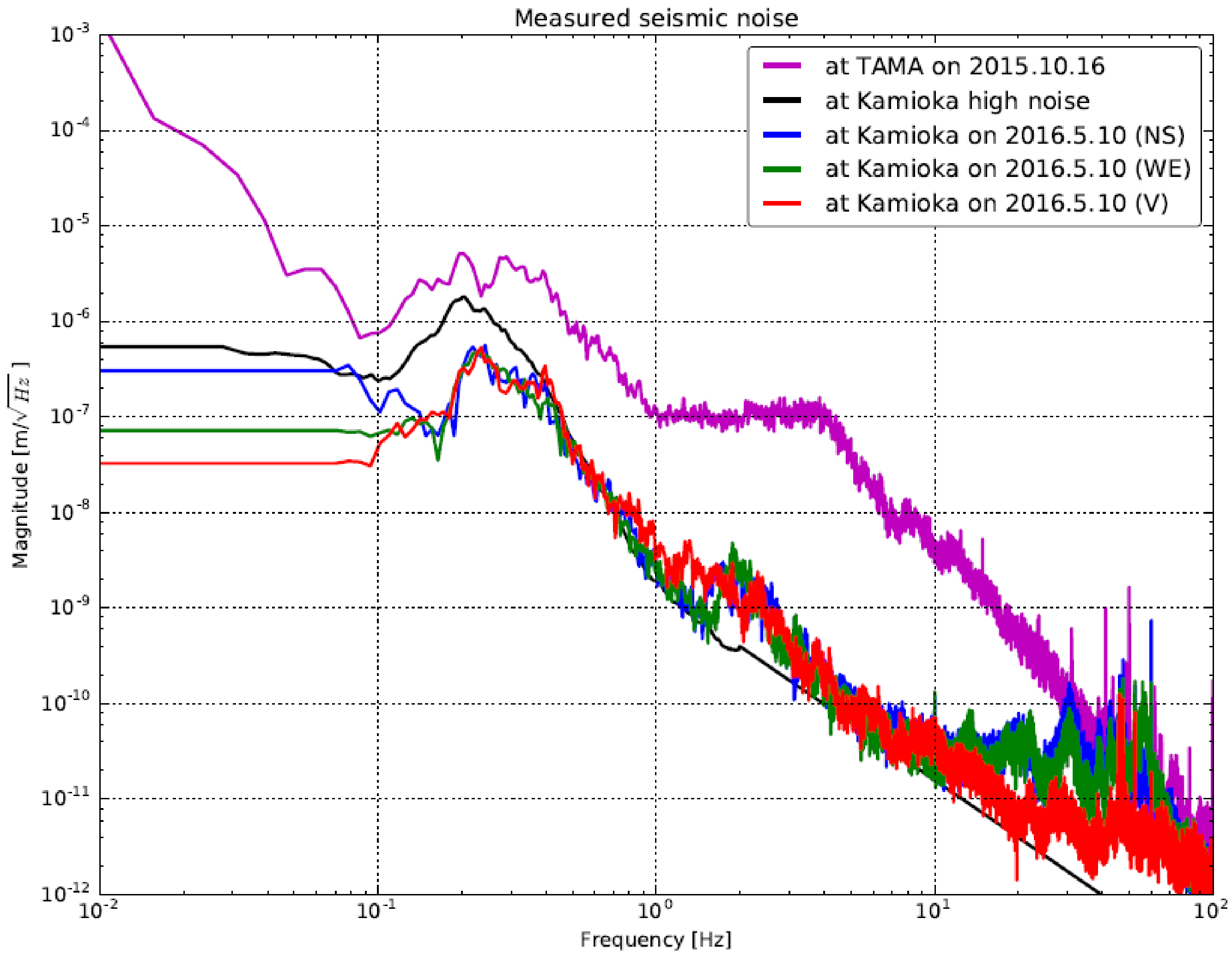
Measured



Model

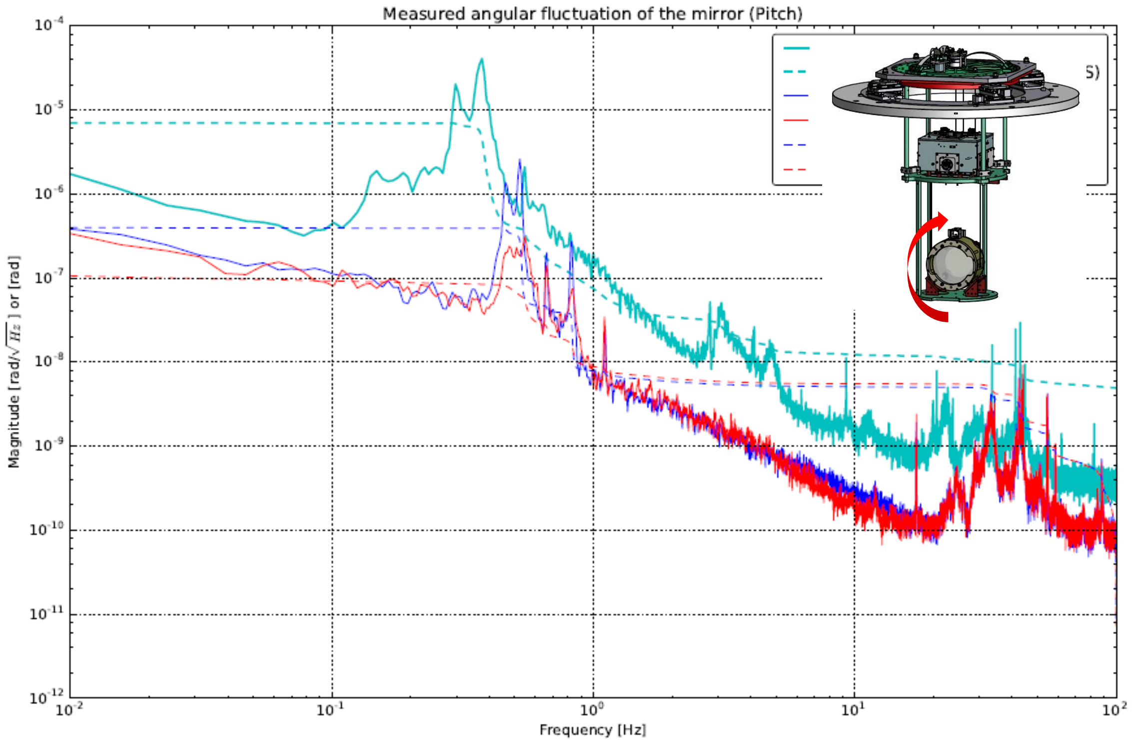


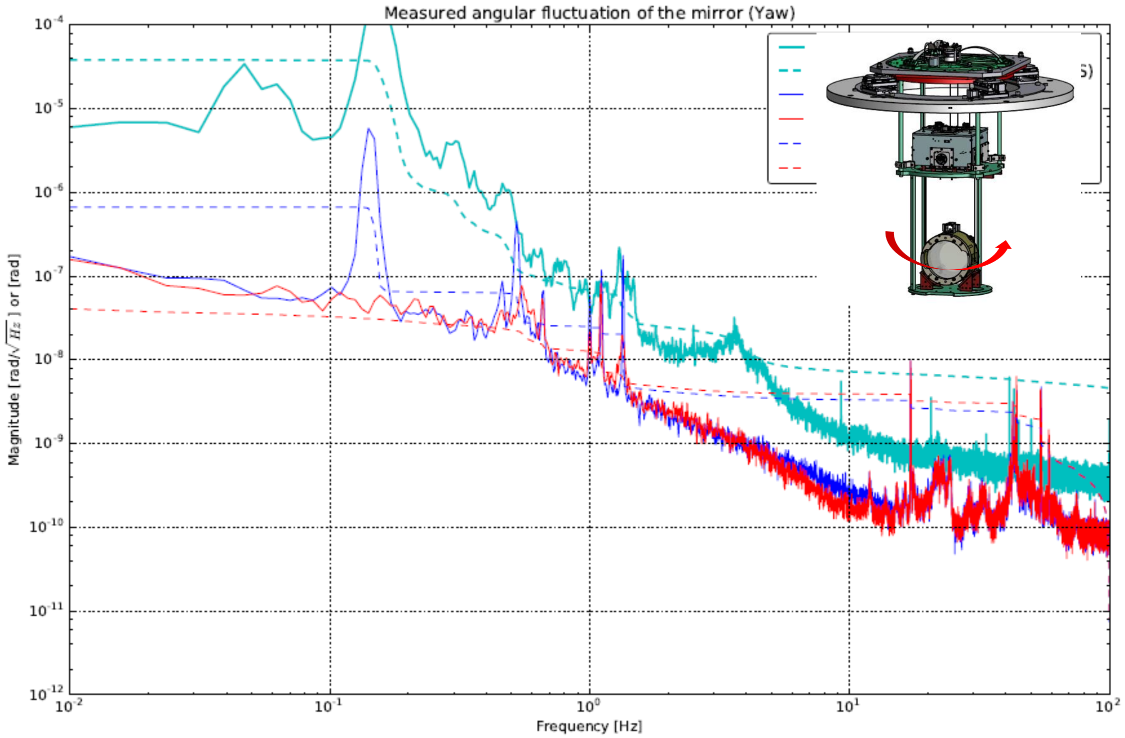
Seismic noise : Kamioka vs. TAMA



Seismic noise of Kamioka on 2016.5.10 was smaller than that of Tokyo,
by ~ one order of magnitude at 1 Hz,
by ~ two order of magnitude at 10 Hz.

Angular fluctuation of the mirror (Type-B1proto vs. type-Bpp)





RMS values

Control OFF (TypeB1proto) : 7.0 urad

Control OFF (Measured) : 0.37 urad

Control ON (Measured) : 0.10 urad

RMS values

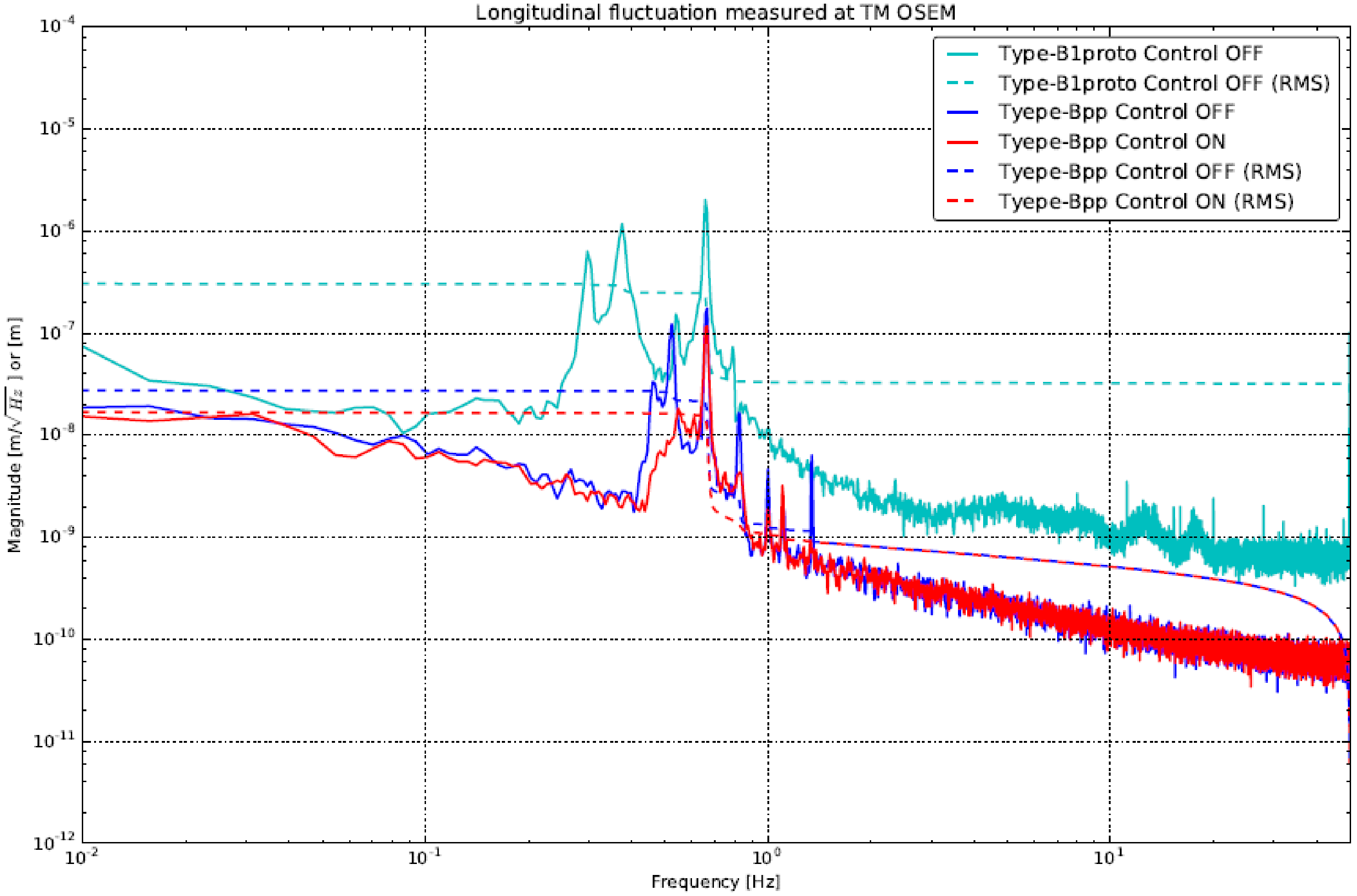
Control OFF (TypeB1proto) : 37 urad

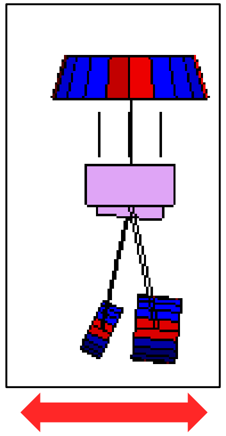
Control OFF (Measured) : 0.63 urad

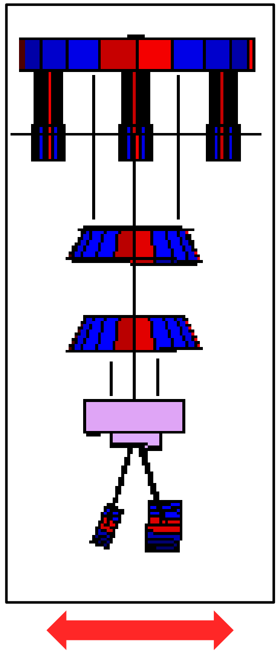
Control ON (Measured) : 0.040 urad

Displacement fluctuation measured by TM-OSEM (Longitudinal)

Type-B1proto vs. type-Bpp







RMS values

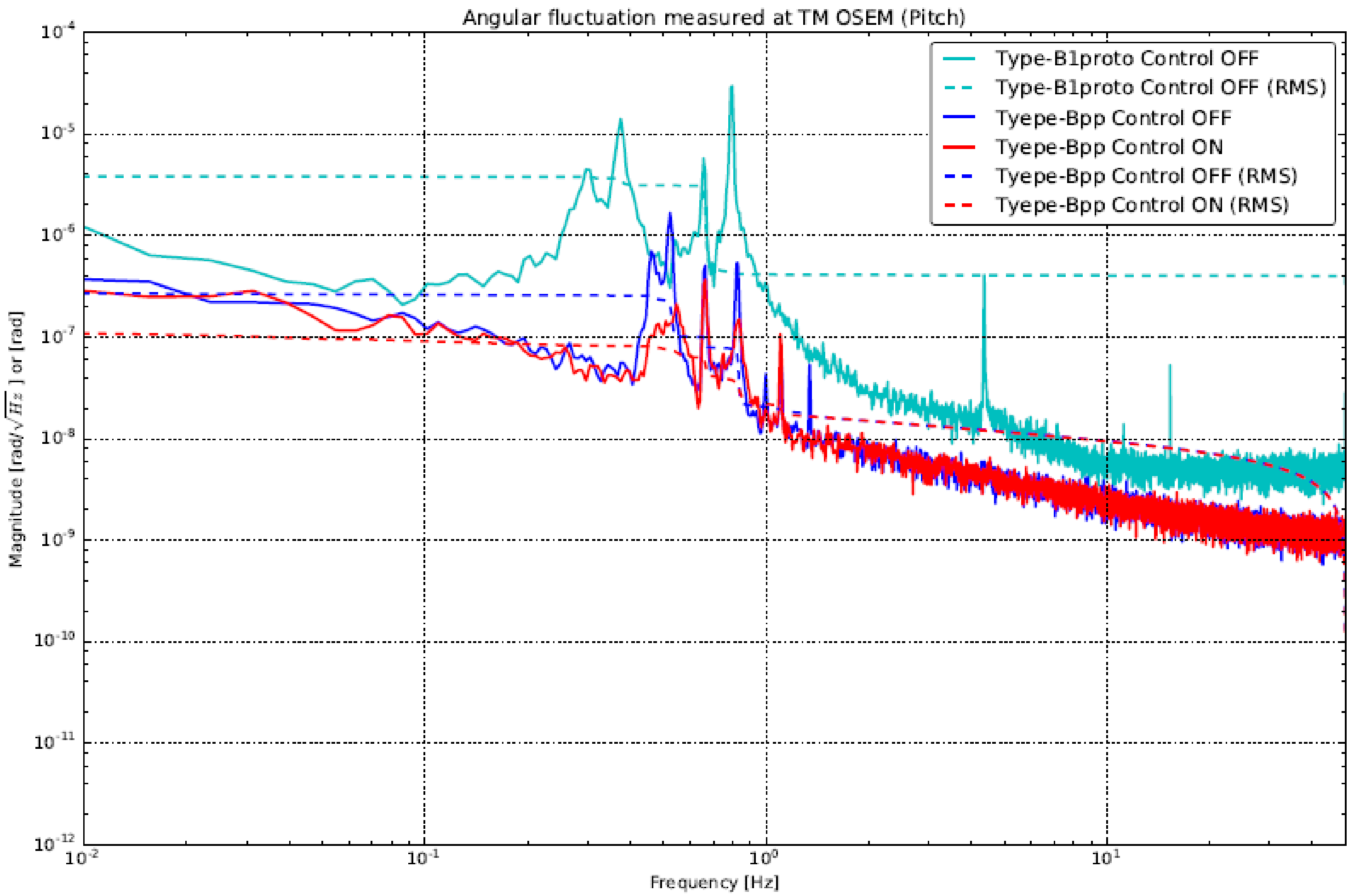
Control OFF (TypeB1proto) : 0.31 um

Control OFF (Measured) : 0.027 um

Control ON (Measured) : 0.016 um

0.3 Hz → 0.4 Hz : Caused by the suspension point difference of the IM

Angular fluctuation measured by TM-OSEM (Pitch)
Type-B1proto vs. type-Bpp



RMS values

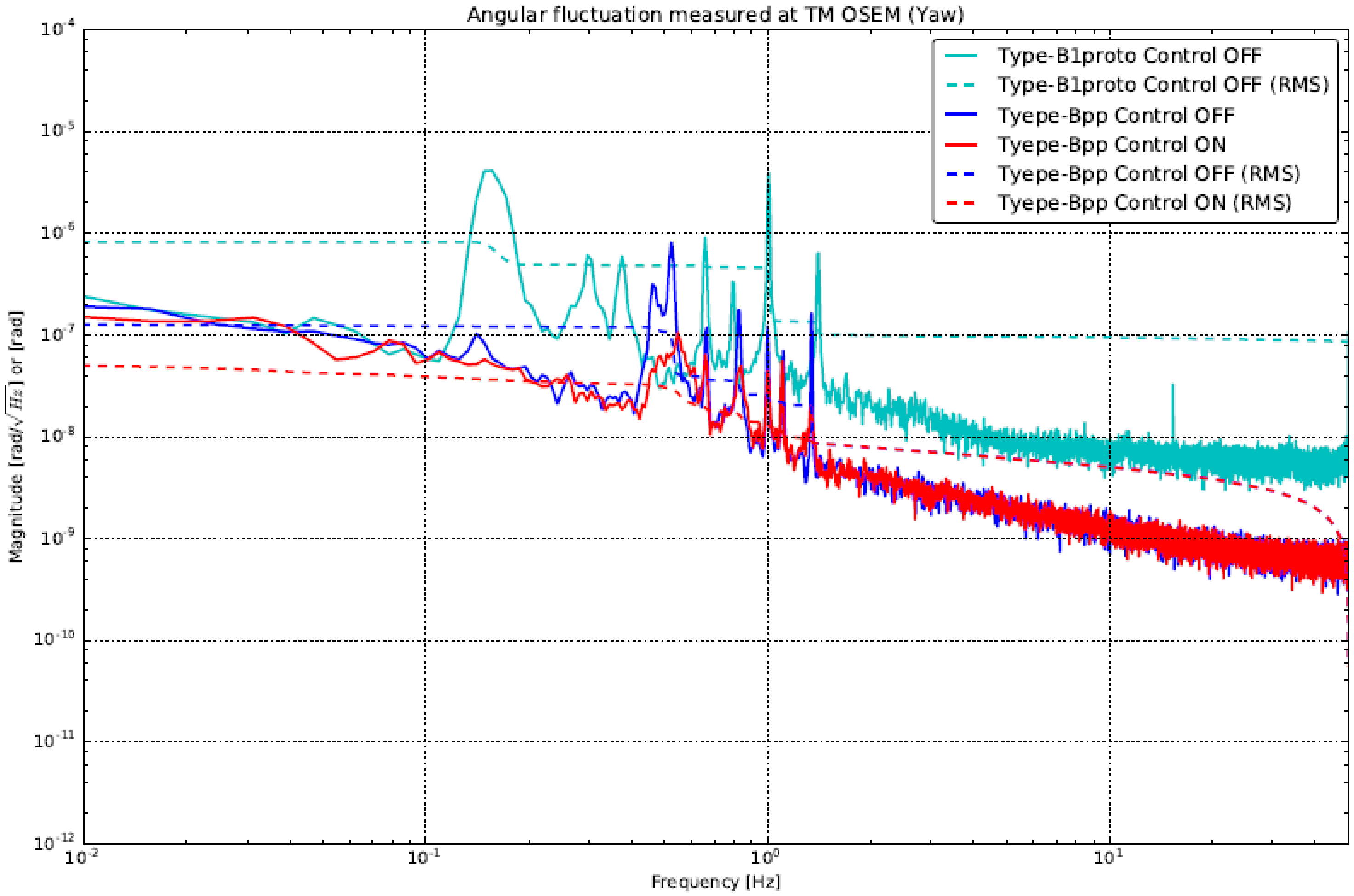
Control OFF (TypeB1proto) : 4.0 urad

Control OFF (Measured) : 0.29 urad

Control ON (Measured) : 0.11 urad

0.3 Hz → 0.4 Hz : Caused by the suspension point difference of the IM

Angular fluctuation measured by TM-OSEM (Yaw)
Type-B1proto vs. type-Bpp



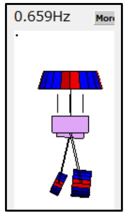
RMS values

Control OFF (TypeB1proto) : 0.83 urad

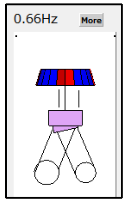
Control OFF (Measured) : 0.13 urad

Control ON (Measured) : 0.052 urad

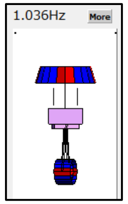
No-controlled damping time comparison



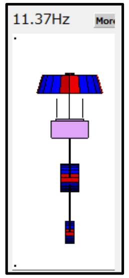
LRM – LTM	0.65 Hz	Measured *t* [s]	Modeled *t* [s]
typeB1proto		1448	1790
typeBpp		268	6585



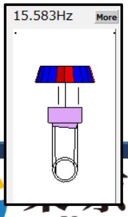
TRM – TTM	0.65 Hz	Measured *t* [s]	Modeled *t* [s]
typeB1proto		442	2009
typeBpp		214	33905



YRM – YTM	1.00 Hz	Measured *t* [s]	Modeled *t* [s]
typeB1proto		1295	2101
typeBpp		398	608



VRM	11.5 Hz	Measured *t* [s]	Modeled *t* [s]
typeB1proto		7	2305
typeBpp		37	1812



RTM	15.8 Hz	Measured *t* [s]	Modeled *t* [s]
typeB1proto		5	18266
typeBpp		57	593

Can be suffered from the aluminum sheet.

3. Summary

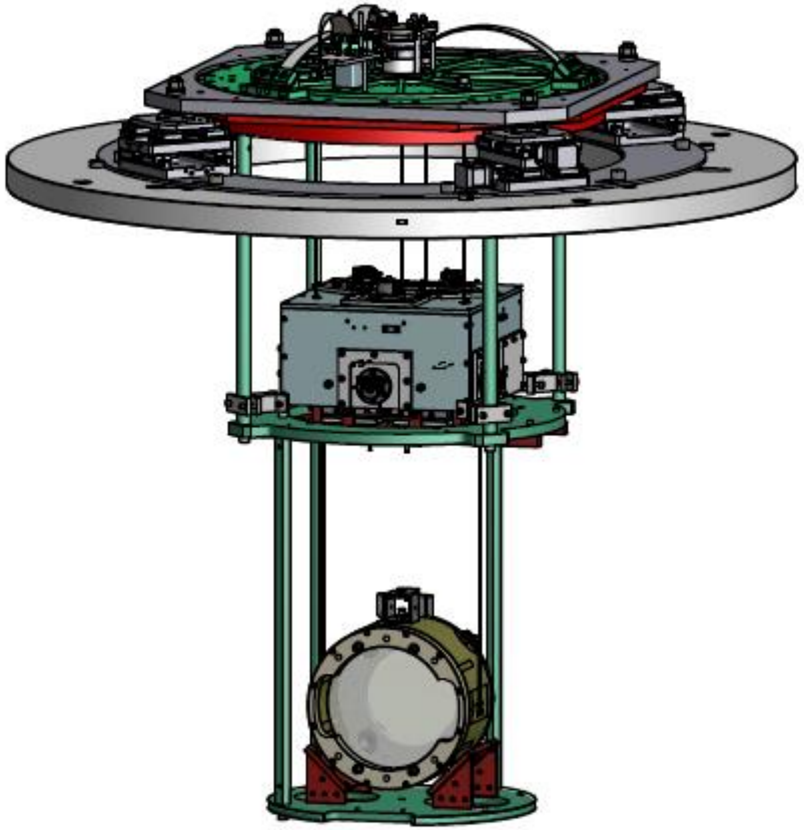
Performance test of iKAGRA PR3 SAS at Kamioka

The differences of p.28 can come from difference of

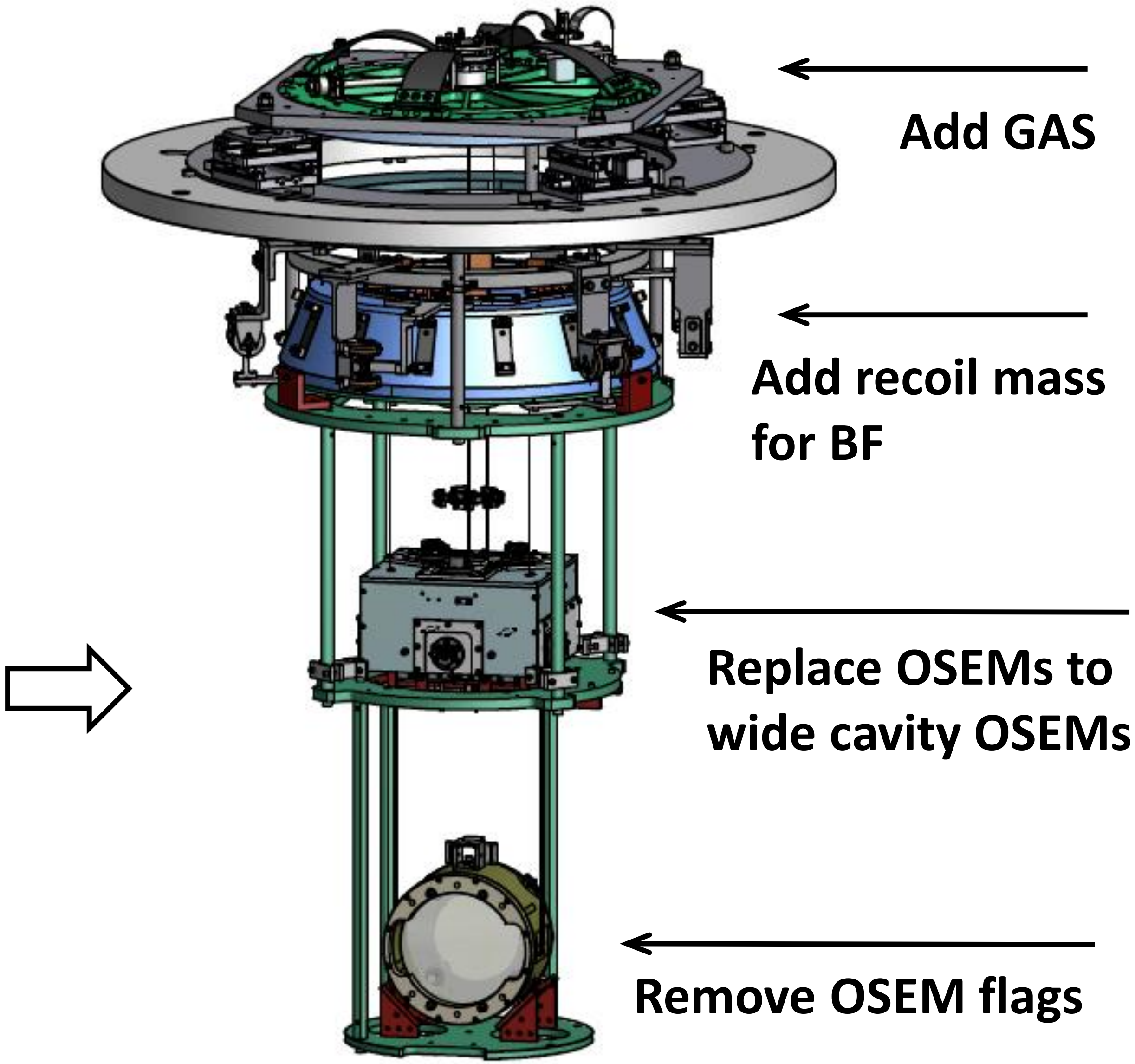
1. **Seismic noise**
2. **Suspension points**
3. **circuits, power supply,.. etc.**

Contents

4. Introduction
bKAGRA PR SAS (= Type-Bp SAS)

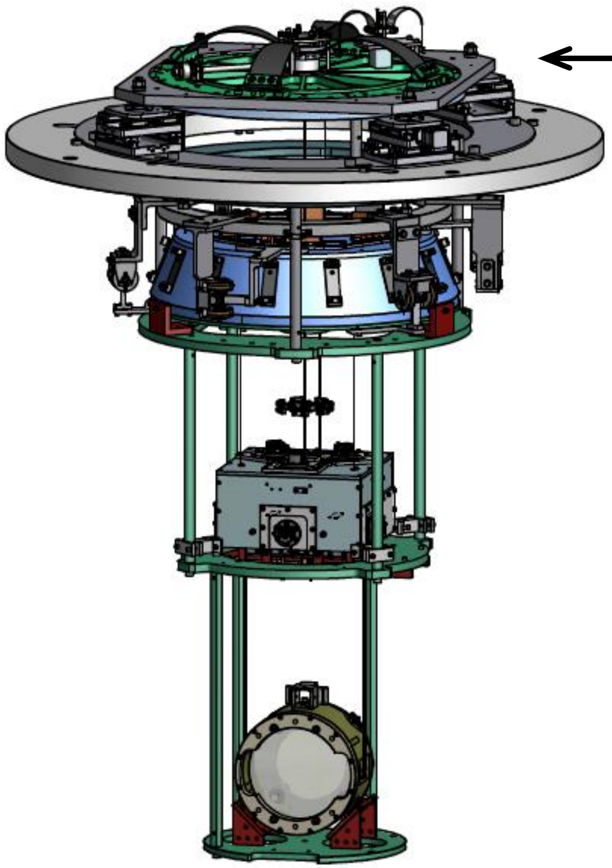


Type-Bpp SAS



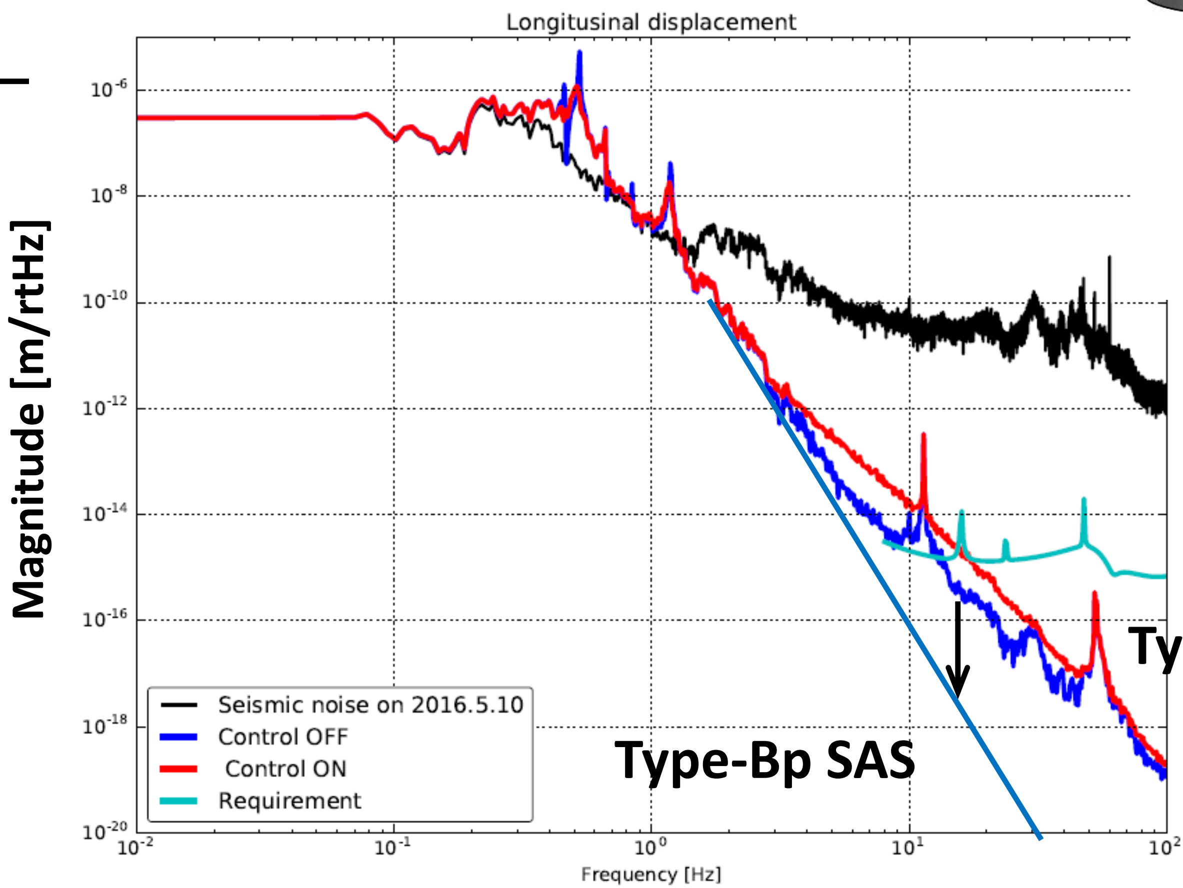
Type-Bp SAS

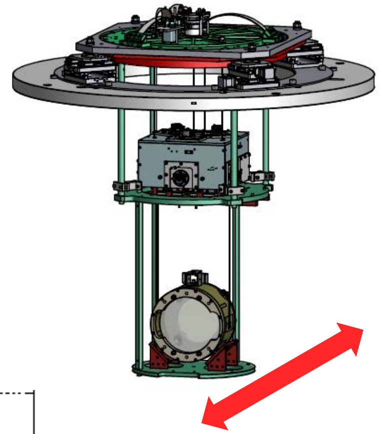
Modification



Type-Bp SAS

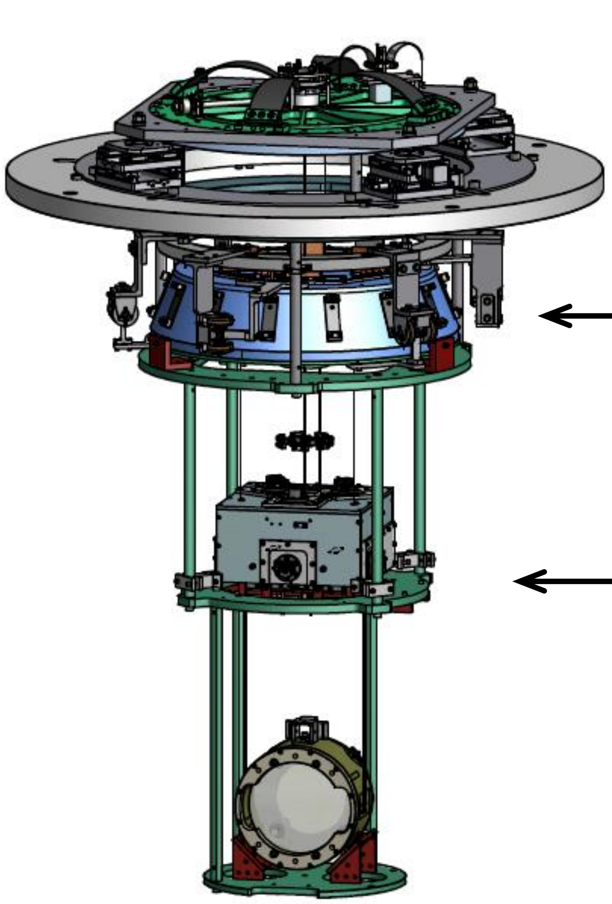
Standard GAS filter





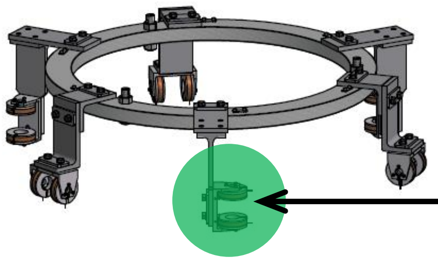
Purpose : improve vibration isolation performance.

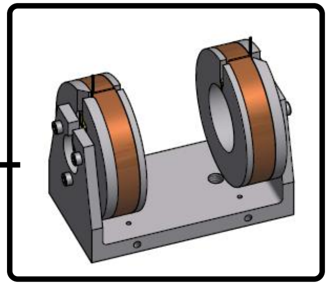
Modification

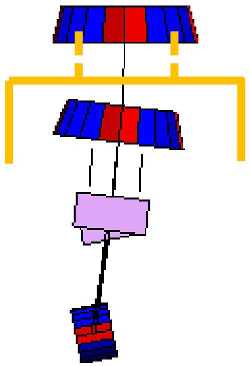


Type-Bp SAS

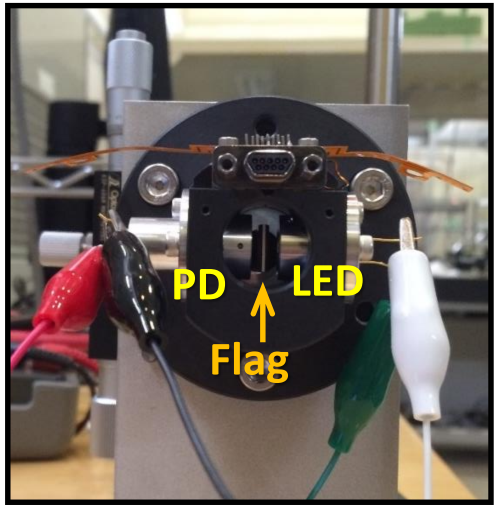
Bottom filter recoil mass

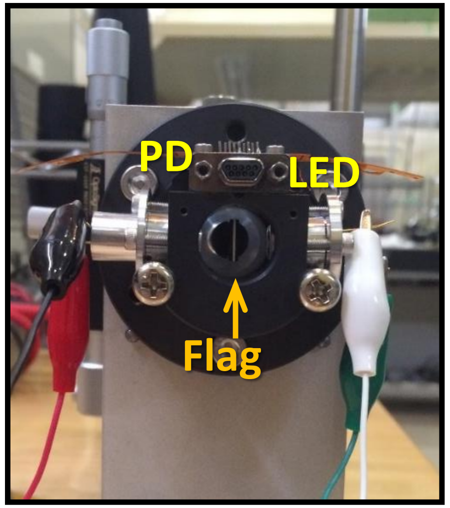






Purpose : damp the whole chain pendulum mode

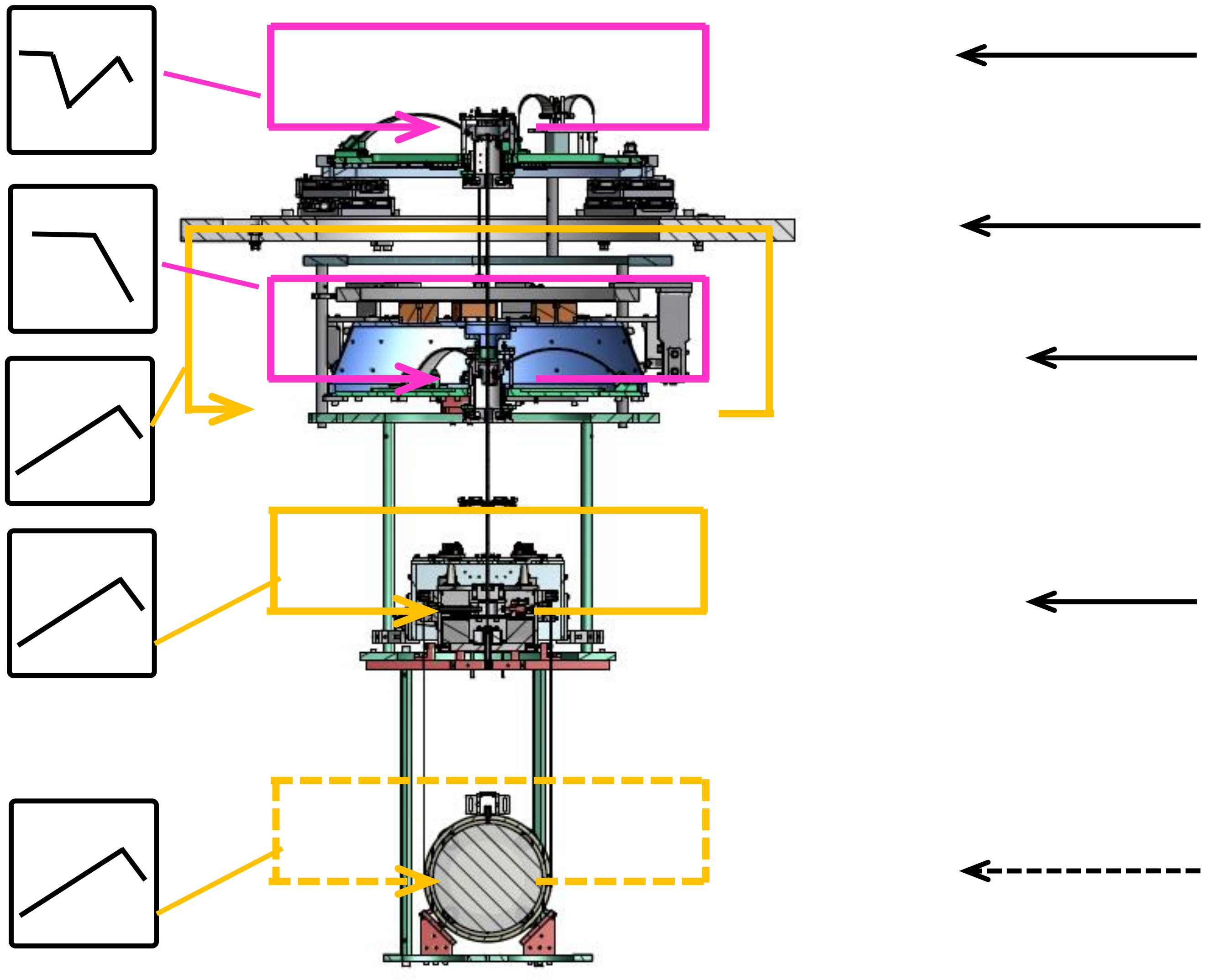




Purpose : reduce risk of breaking OSEM flags

Controllability of Type-Bp SAS

Control loops in damping phase



SF - GAS:
DC +damping control, with LVDT

BF - GAS:
DC control, with LVDT

BF – BR :
Damping control, with small LVDT

IM – IR :
Damping control, with OSEM

TM – RM :
(Damping control, with Oplev & OSEM) actuators

Requirements for control

Making servo filters for the each phase

1. Damping phase →
2. Lock-acquisition phase
3. Observation phase

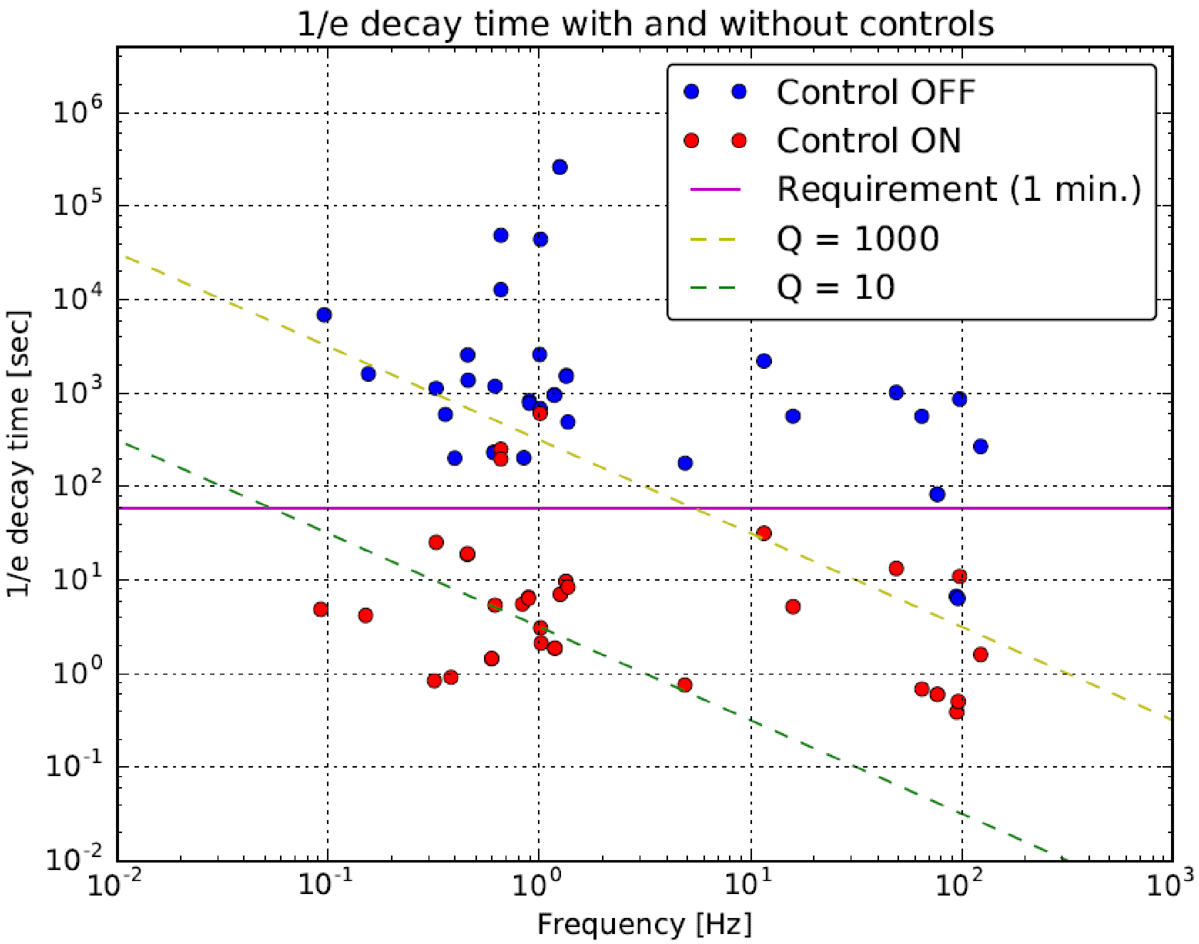
Damping

Requirement

1. Damping time < 1min.
2. RMS displacement (L) < 50 um
3. RMS displacement (T, V) < 1 mm
4. RMS displacement (P, Y) < 50 urad

Simulated damping time: Control ON vs. Control OFF

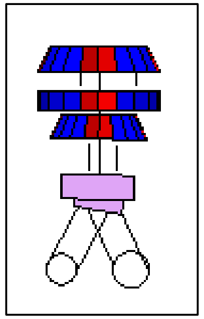
Model



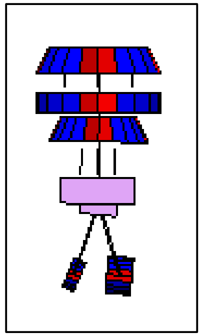
GAS : DC

IM : Damping (IMOSEM→ IMOSEM)

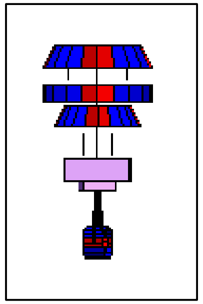
If oplev is not available…



252 sec



198 sec

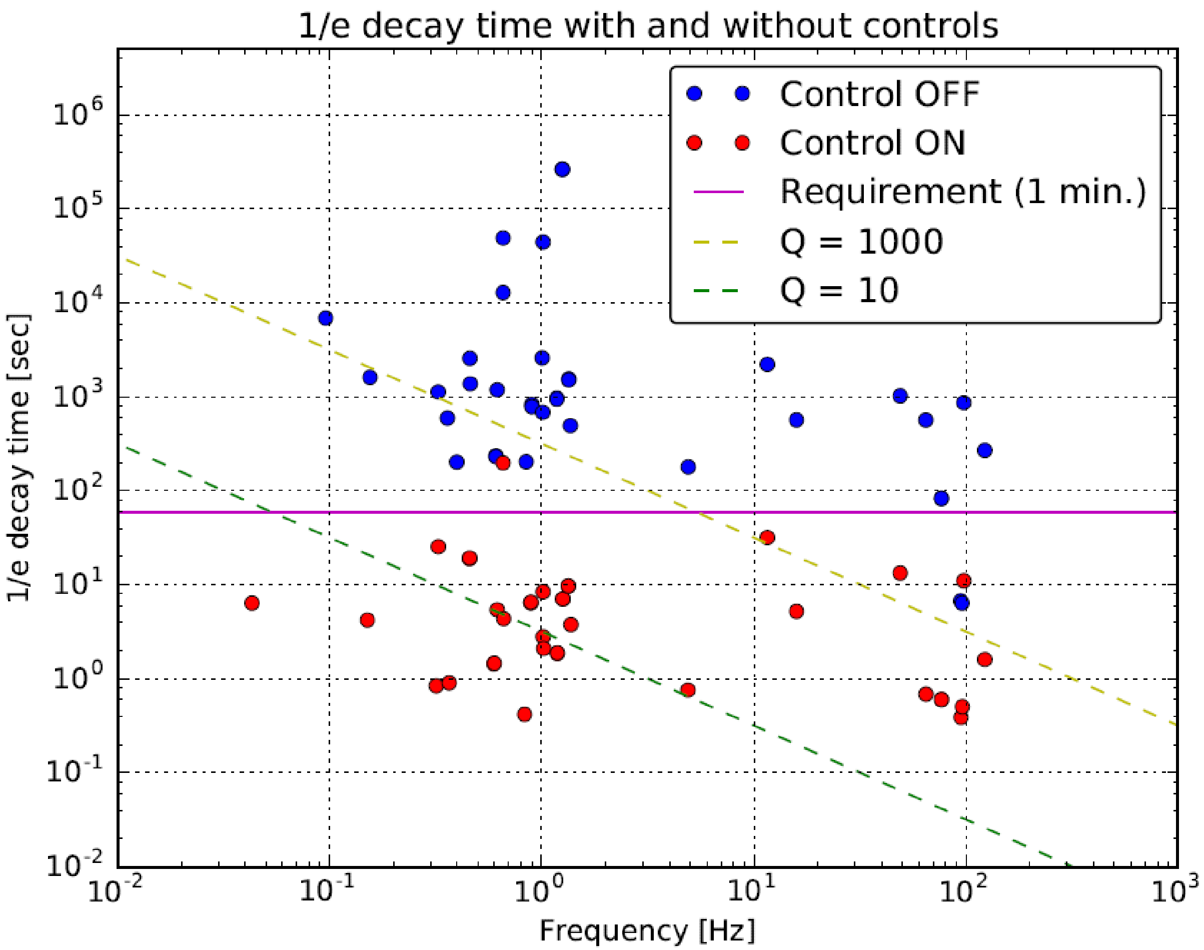


609 sec

To be investigated :
if oplev is available just after large disturbance.

Simulated damping time: Control ON vs. Control OFF

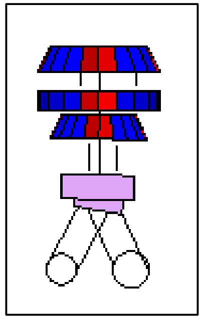
Model



GAS : DC

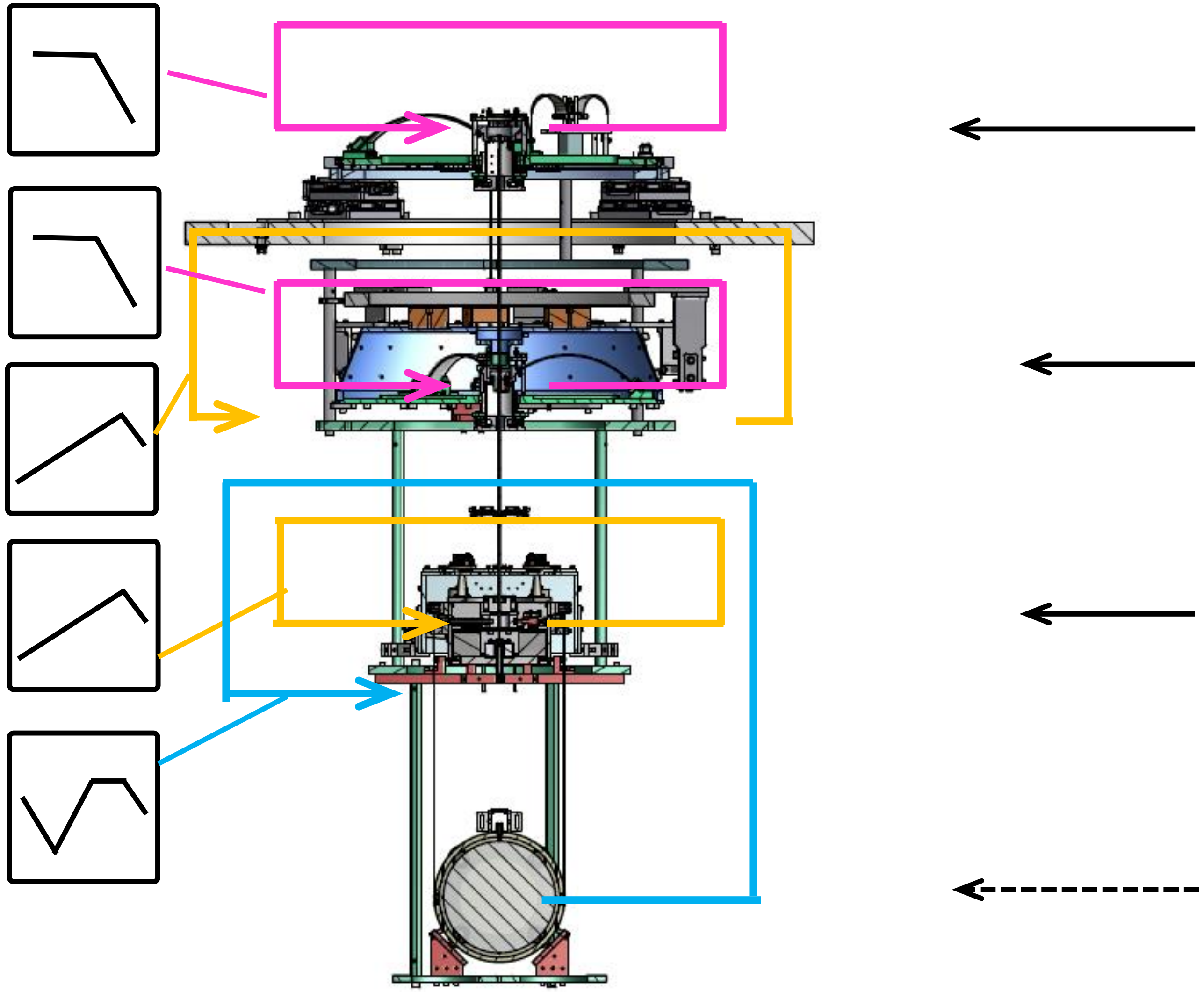
IM : Damping (IMOSEM→ IMOSEM)

TM : Damping (TMoplev → TMOSEM)



198 sec

Control loops in lock-acquisition phase



GAS :
DC control, with LVDT

BF – BR :
Damping control, with small LVDT

IM – IR :
Damping control, with OSEM
(only L, T, V, R)

TM – IM :
DC
+ damping control, with oplev & IM OSEM actuator

(Servo_lock5)

Requirements for control

According to **(below calculation),
the velocity requirement for PR TM is
around~ 7, 8 um/sec.
Thus anyway I set the requirement at 5um/sec.

Making servo filters for the each phase

1. Damping phase
2. Lock-acquisition phase
3. Observation phase
4.

→

Requirement

1. RMS velocity (L) < 5 um/sec.
2. RMS displacement (T, V) < 1 mm
3. RMS displacement (P, Y) < 2 urad

**

$$\text{(Maximum power of actuator)} \times \frac{d_{FWHW}}{\text{RMS velocity}} > M \times \text{(RMS velocity)}$$

4* 0.129 N/A * 136e-3 A

532 nm/57

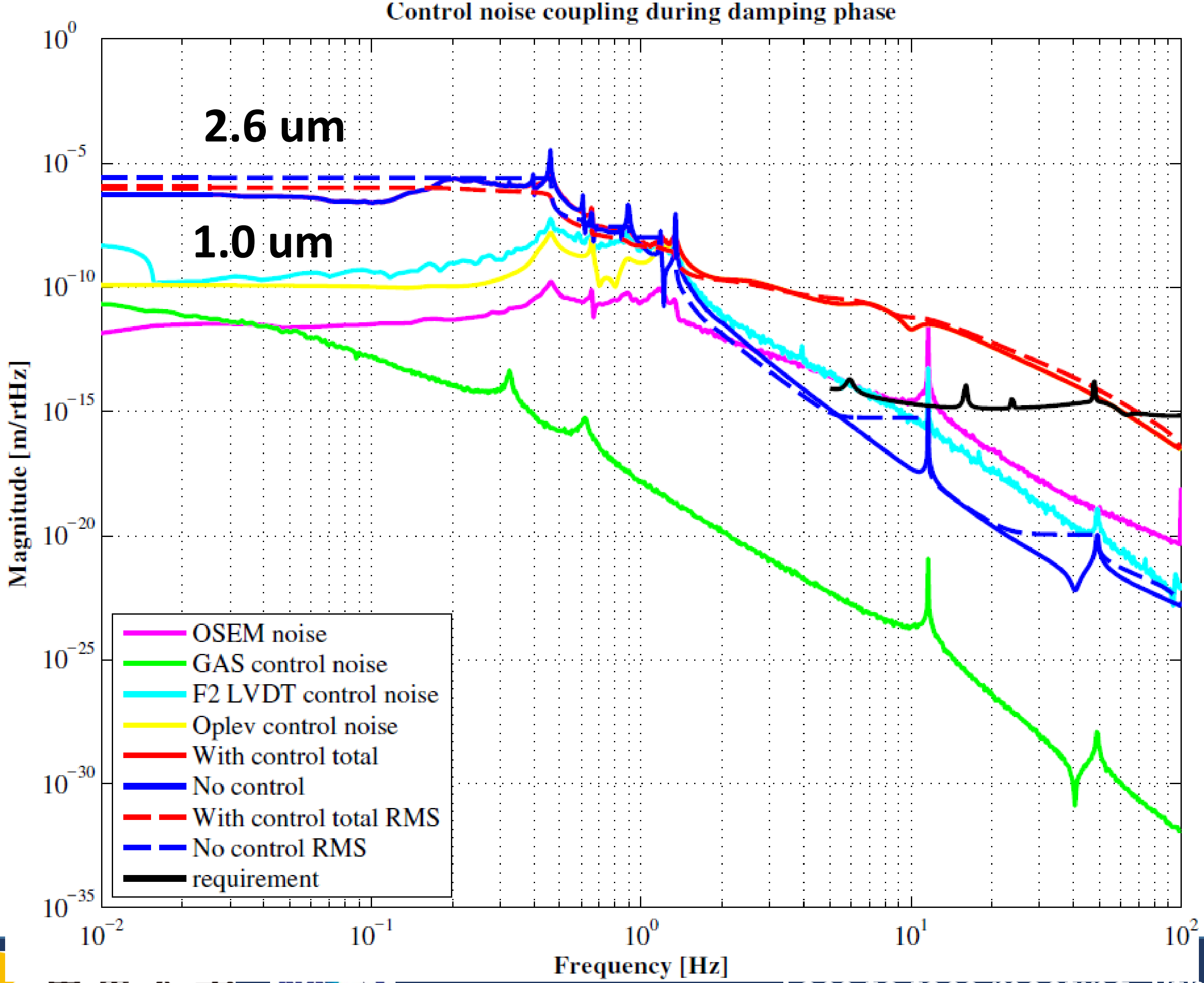
10 kg

→ RMS velocity < 8.1 um/sec

http://gwwiki.icrr.u-tokyo.ac.jp/JGWwiki/KAGRA/Subgroups/VIS/ActuatorDesign

Longitudinal displacement fluctuation with “KamiokaHighNoise”

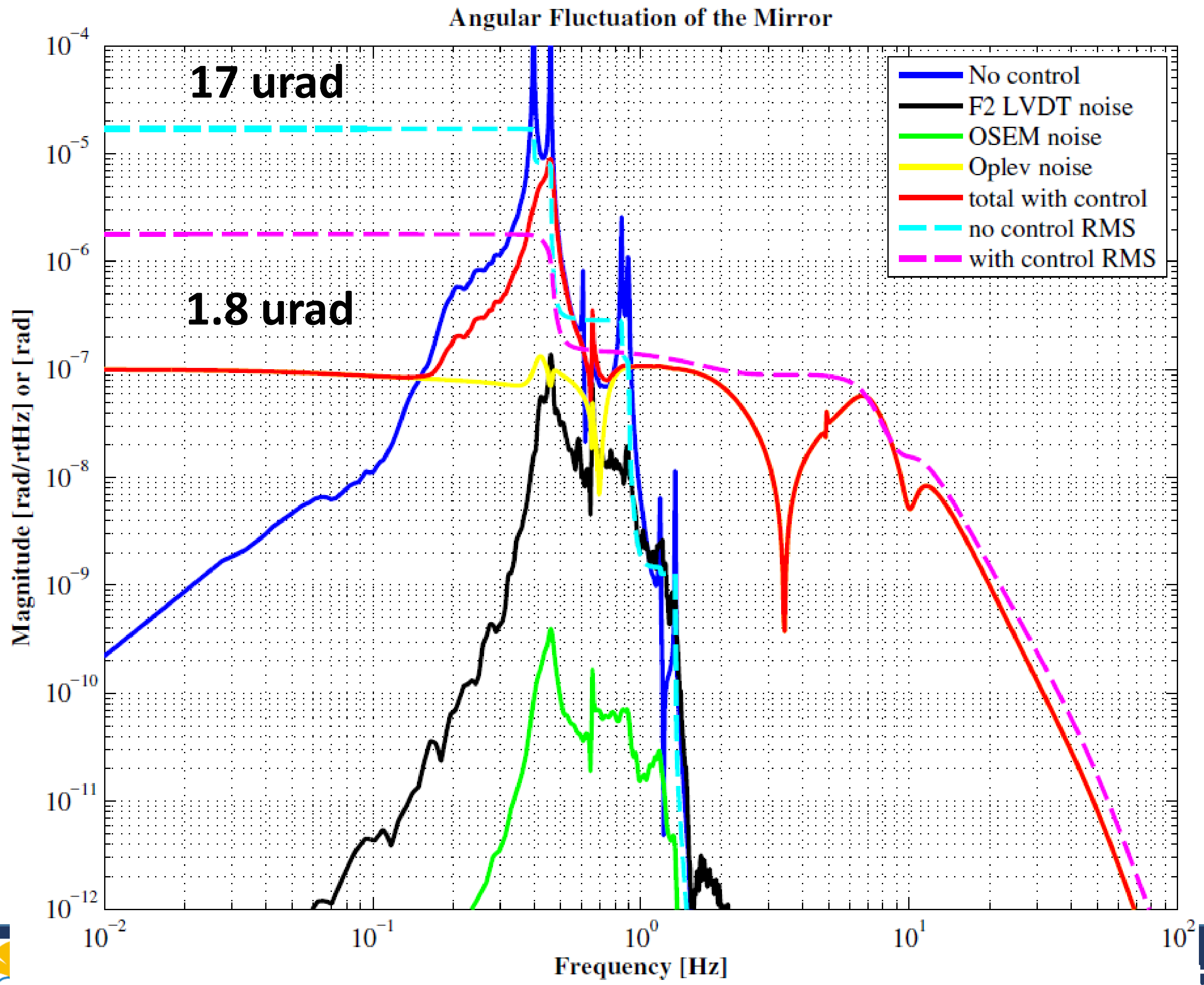
Model



Angular fluctuation (Pitch)

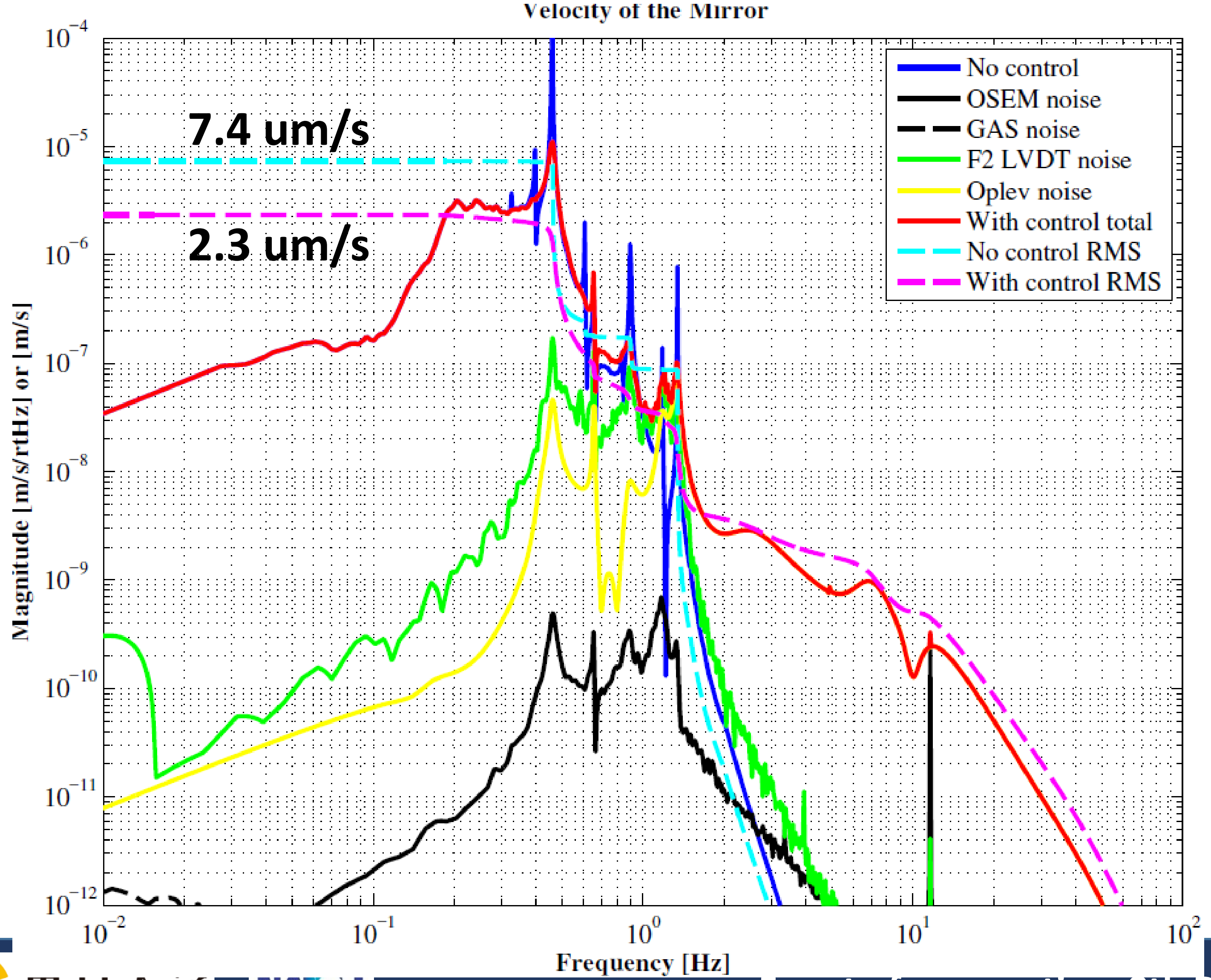
With “KamiokaHighNoise”

Model

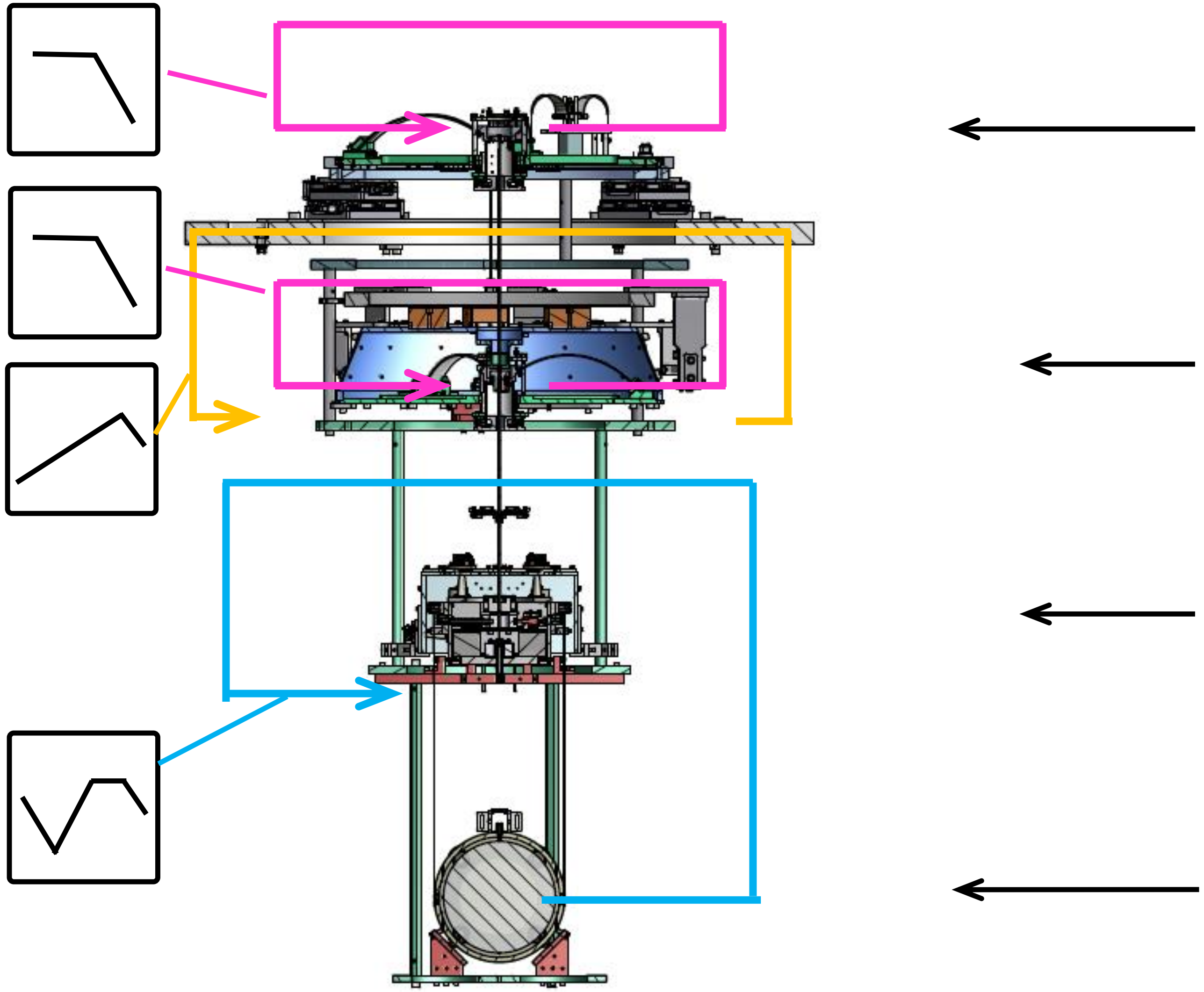


Longitudinal velocity fluctuation with "KamiokaHighNoise"

Model



Control loops in observation phase



GAS :
DC control, with LVDT

BF – BR :
Damping control, with small LVDT

IM – IR :
No control,

TM – IM :
DC
+ damping control, with WFS & IM OSEM actuator

(Servo_obs3)

Requirements for control

Making servo filters for the each phase

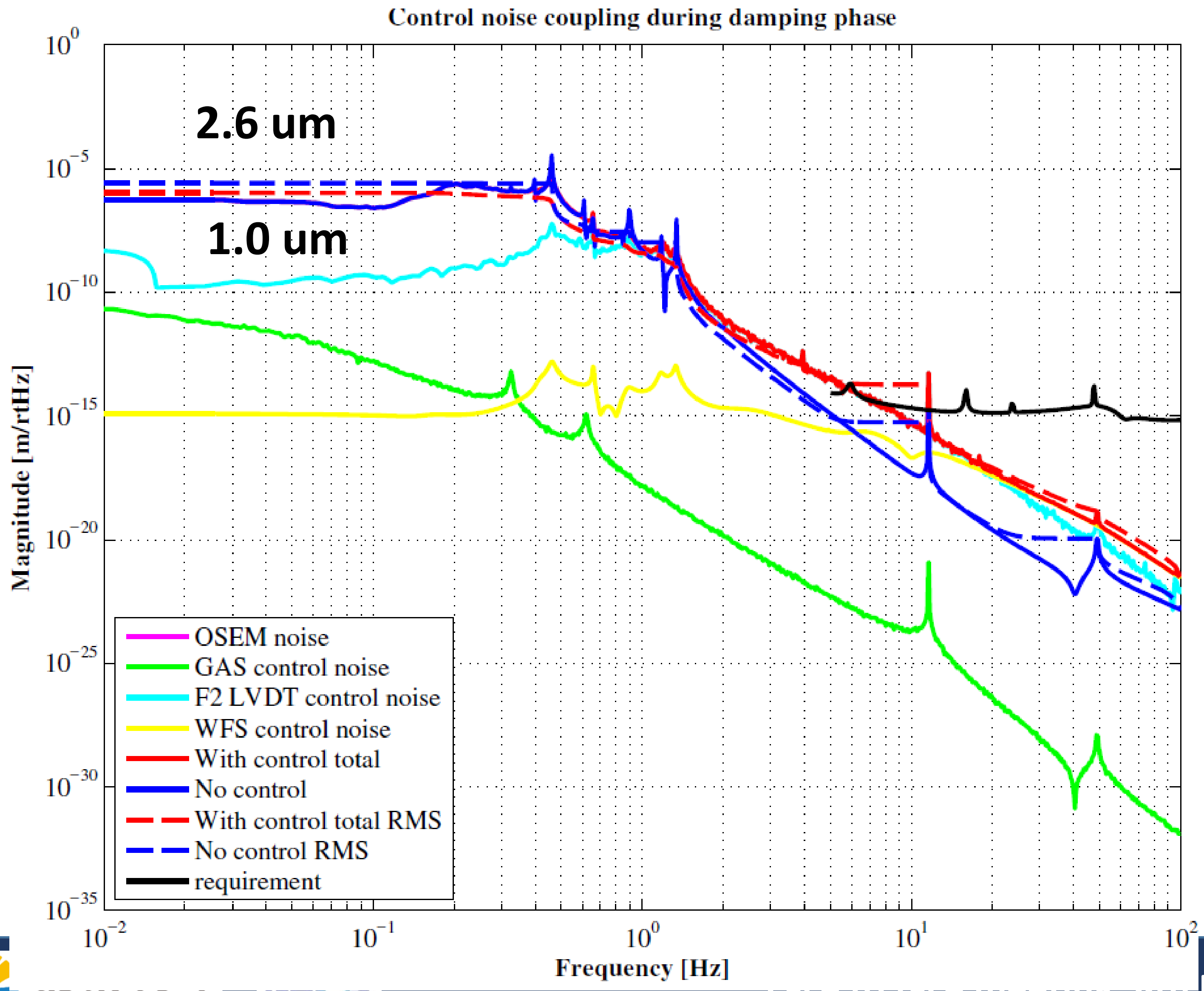
1. Damping phase →
2. Lock-acquisition phase
3. Observation phase
4.

Requirement

1. Displacement (L) < 1e-15 m at 10 Hz
2. RMS displacement (L) < 70 um
3. RMS displacement (T, V) < 1 mm
4. RMS displacement (P, Y) < 2 urad

Longitudinal displacement fluctuation With “KamiokaHighNoise”

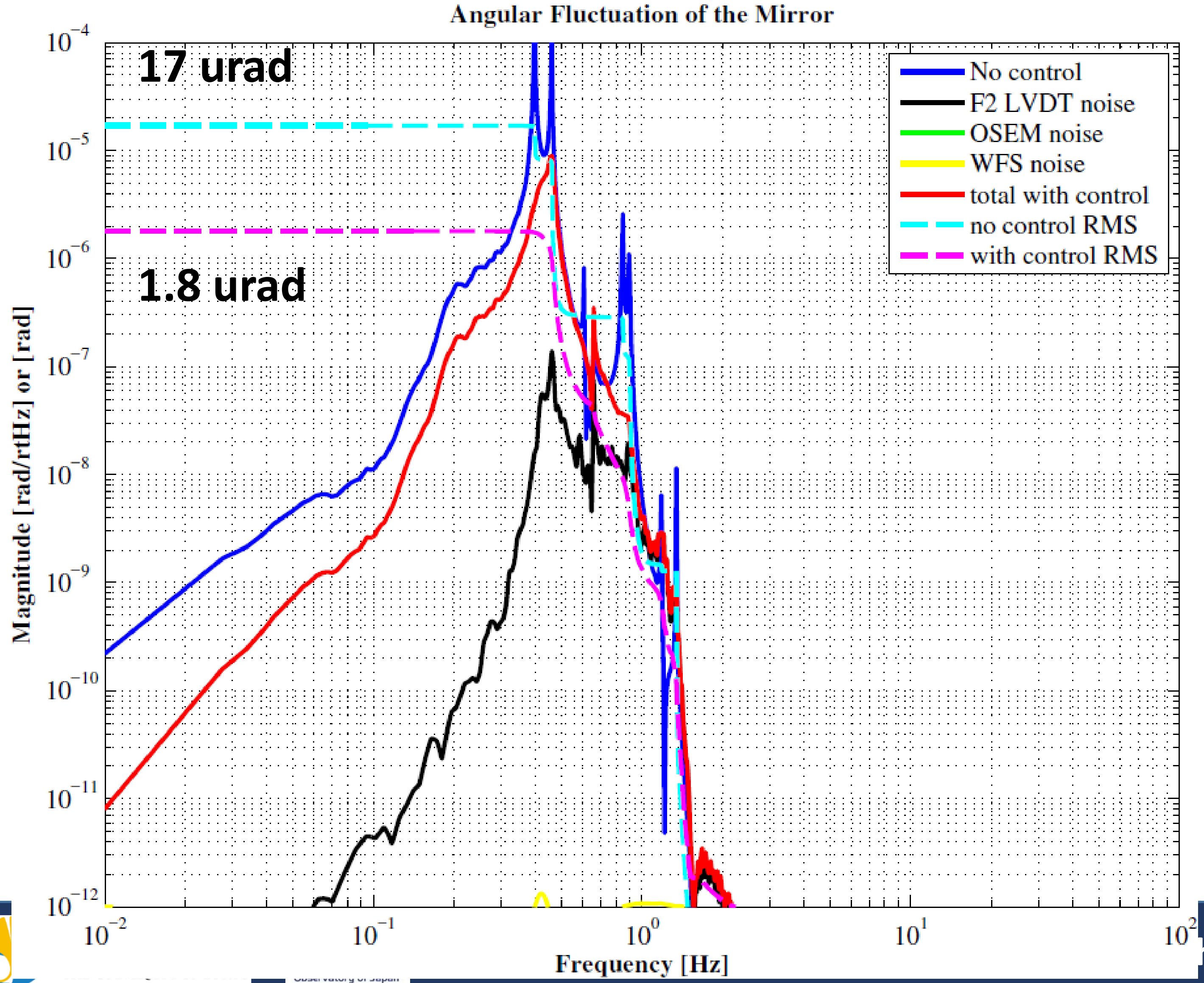
Model



Angular fluctuation (Pitch)

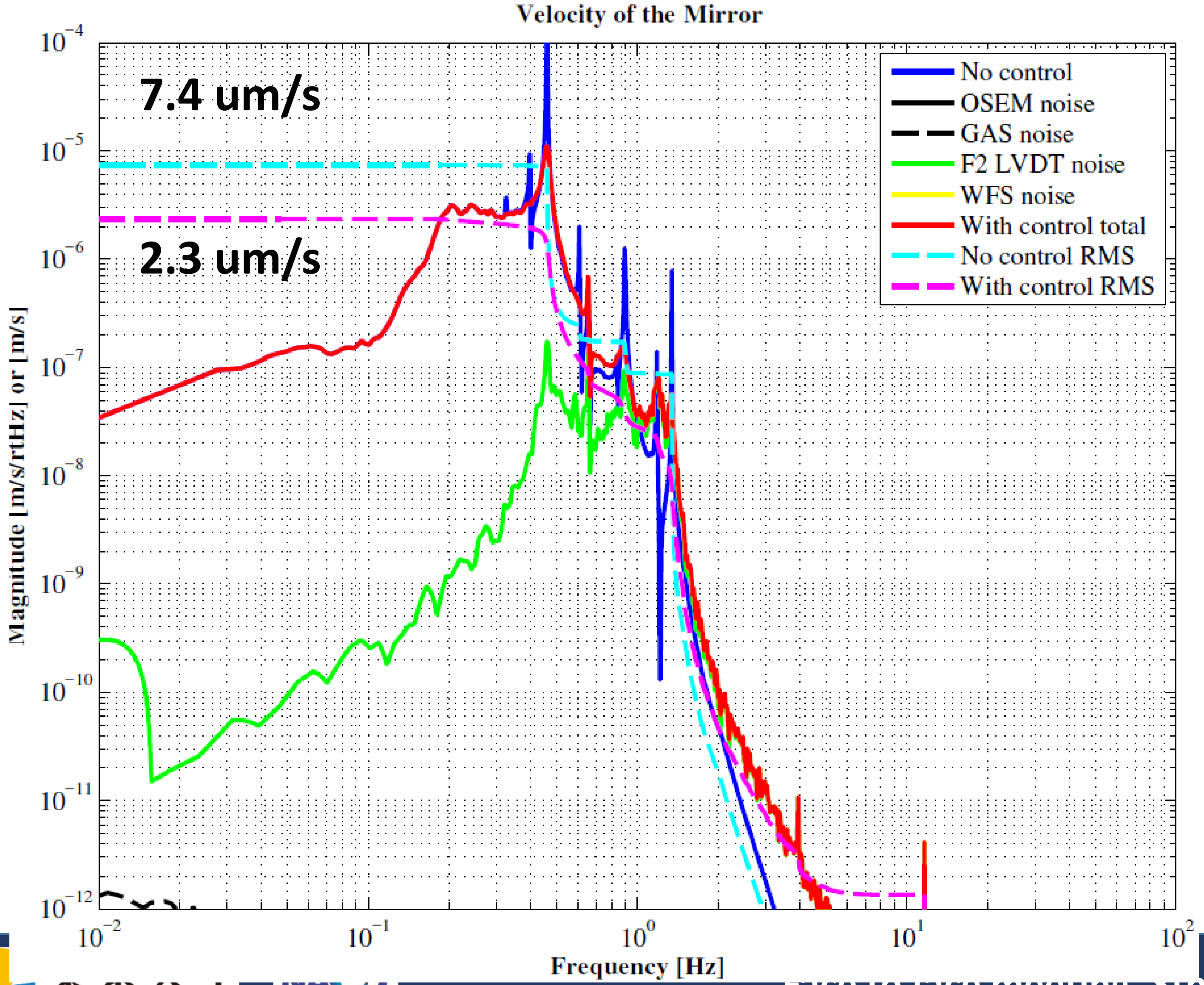
With “KamiokaHighNoise”

Model

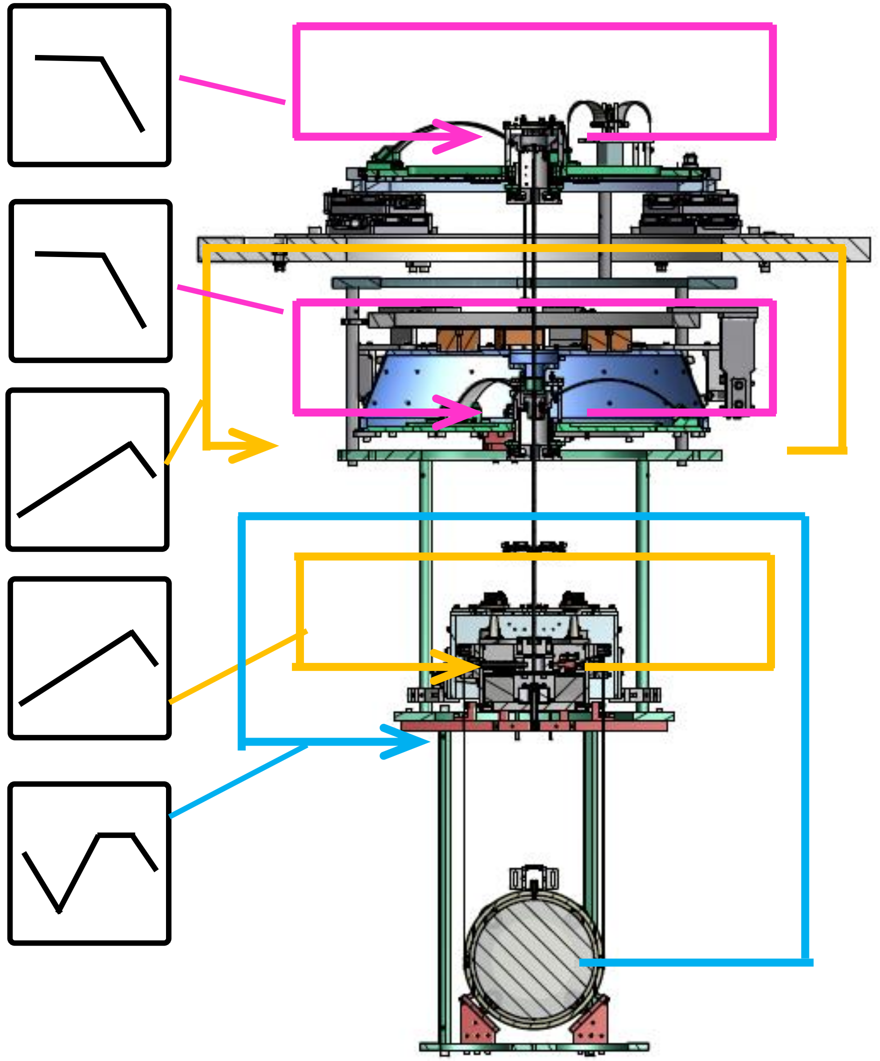


Longitudinal velocity fluctuation

Model



Control loops in observation phase with IM-OSEMs (another option)



GAS :
DC control, with LVDT

BF – BR :
Damping control, with small LVDT

IM – IR :
Damping control, with OSEM
(only L, T, R)

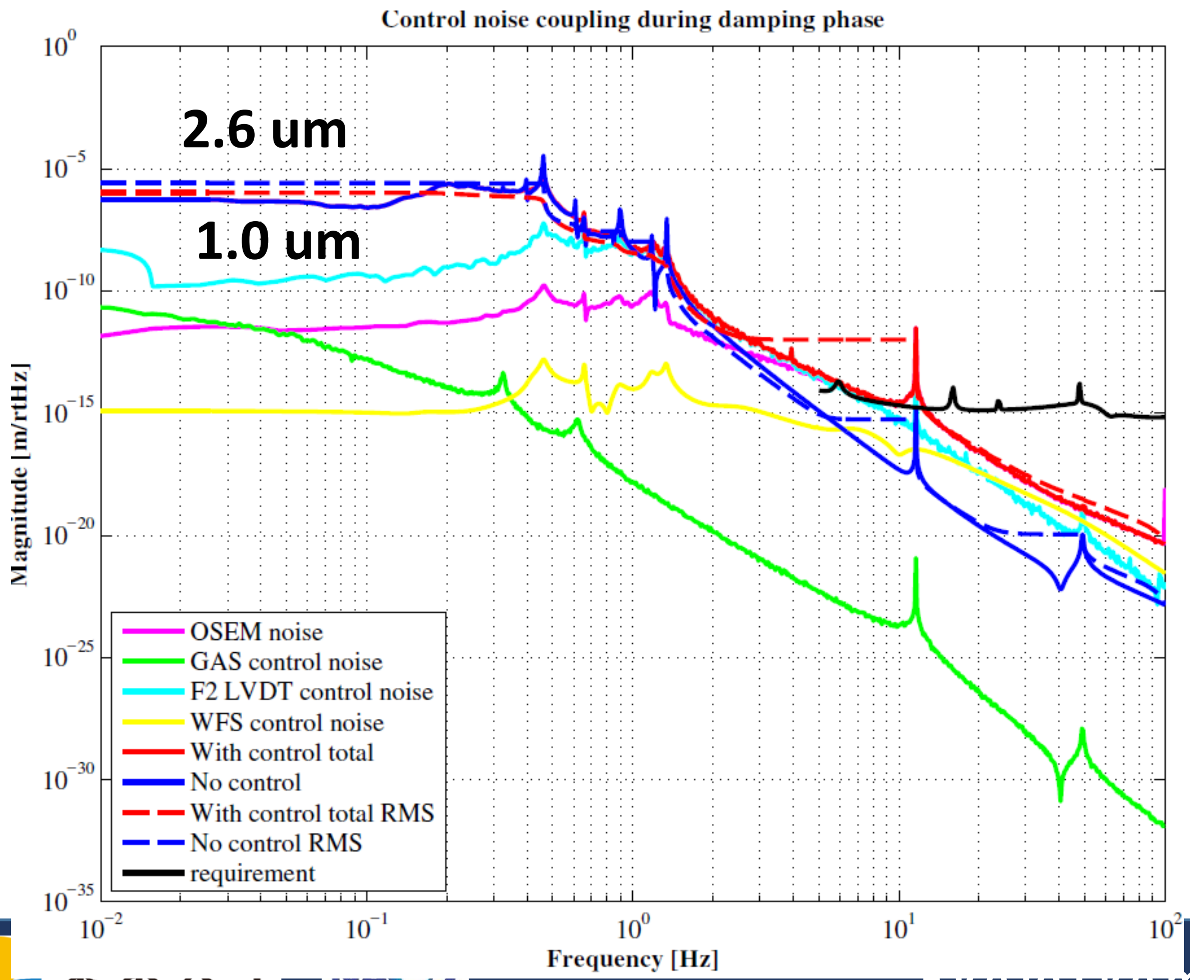
TM – IM :
DC
+ damping control, with WFS & IM OSEM actuator

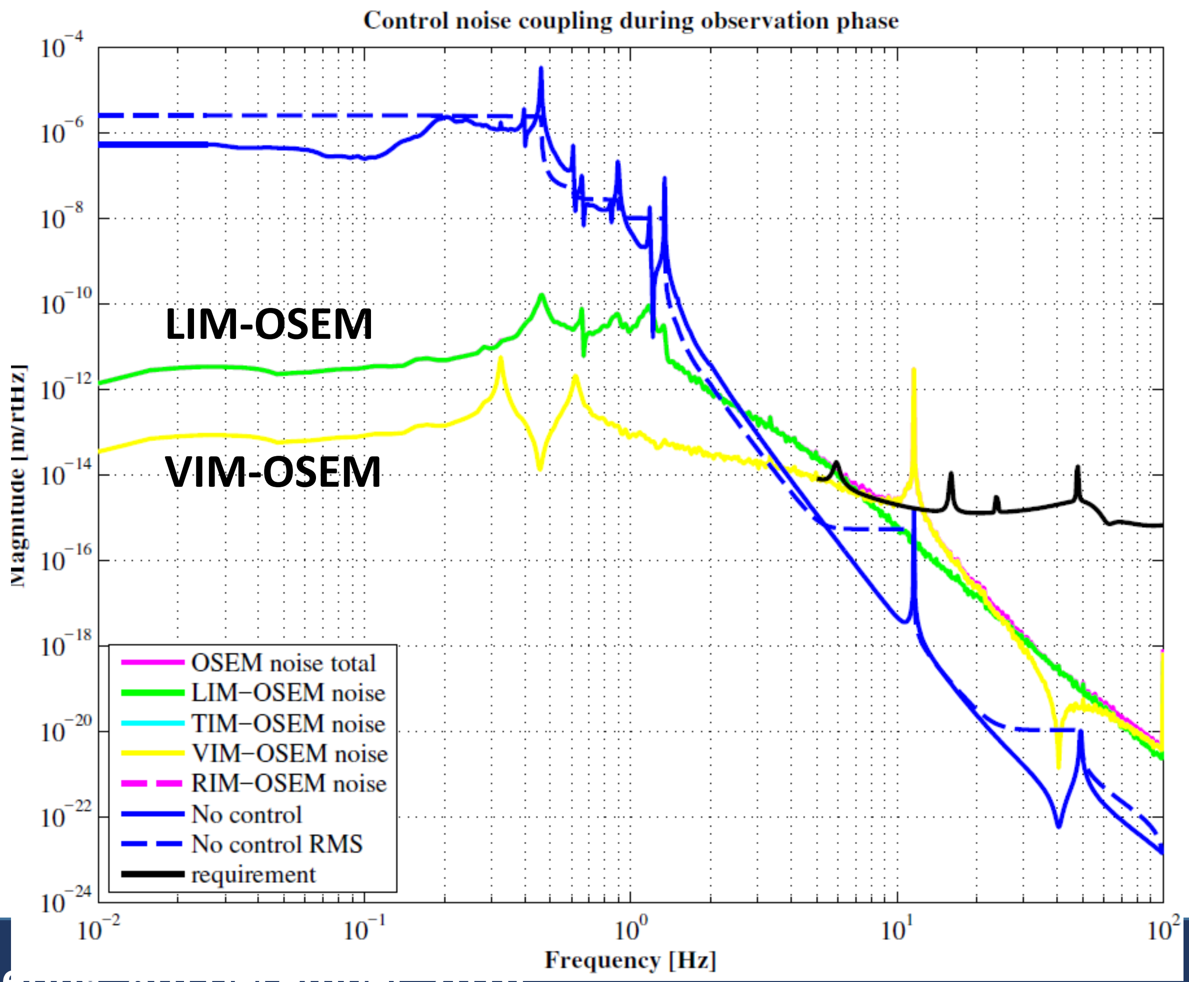
(Servo_obs5)

Longitudinal displacement fluctuation   With "KamiokaHighNoise"

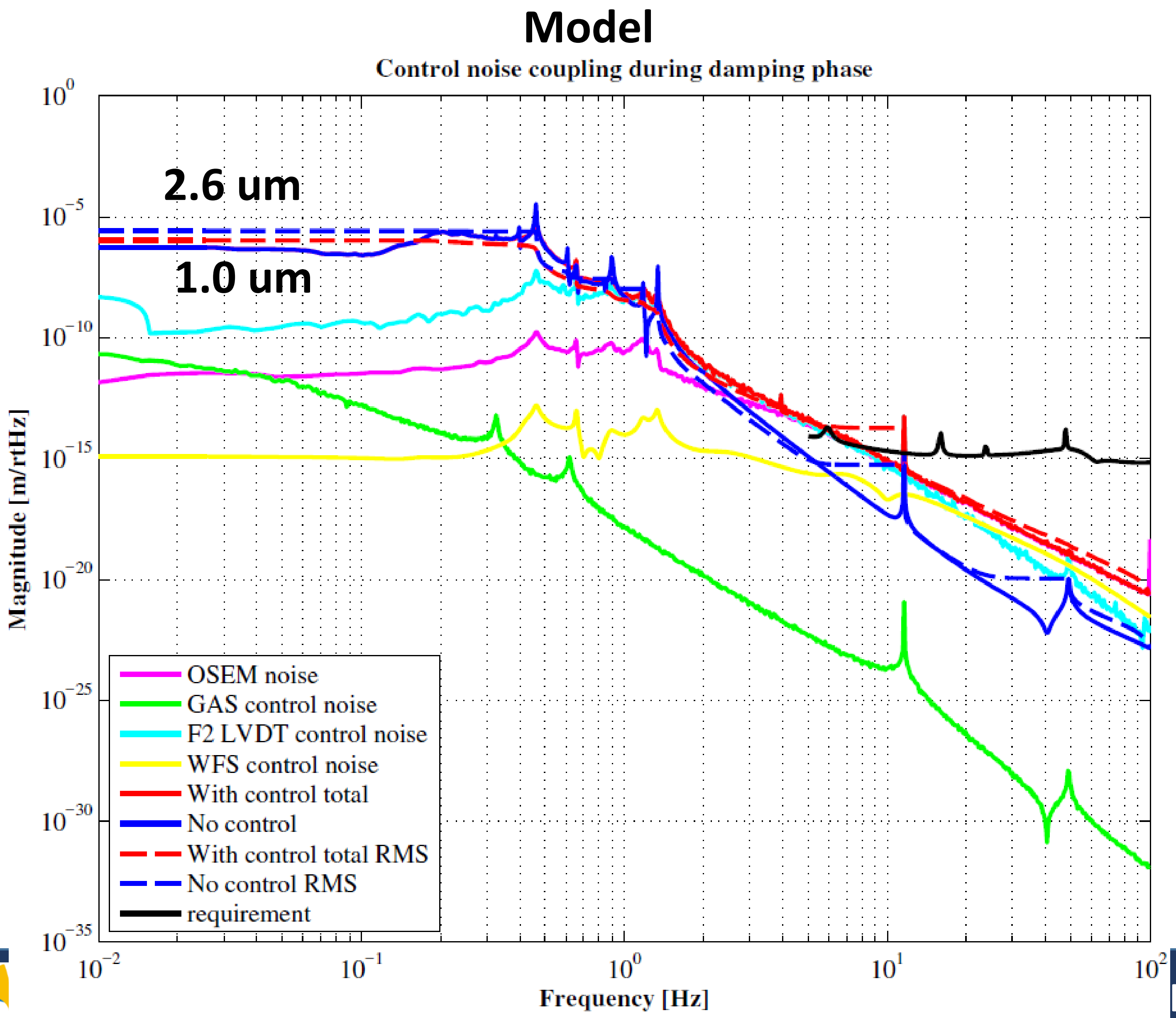
IM – IR : If IM-OSEM damping controls are ON (for L, T, V, R DoF)

Model





Longitudinal displacement fluctuation With “KamiokaHighNoise”

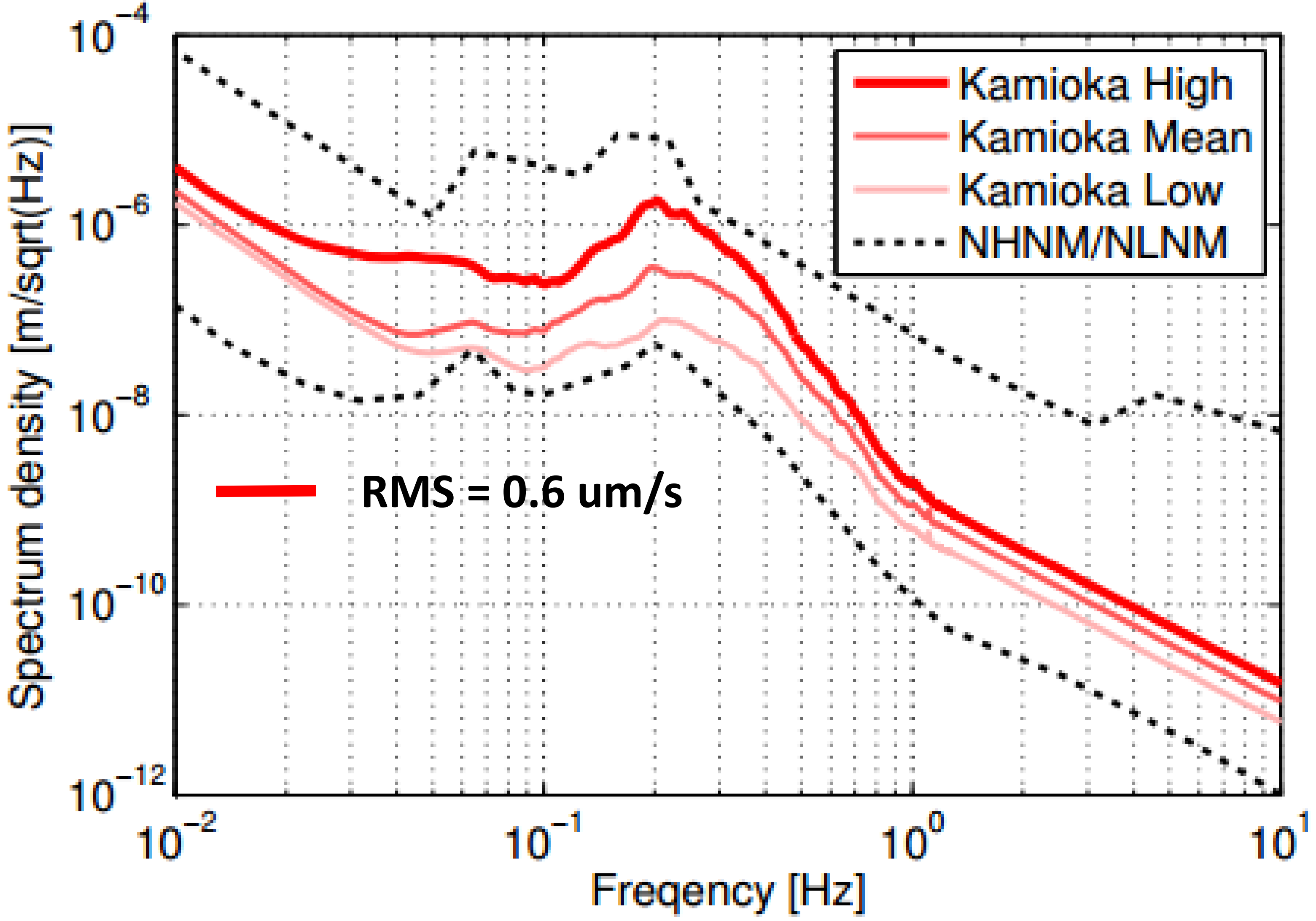


IM – IR :

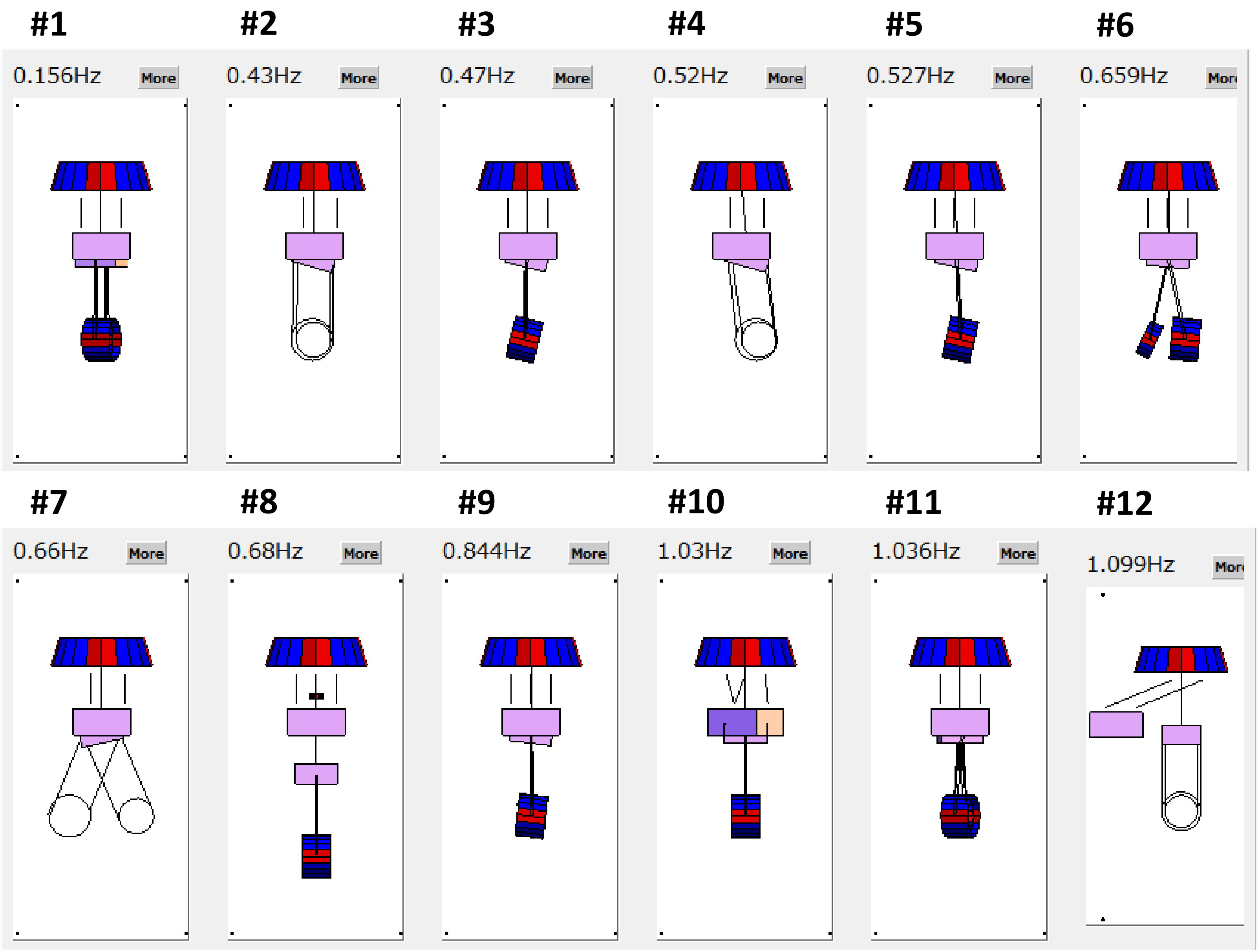
If IM-OSEM damping controls are ON (for L, T, R DoF)

Using OSEM would be available only for type-Bp SAS though, maybe..

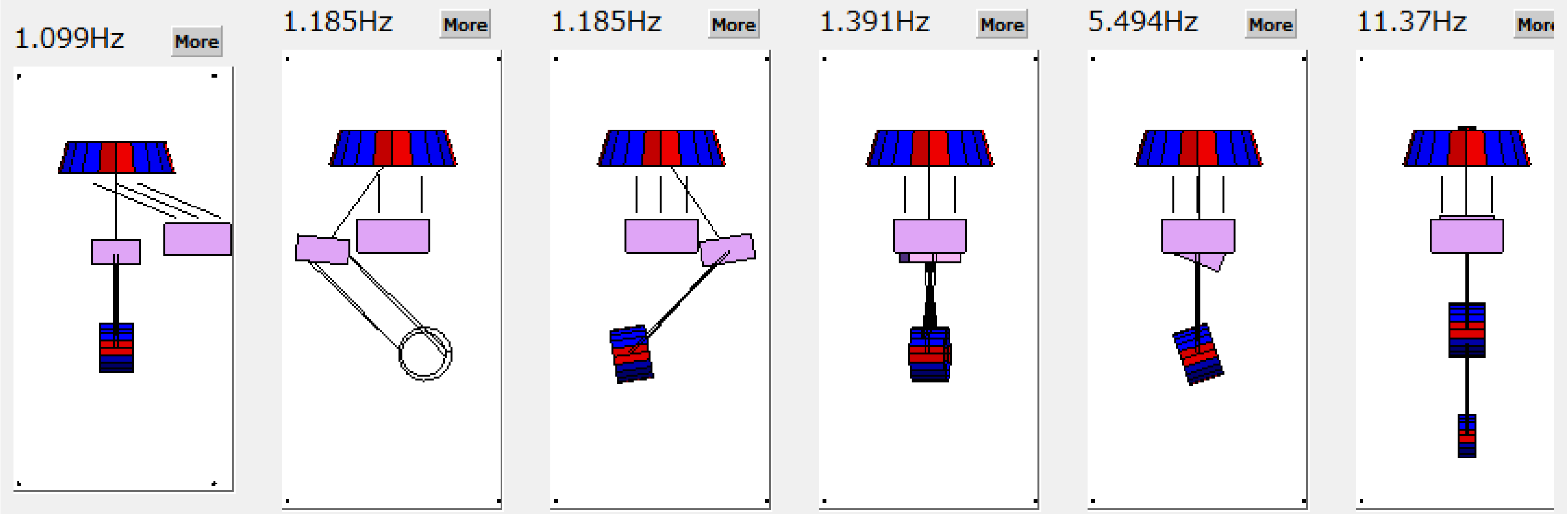
Typical seismic noise of Kamioka:



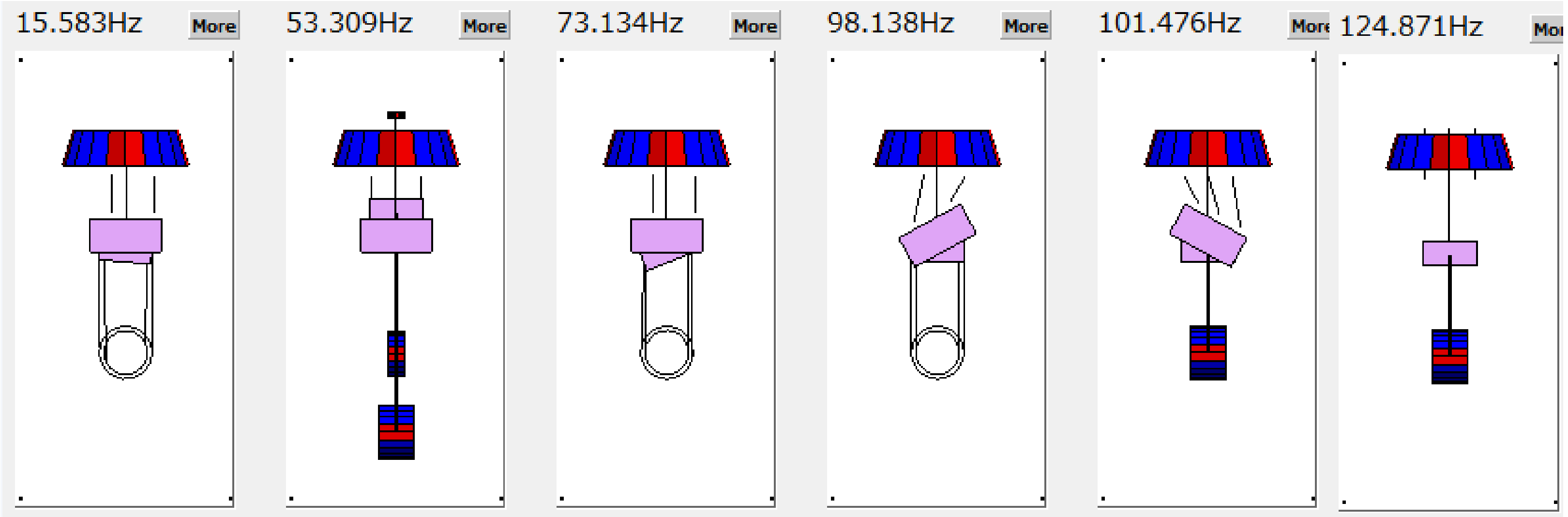
TypeBpp SAS
Eigen mode List : 24 modes



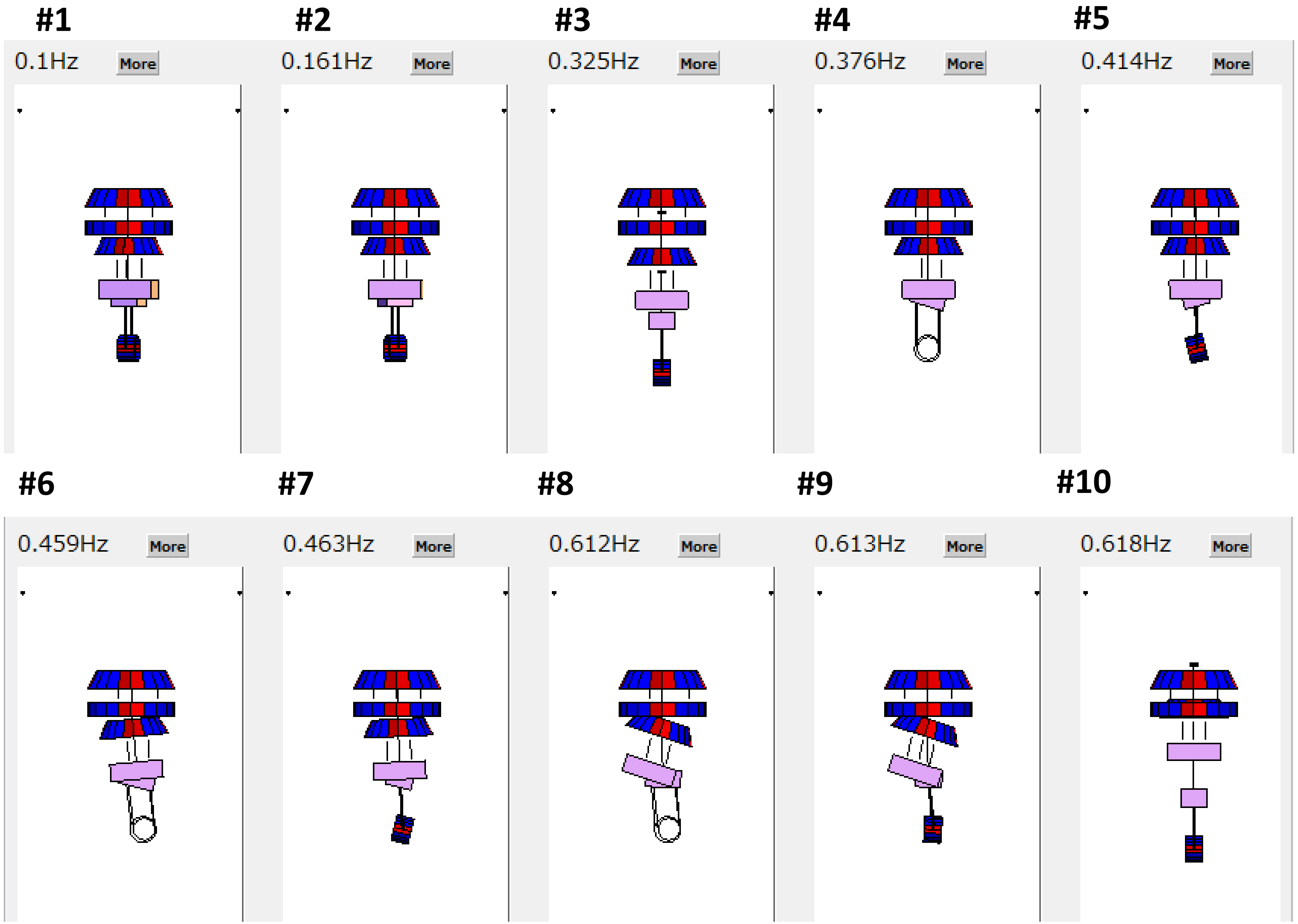
#13 #14 #15 #16 #17 #18

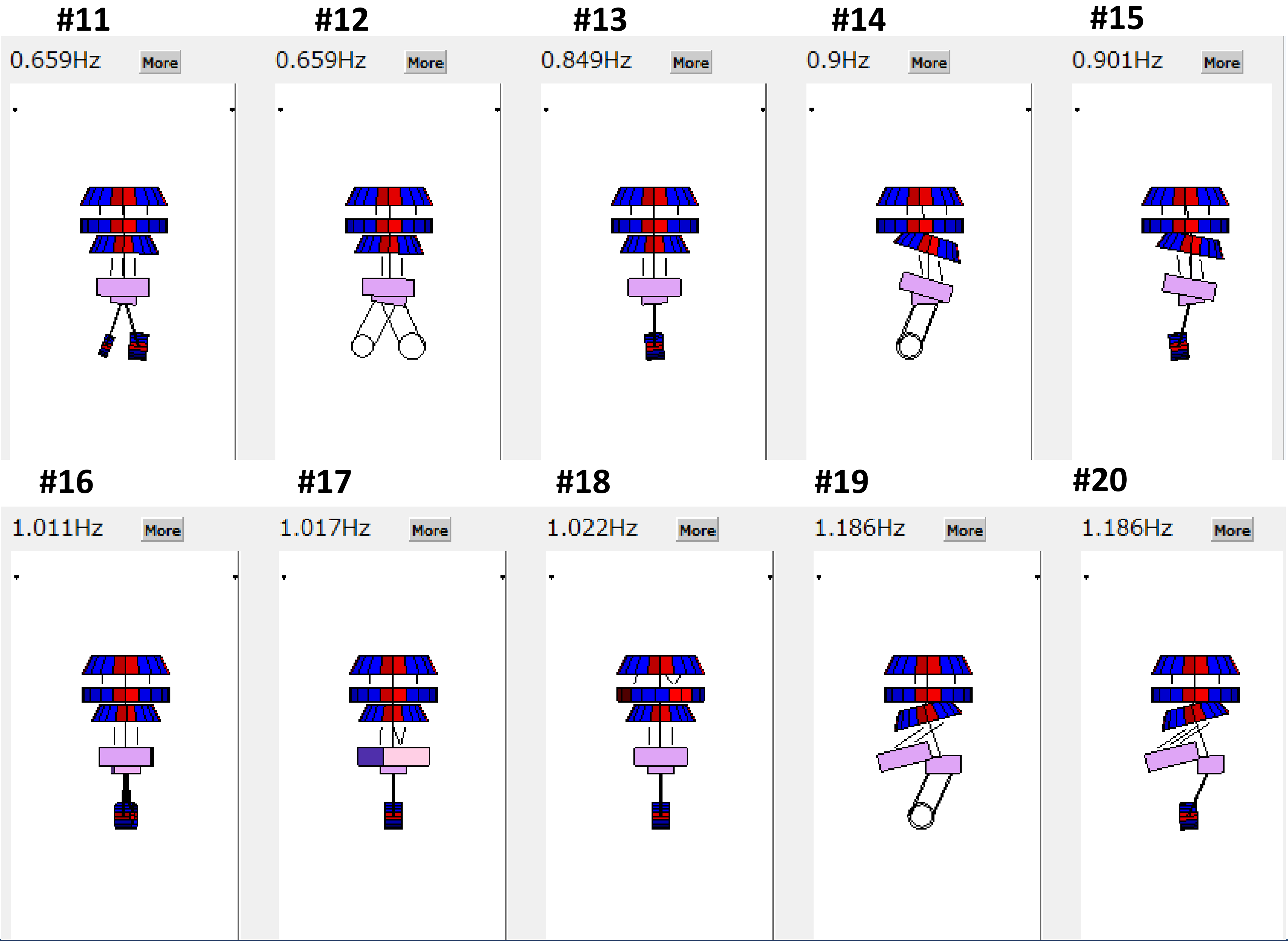


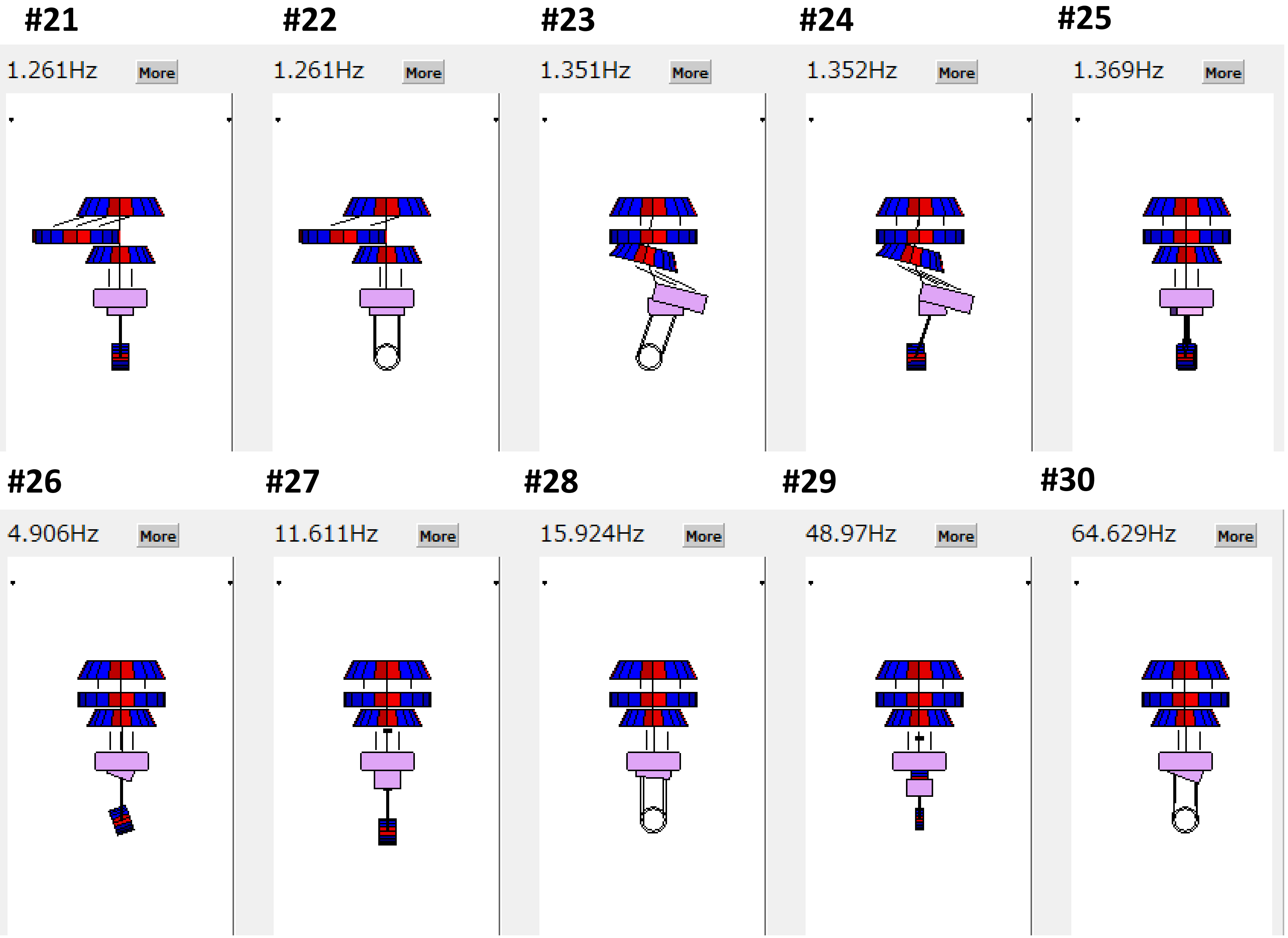
#19 #20 #21 #22 #23 #24



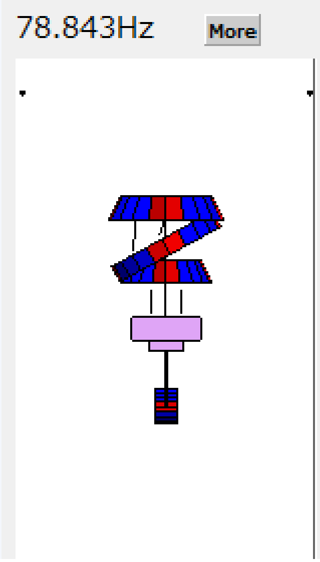
TypeBp SAS
Eigen mode List : 36 modes



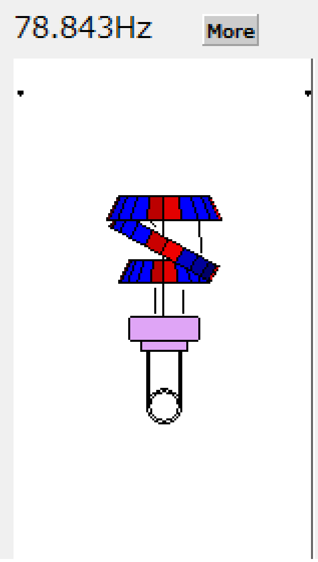

#11
0.659Hz
More
#12
0.659Hz
More
#13
0.849Hz
More
#14
0.9Hz
More
#15
0.901Hz
More
#16
1.011Hz
More
#17
1.017Hz
More
#18
1.022Hz
More
#19
1.186Hz
More
#20
1.186Hz
More


#21
1.261Hz
More
#22
1.261Hz
More
#23
1.351Hz
More
#24
1.352Hz
More
#25
1.369Hz
More
#26
4.906Hz
More
#27
11.611Hz
More
#28
15.924Hz
More
#29
48.97Hz
More
#30
64.629Hz
More

#31



#32



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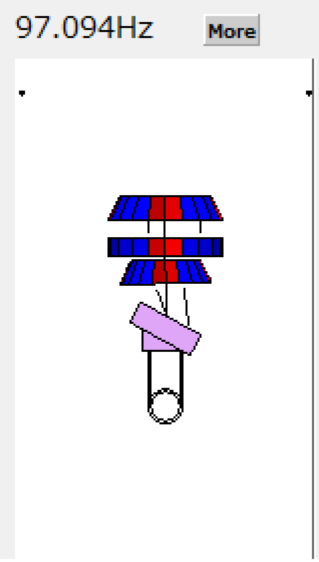
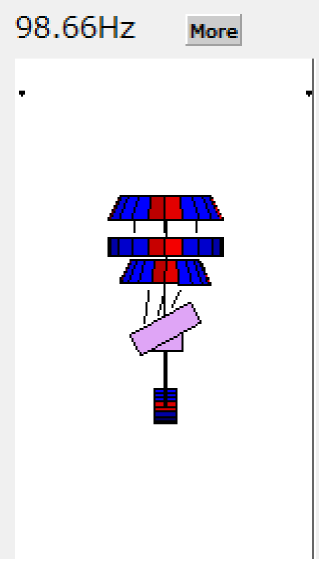
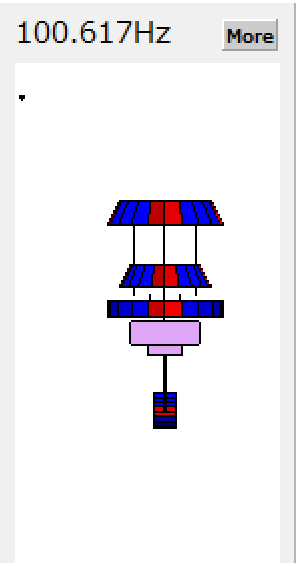


#34



#35



#36