## 1 ITRF94 coordinate system

Reference site: http://vldb.gsi.go.jp/sokuchi/surveycalc/main.html

| Ellipsoid | GRS80 |
| :---: | :---: |
| Semi-major axis | 6378137 m |
| Flattening | $1 / 298.257222101$ |
| Semi-minor axis | $b_{G R S 80}=a_{G R S 80}\left(1-f_{G R S 80}\right)$ |

Height: $H_{e}=H_{o}+H_{g}$ where

$$
H_{e}: \text { ellipsoid height }
$$

$H_{g}:$ geoid height $=$ height of geoid surface from GRS80 surface.
$H_{o}$ : orthometric height $=$ height from geoid surface

The Geospatial Information Authority of Japan gives $H_{g}$ from $(B, L)$ at http://vldb.gsi.go.jp/sokuchi/surveycalc/main.html.
$B$ and $L$ are the latitude and the longitude in the ITRF94 geodesic coordinate system. The 3-D international terrestrial reference system $(X, Y, Z)$ of the position specified by the ITRF94 geodesic coordinate $(B, L)$ are computed by

$$
\begin{align*}
& X=\left(\frac{a_{G R S 80}^{2}}{\sqrt{a_{G R S 80}^{2} \cos ^{2} B+b_{G R S 80}^{2} \sin ^{2} B}}+H_{e}\right) \cos B \cos L,  \tag{1}\\
& Y=\left(\frac{a_{G R S 80}^{2}}{\sqrt{a_{G R S 80}^{2} \cos ^{2} B+b_{G R S 80}^{2} \sin ^{2} B}}+H_{e}\right) \cos B \sin L,  \tag{2}\\
& Z=\left(\frac{b_{G R S 80}^{2}}{\sqrt{a_{G R S 80}^{2} \cos ^{2} B+b_{G R S 80}^{2} \sin ^{2} B}}+H_{e}\right) \sin B \tag{3}
\end{align*}
$$

The Geospatial Information Authority of Japan gives $(X, Y, Z)$ from $(B, L)$ at http://vldb.gsi.go.jp/sokuchi/surveycalc/main.html.

LALDetectors.h requires the azimuth angule $\zeta_{G R S 80}$ and the altitude angle $\mathcal{A}_{G R S 80}$ of the arms. The LALDetector.h document says " The c LALFrDetector structure stores the directions along the two arms of an interferometer in an altitude/azimuth representation with respect to the local tangent plane to the reference ellipsoid, known as the local horizontal. The altitude $\mathcal{A}$ is the angle the direction vector makes with the horizontal, $\mathcal{A}>0$ meaning above horizontal, $\mathcal{A}<0$ below. The azimuth angle $\zeta$ is found by projecting the direction onto the local horizontal plane, then measuring the angle clockwise from North to this projected direction.".

Define the following vectors. $\vec{u}$ is the unit vector from the BS to the X-End. $\vec{v}$ is the unit vector from the BS to the Y-End. $\vec{n}$ is the normal unit vector to
the local horizontal at the BS. $\vec{m}$ is the unit vector on the local horizontal at the BS and directed to the local North. $\vec{l}$ is the unit vector on the local horizontal at the BS and directed to the local East $(\vec{l}=\vec{m} \times \vec{n})$.

Then the azimuth angule $\zeta_{G R S 80}$ and the altitude angle $\mathcal{A}_{G R S 80}$ are defined by

$$
\begin{align*}
& \vec{n}=(\cos L \cos B, \sin L \cos B, \sin B),  \tag{4}\\
& \vec{m}=(-\cos L \sin B,-\sin L \sin B, \cos B),  \tag{5}\\
& \vec{l}=(\sin L,-\cos L, 0),  \tag{6}\\
& \sin \left(\mathcal{A}_{G R S 80, X-a r m}\right)=\vec{n} \cdot \vec{u},  \tag{7}\\
& \tan \zeta_{G R S 80, X-a r m}=\frac{\vec{l} \cdot \vec{u}}{\vec{m} \cdot \vec{u}},  \tag{8}\\
& \sin \left(\mathcal{A}_{G R S 80, Y-a r m}\right)=\vec{n} \cdot \vec{v},  \tag{9}\\
& \tan \zeta_{G R S 80, Y-a r m}=\frac{\vec{l} \cdot \vec{v}}{\vec{m} \cdot \vec{v}} \tag{10}
\end{align*}
$$

For KAGRA, it turns out that $\zeta_{G R S 80, X-a r m}>0$ (X-arm is directed to the local North East) and $\zeta_{G R S 80, Y-a r m}<0$ (Y-arm is directed to the local North West). Then it was checked that $\zeta_{G R S 80, X-a r m}-\zeta_{G R S 80, Y-a r m}-\pi / 2=4 \times 10^{-6}$ radians.

The locations of the KAGRA mirrors are given by Prof. Yoshio Saito (the KAGRA project manager) as the document JGW-G140105-v1 (2014) and shown in the Tables 1, 2 , and 3 .

Table 1: Beam Splitter.

| B [ddmmss] | L [dddmmss] | $H_{e}[\mathrm{~m}]$ | $H_{g}[\mathrm{~m}]$ | $H_{o}[\mathrm{~m}]$ |
| :---: | :---: | :---: | :---: | :---: |
| 362442.69722 | 1371821.44171 | 414.181 | 41.0464 | 373.135 |
| B [radians] | L [radians] | $X[\mathrm{~m}]$ | $Y[\mathrm{~m}]$ | $Z[\mathrm{~m}]$ |
| 0.6355068497 | 2.396441015 | -3777336.024 | 3484898.411 | 3765313.697 |

Table 2: X-End.

| B [ddmmss] | L [dddmmss] | $H_{e}[\mathrm{~m}]$ | $H_{g}[\mathrm{~m}]$ | $H_{o}[\mathrm{~m}]$ |
| :---: | :---: | :---: | :---: | :---: |
| 362531.18475 | 1372007.07060 | 424.407 | 41.1788 | 383.228 |
| B [radians] | L [radians] | $X[\mathrm{~m}]$ | $Y[\mathrm{~m}]$ | $Z[\mathrm{~m}]$ |
| 0.6357419239 | 2.396953119 | -3778473.700 | 3482367.772 | 3766522.541 |

Table 3: Y-End.

| B [ddmmss] | L [dddmmss] | $H_{e}[\mathrm{~m}]$ | $H_{g}[\mathrm{~m}]$ | $H_{o}[\mathrm{~m}]$ |
| :---: | :---: | :---: | :---: | :---: |
| 362607.96387 | 1371721.48451 | 403.934 | 40.8740 | 363.06 |
| B [radians] | L [radians] | $X[\mathrm{~m}]$ | $Y[\mathrm{~m}]$ | $Z[\mathrm{~m}]$ |
| 0.6359202341 | 2.396150335 | -3775170.073 | 3484932.092 | 3767422.582 |

Table 4: X-arm: $\vec{U}=$ (X-end) - (Beam Splitter)

| $U_{x}[\mathrm{~m}]$ | $U_{y}[\mathrm{~m}]$ | $U_{z}[\mathrm{~m}]$ | $\|\vec{U}\|[\mathrm{m}]$ |
| :---: | :---: | :---: | :---: |
| -1137.676 | -2530.639 | 1208.844 | 3026.507 |
| $\vec{u}_{x}$ | $\vec{u}_{y}$ | $\vec{u}_{z}$ | $\|\vec{u}\|$ |
| -0.3759040 | -0.8361583 | 0.3994189 | 1.0000000 |
| $\mathcal{A}_{G R S 80}$ [radians] | $\zeta_{G R S 80}$ [radians] | - | - |
| 0.0031414 | 1.054113 | - | - |

Table 5: Y-arm: $\vec{V}=$ (Y-end) - (Beam Splitter)

| $V_{x}[\mathrm{~m}]$ | $V_{y}[\mathrm{~m}]$ | $V_{z}[\mathrm{~m}]$ | $\|\vec{V}\|[\mathrm{m}]$ |
| :---: | :---: | :---: | :---: |
| 2165.951 | 33.681 | 2108.885 | 3023.222 |
| $\vec{v}_{x}$ | $\vec{v}_{y}$ | $\vec{v}_{z}$ | $\|\vec{v}\|$ |
| 0.7164378 | 0.01114076 | 0.6975620 | 1.0000000 |
| $\mathcal{A}_{G R S 80}$ [radians] | $\zeta_{G R S 80}$ [radians] | - | - |
| -0.0036270 | -0.5166798 | - | - |

