

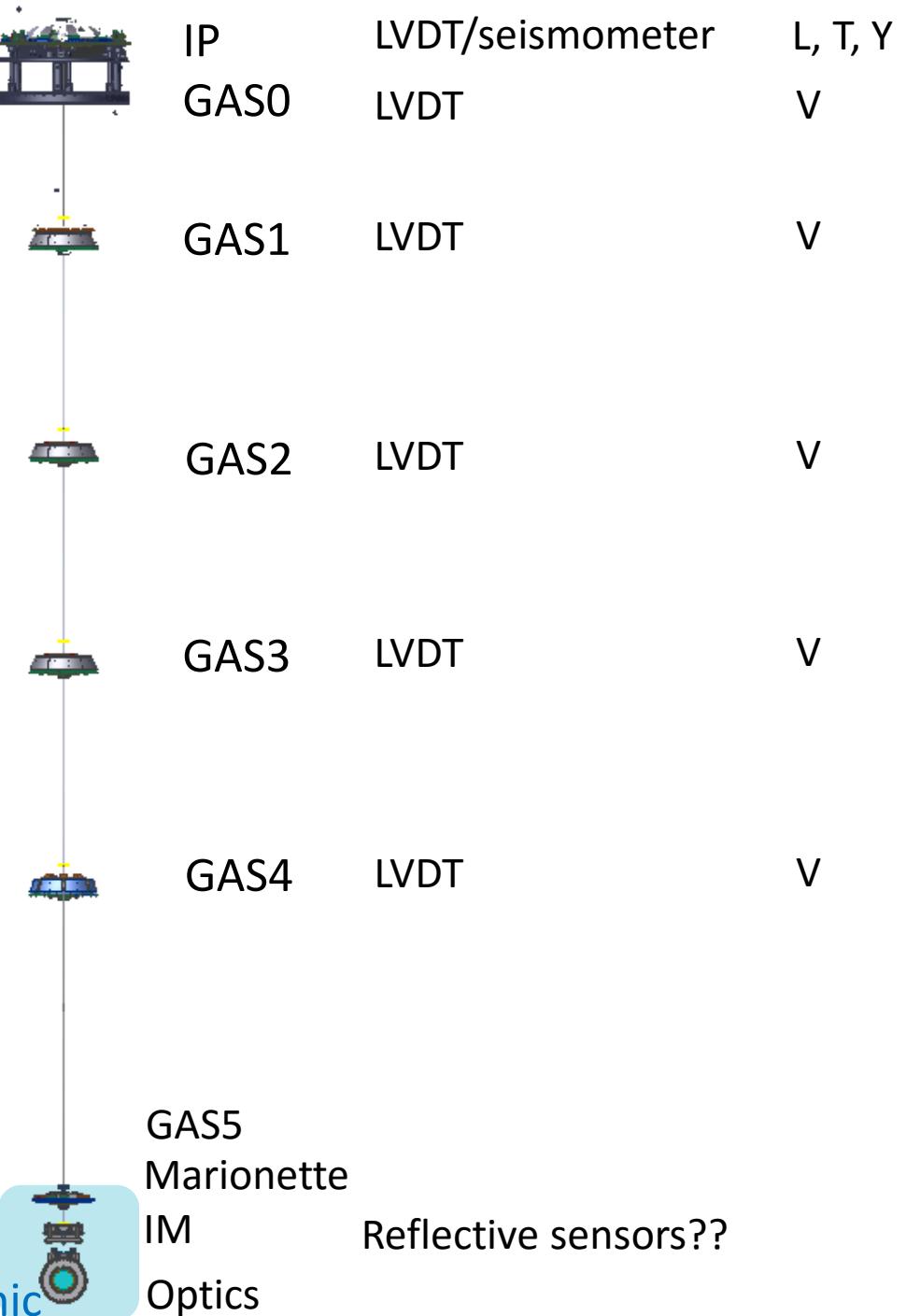
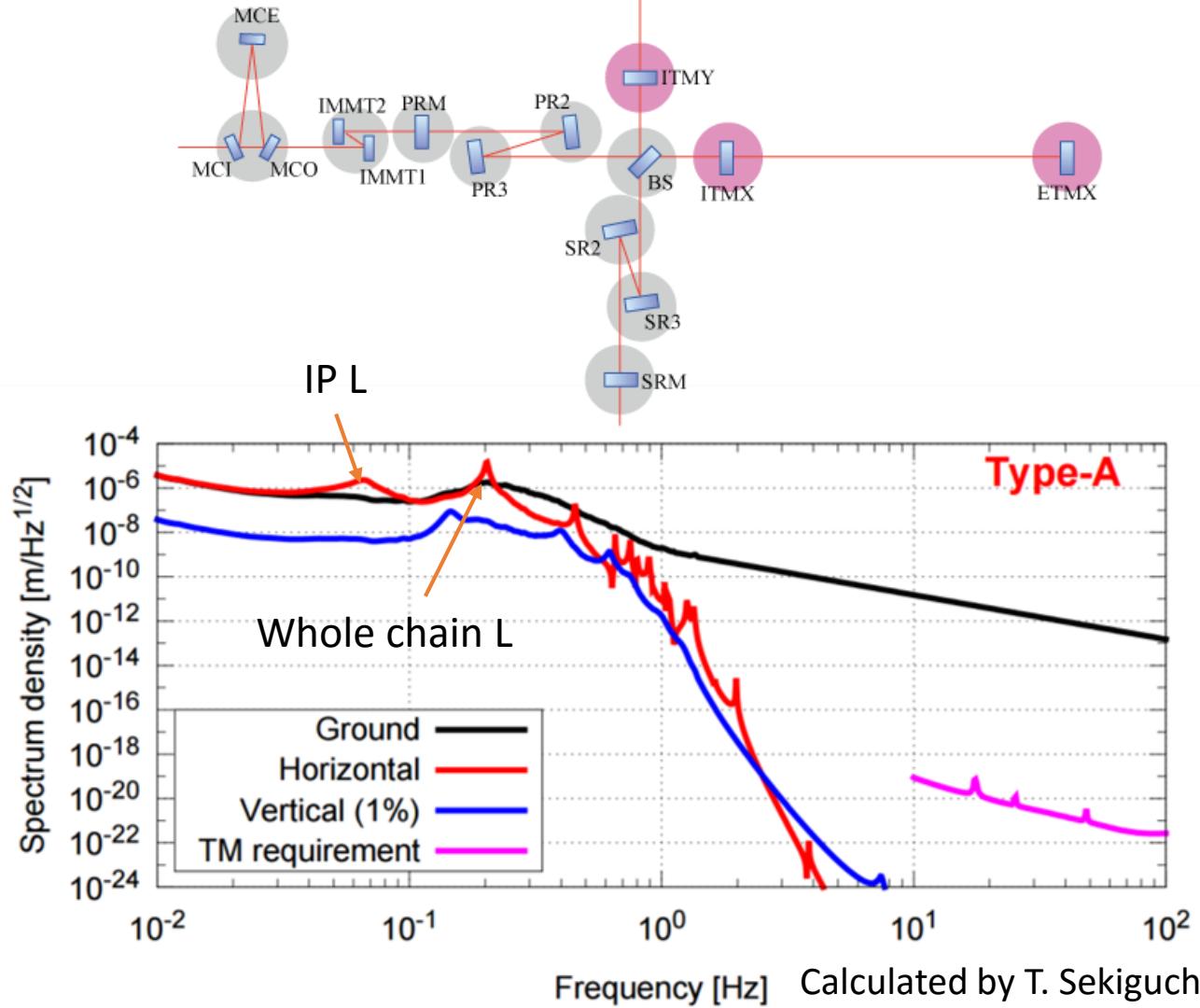
# Damping control for KAGRA suspensions

# Requirement for the damping

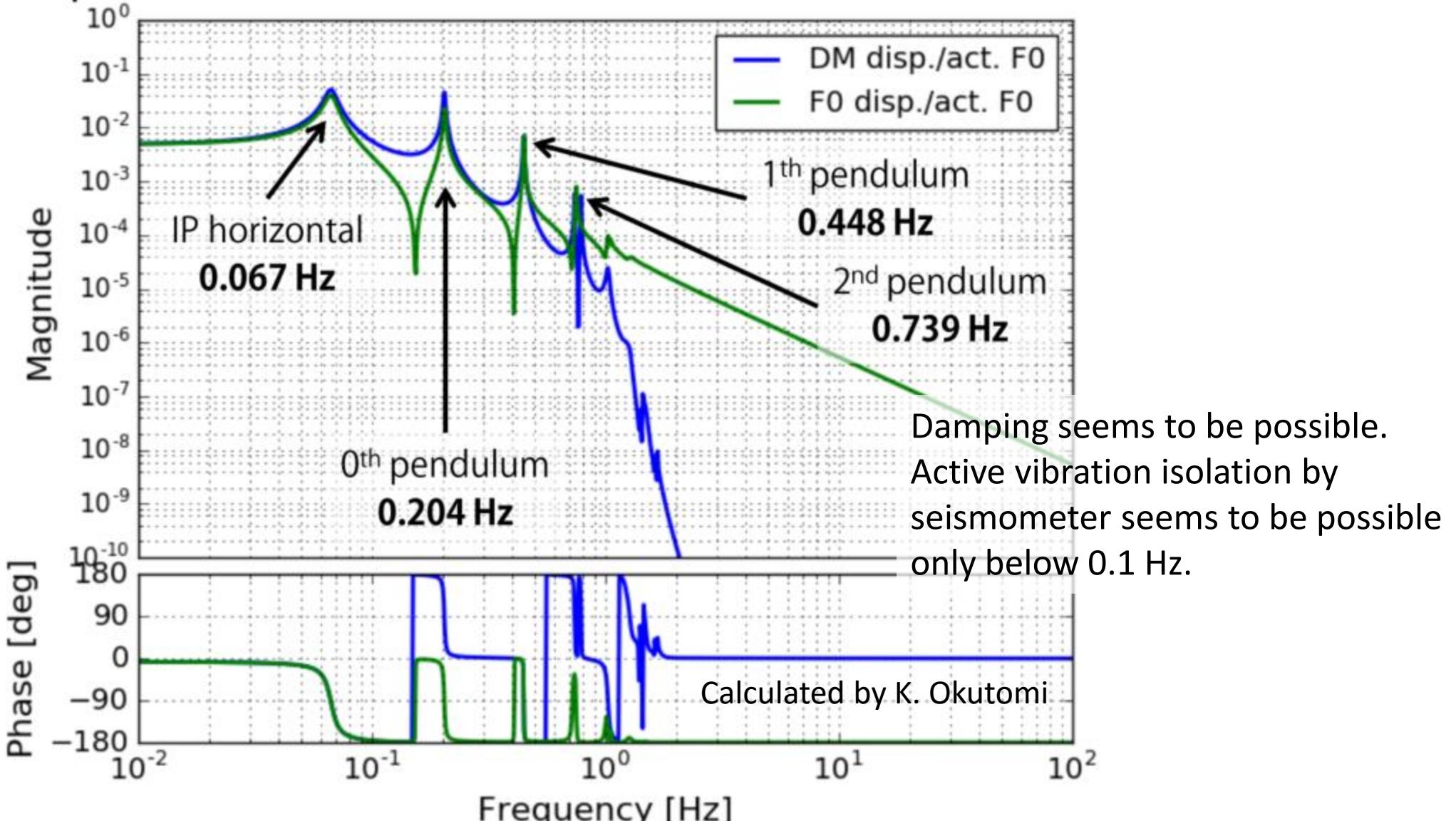
	Type-A	Type-B	Type-Bp
Lock-acquisition phase	RMS velocity 50 um/sec (for green lock)	0.7 um/sec	0.5 um/sec
	RMS angle 0.1 urad	1 urad	1 urad
Observation phase	Control noise @ 10Hz $1 \times 10^{-19} \text{ m/rtHz}$	$5 \times 10^{-18} \text{ m/rtHz}$	$1 \times 10^{-15} \text{ m/rtHz}$

Caution: The values are old!!

# Type-A

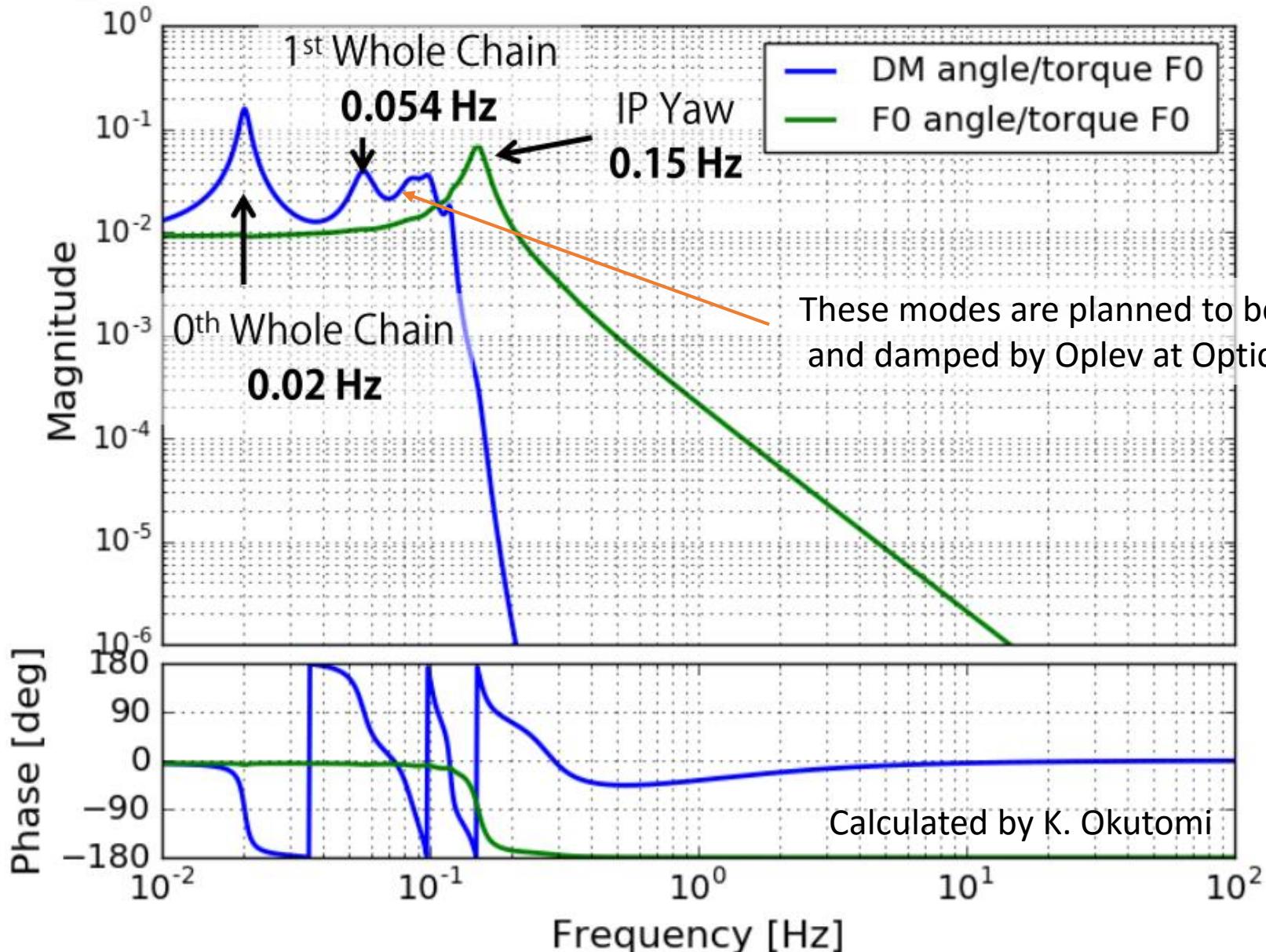


# Displacement/Force Transfer Function L



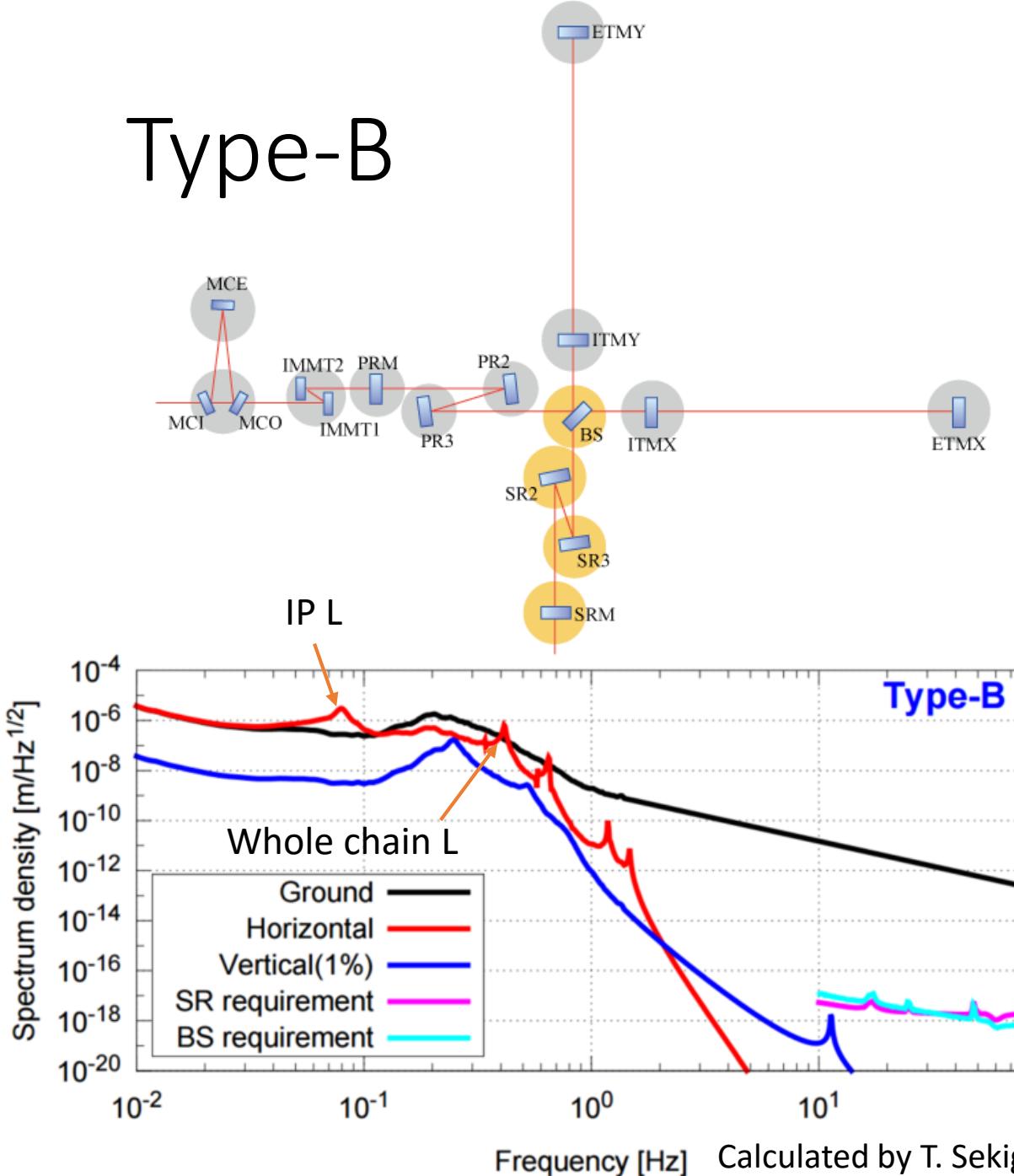
\*Eigenmode identification will be added

# Displacement/Force Transfer Function Y



Further investigation is necessary...

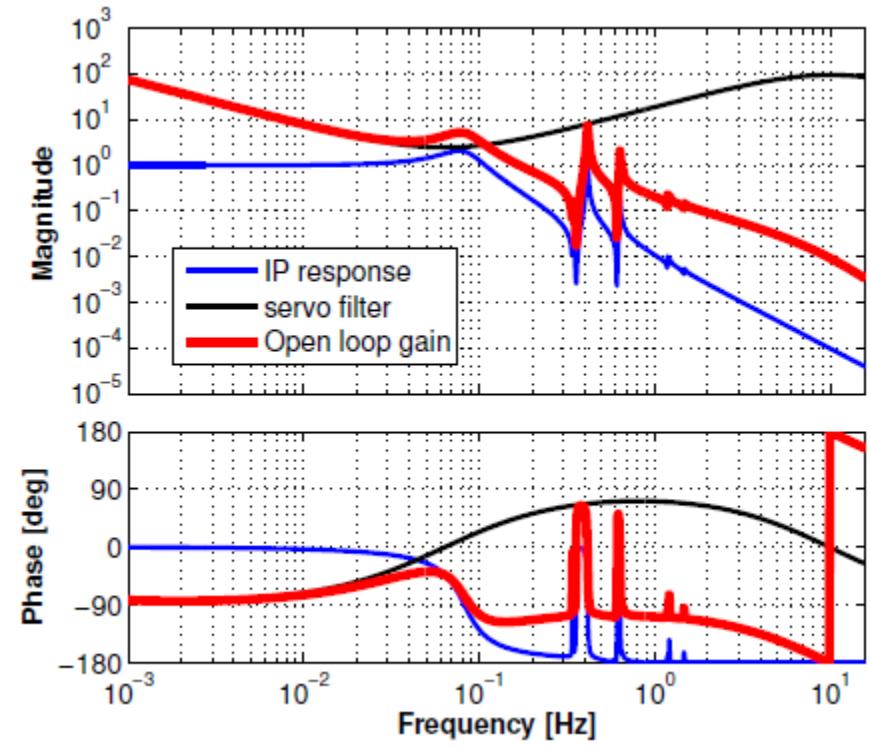
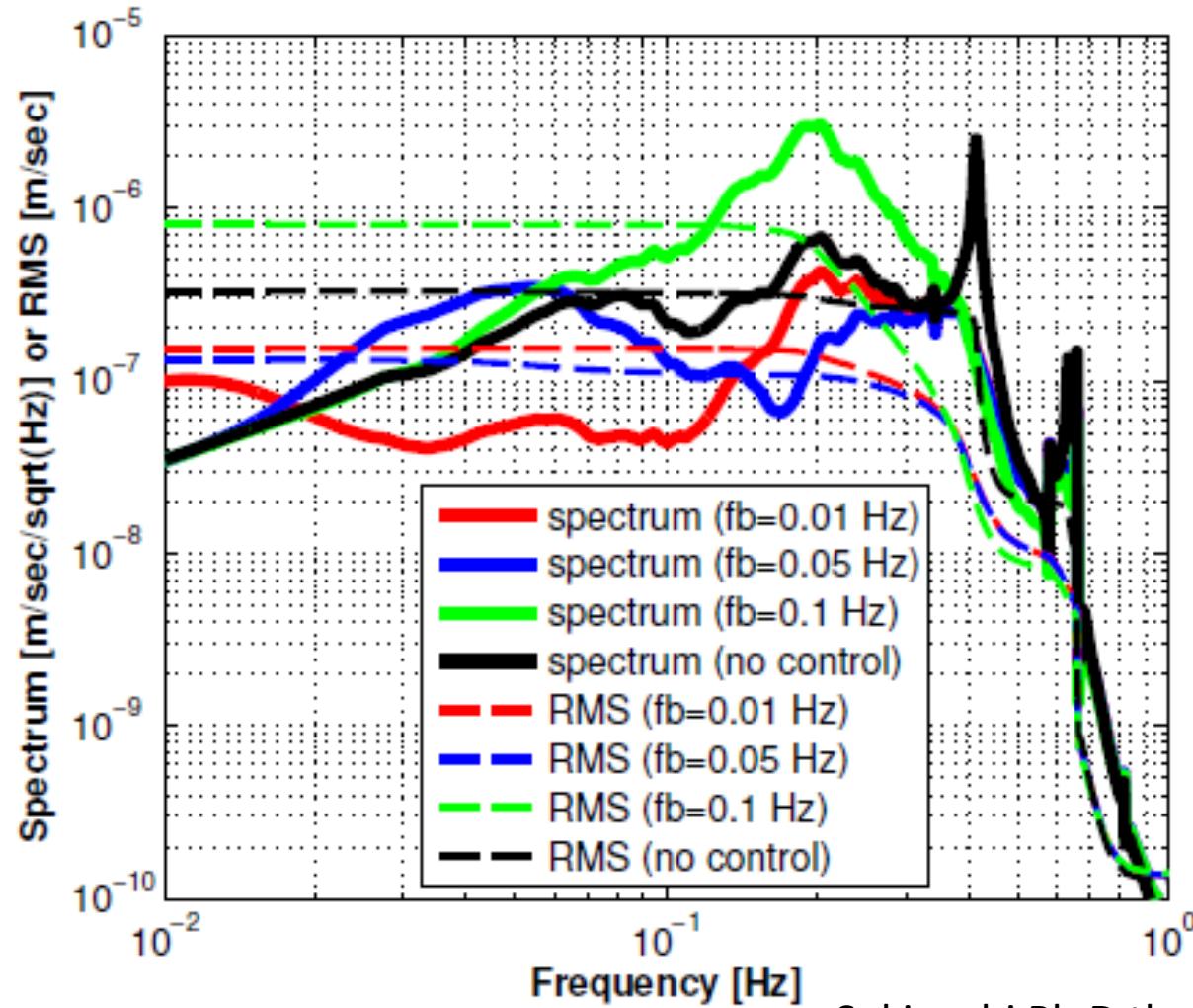
# Type-B



IP	LVDT	L, T, Y
GAS0	LVDT	V
MD		
GAS1	LVDT	V
GAS2	LVDT	V
IM	OSEM	L, T, V Y, R, P
Optic	OSEM	L, P, Y

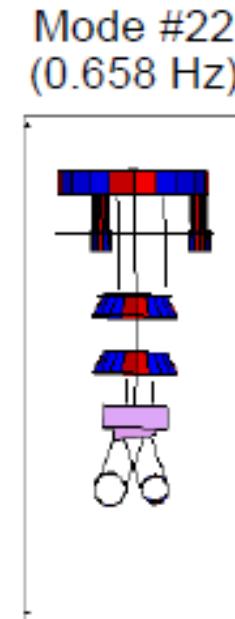
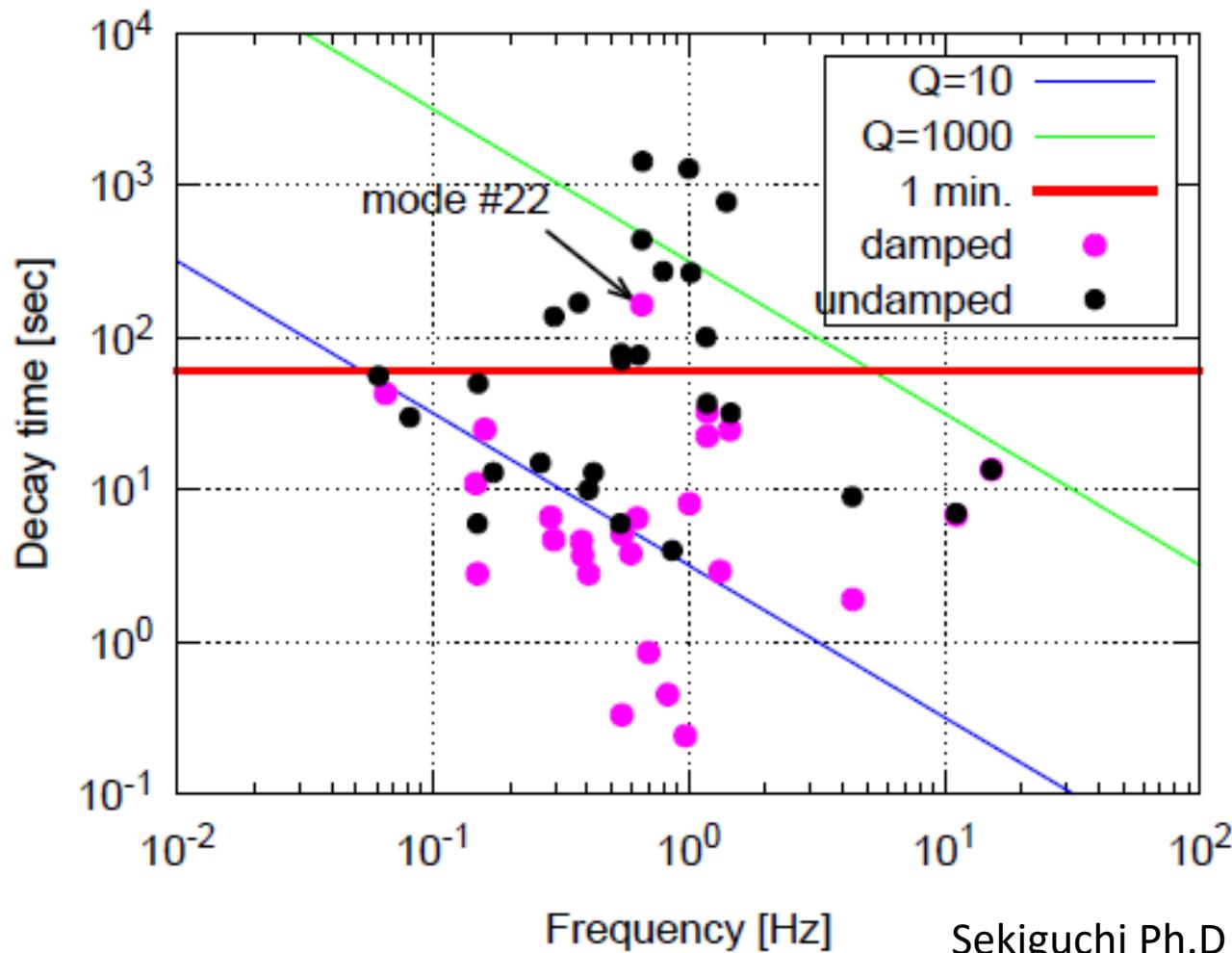
Calculated by T. Sekiguchi

# IP control in TAMA prototype experiment



Sekiguchi Ph.D thesis

# Q factors



# Residual RMS

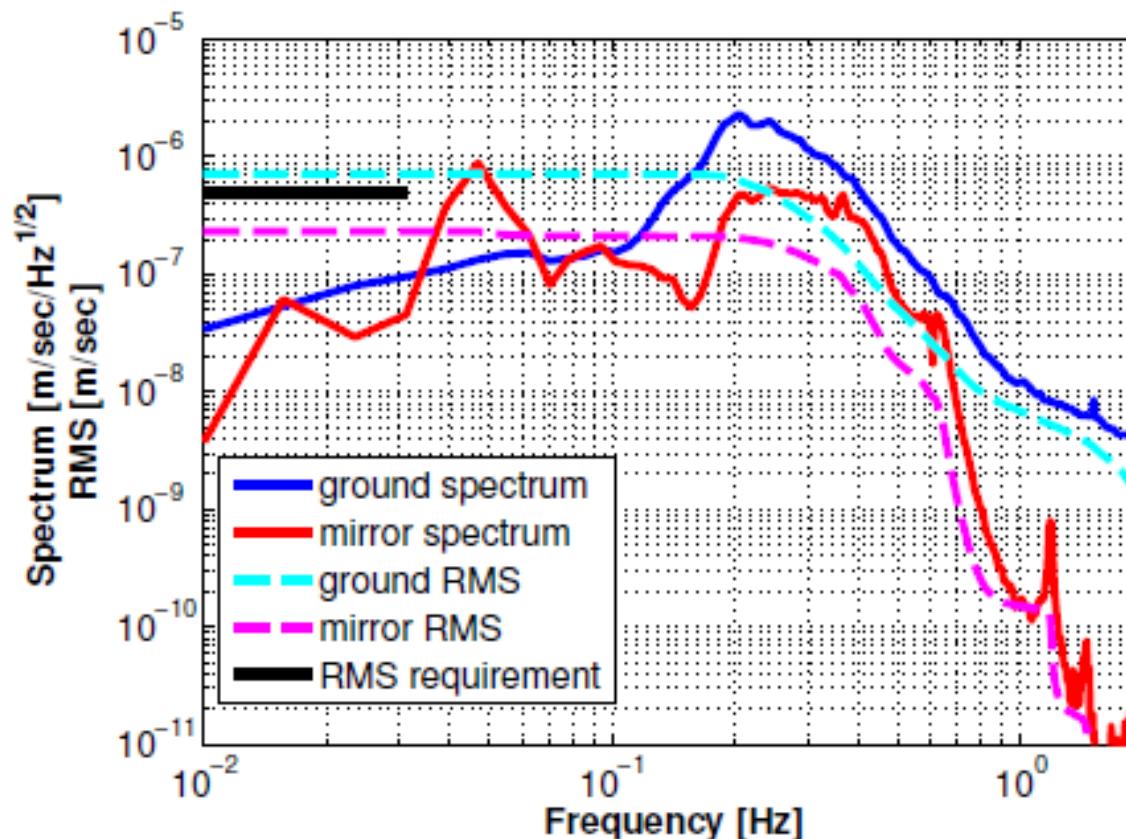
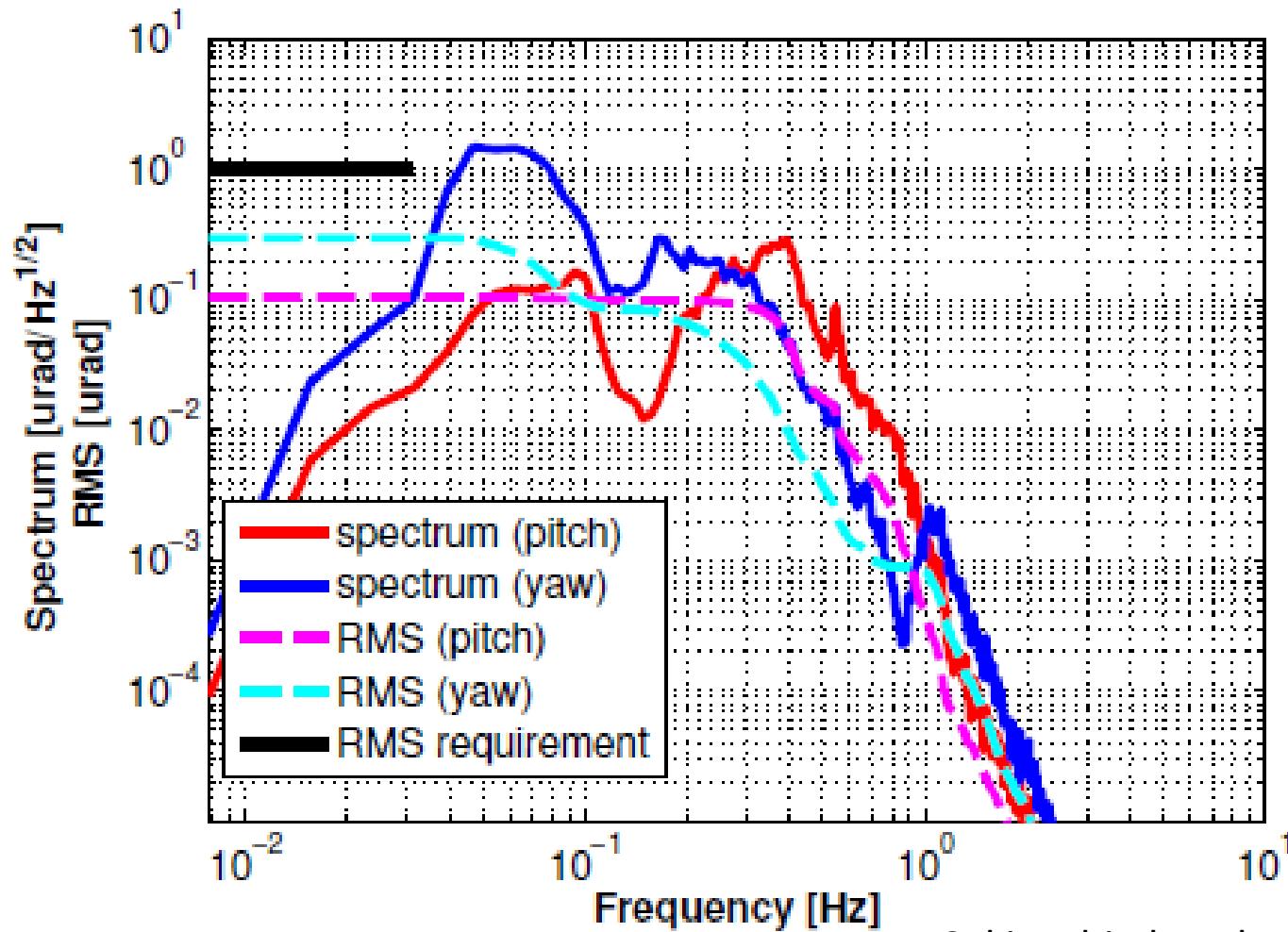
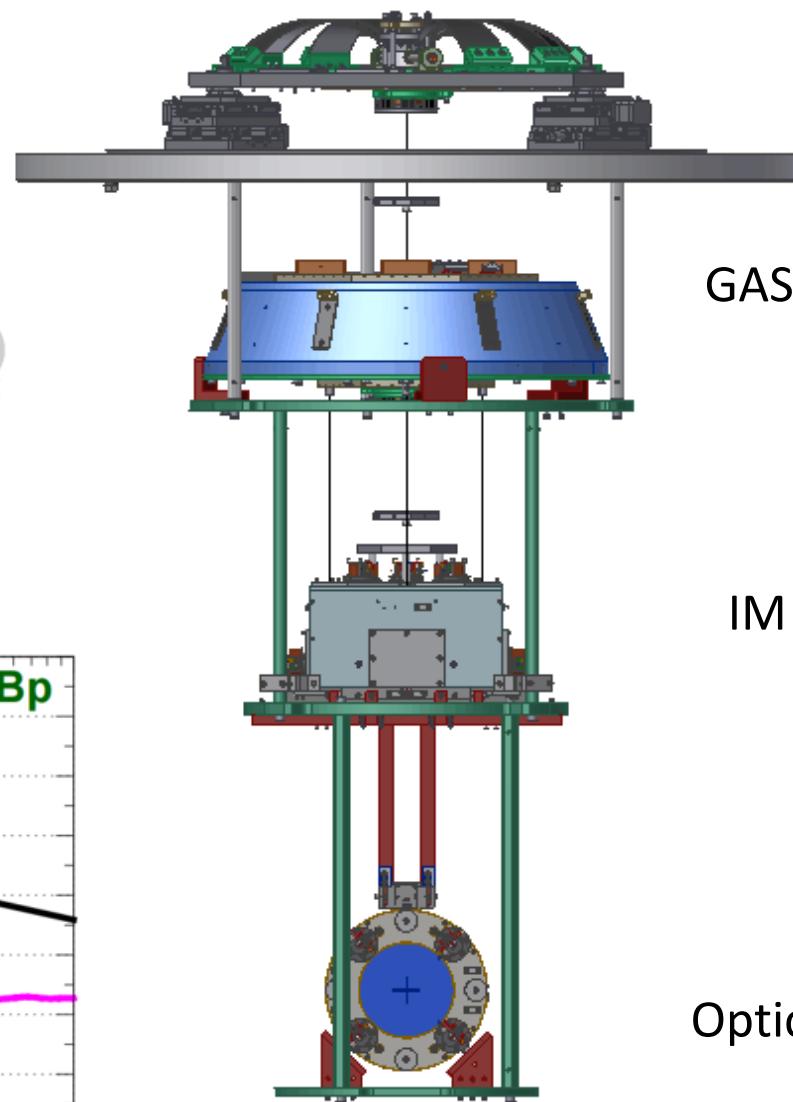
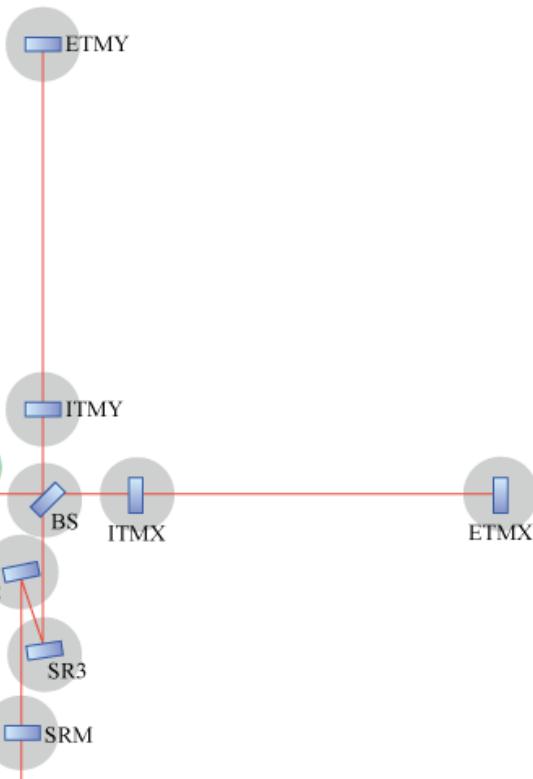
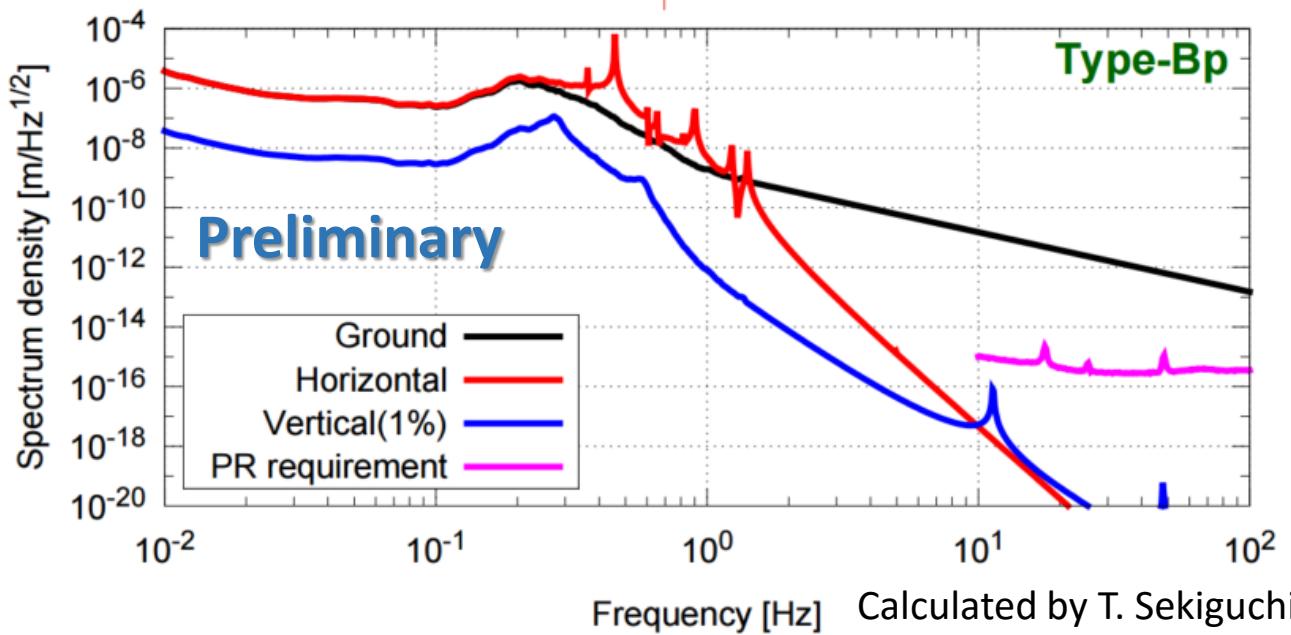


Figure 8.17: The mirror longitudinal vibration spectra estimated with the measured transfer function, assuming seismic vibration in the KAGRA site. Sekiguchi Ph.D thesis

# Residual RMS measured by Oplev (tilt)

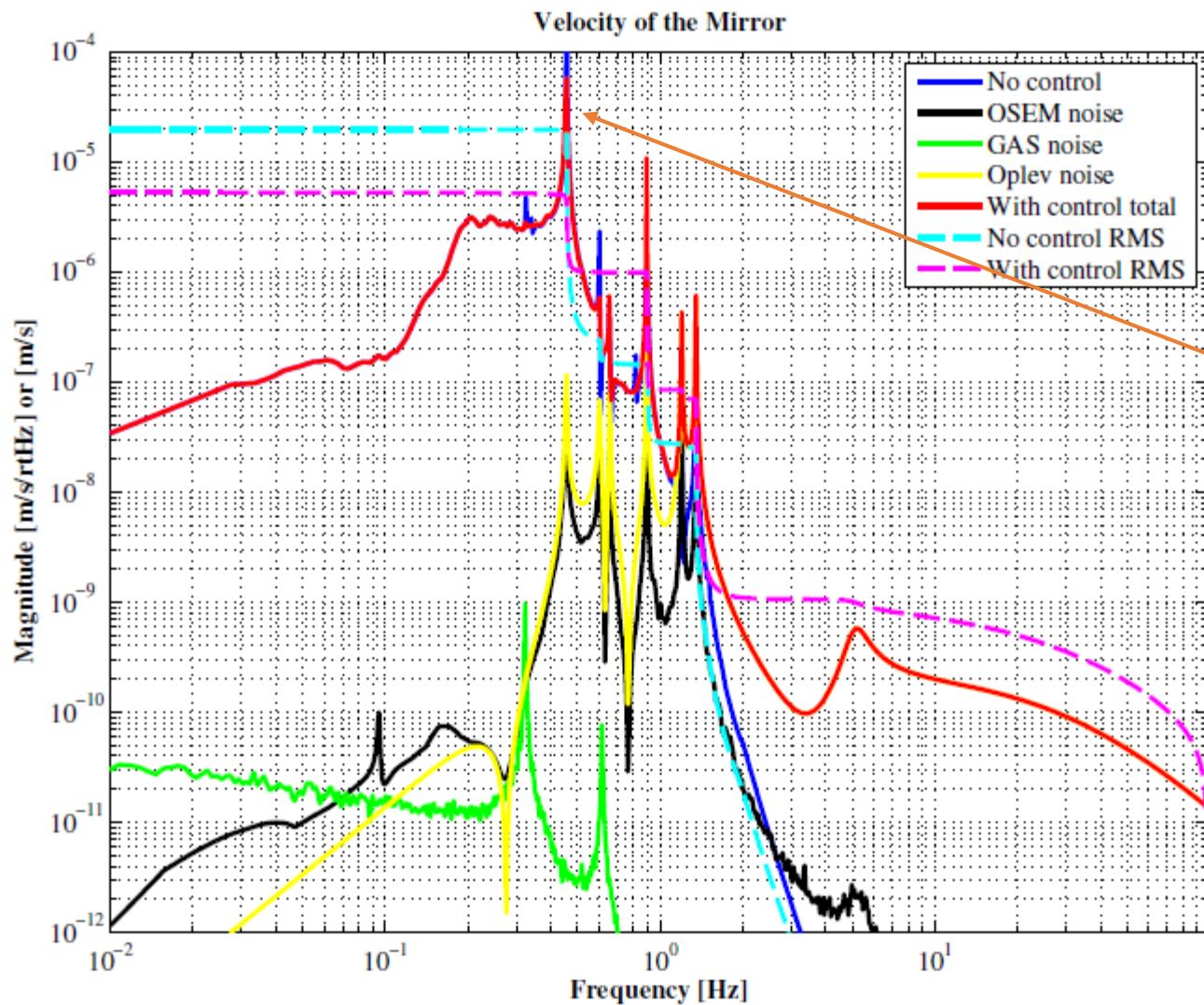


# Type-Bp



GAS1	LVDT	V
GAS2	LVDT	V
IM	OSEM	L, T, V Y, R, P
Optic	OSEM Oplev	L, P, Y

# Problem in Type-Bp

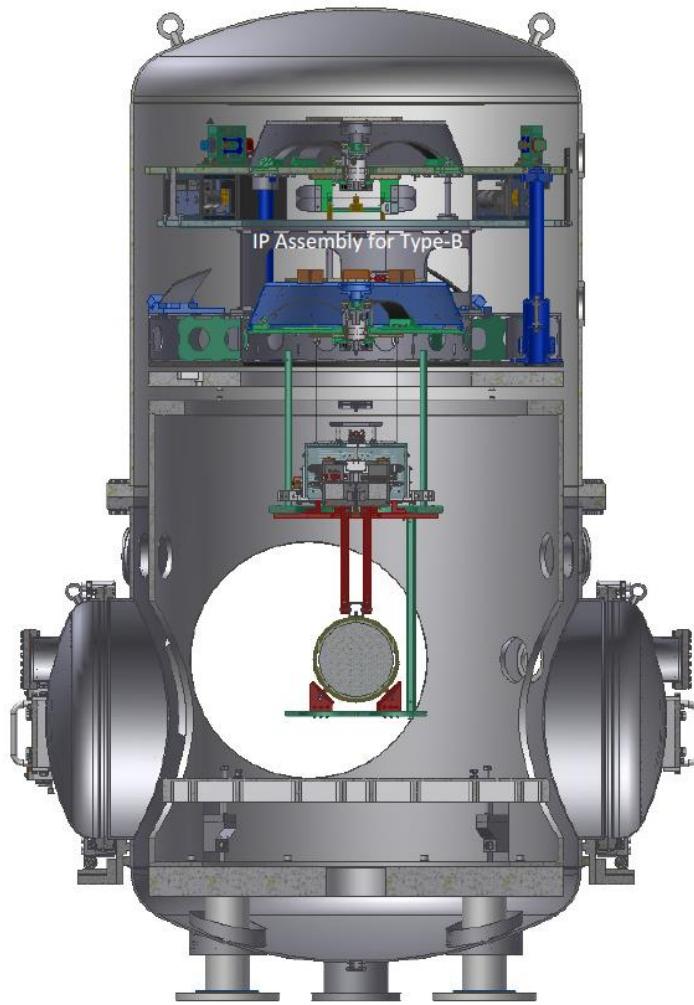


Cannot be damped!

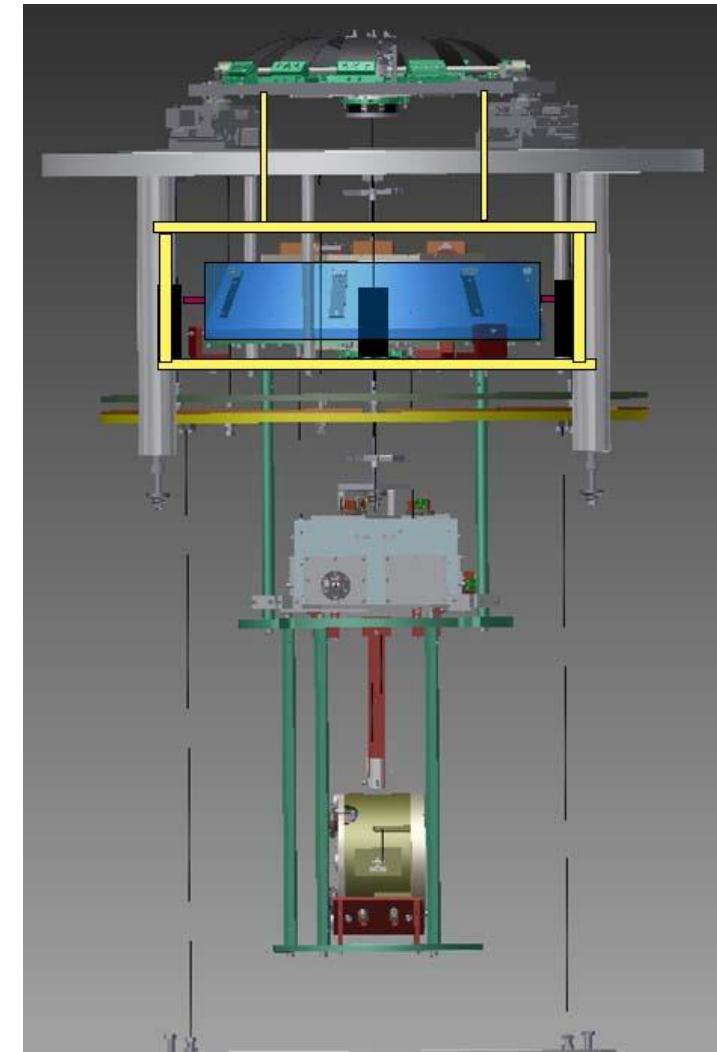


# Modification plan

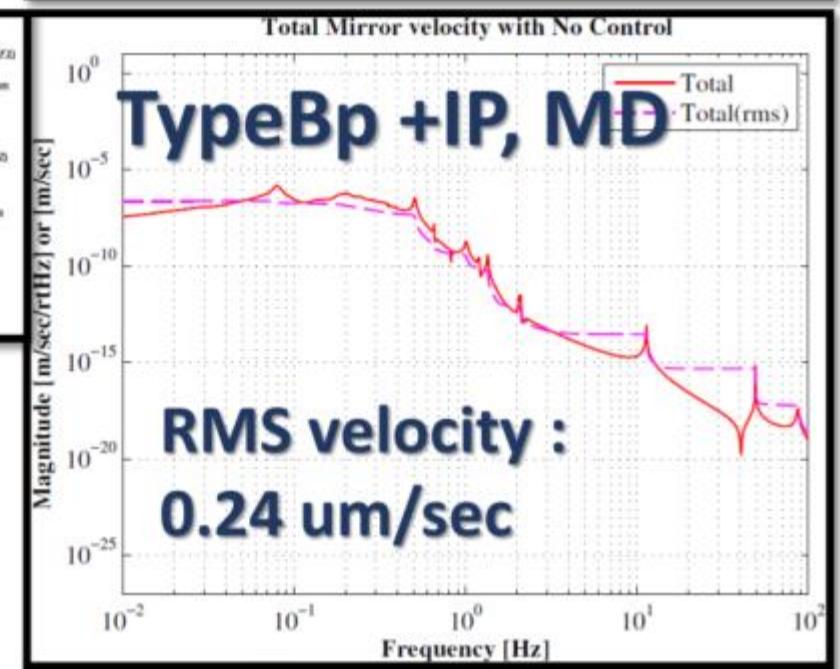
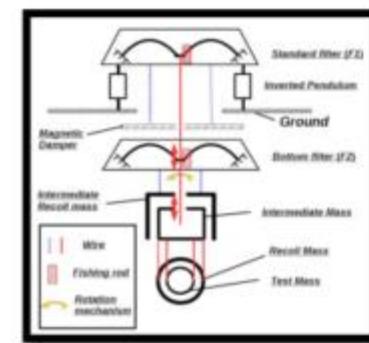
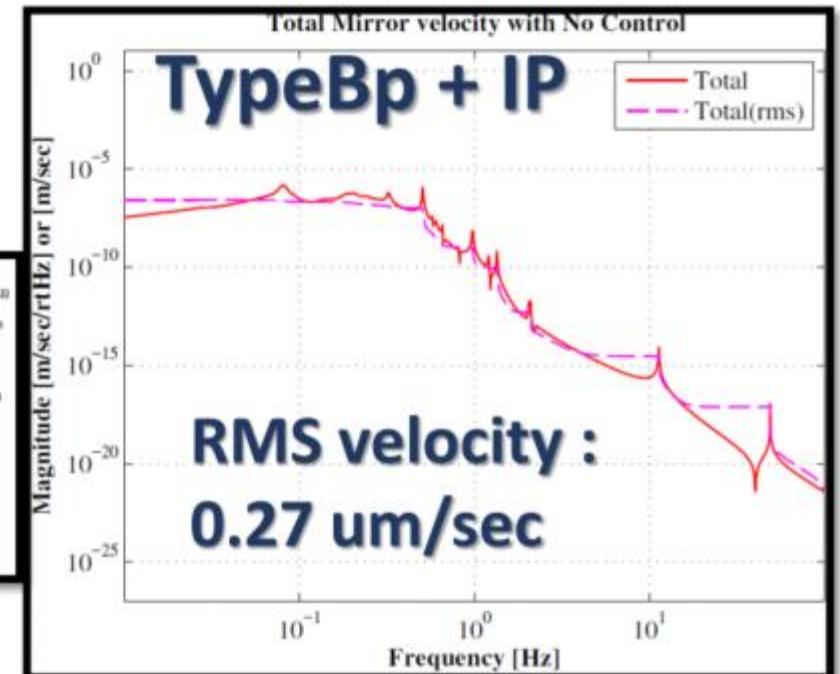
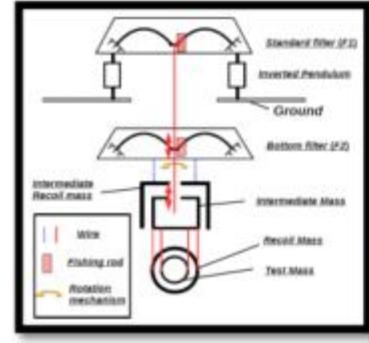
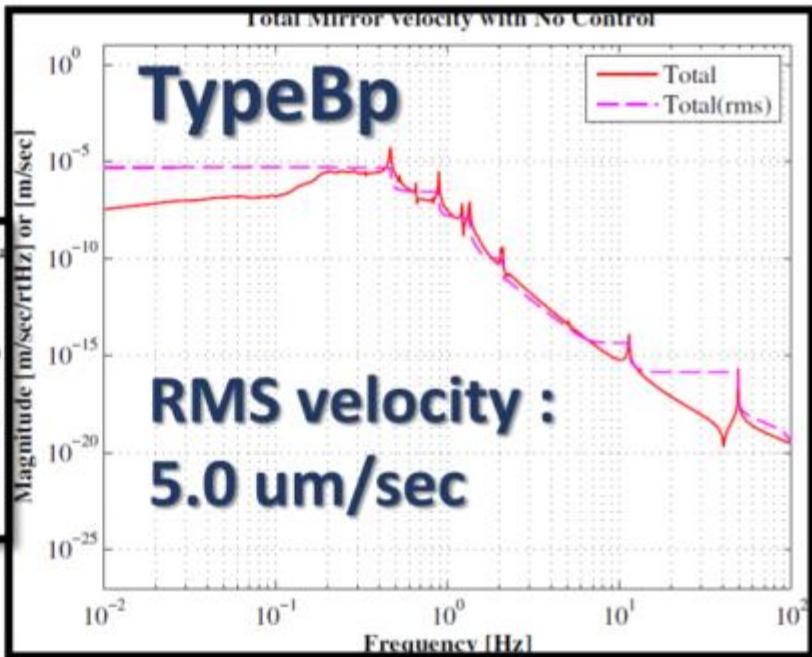
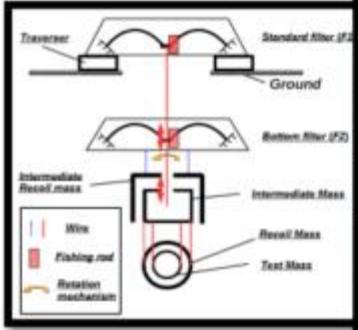
Plan A: Add IP



Plan B: Add active damping at the BF



# TM velocity without control



Calculated by Y. Fujii

MD doesn't bother the TM velocity.

# Feedback on BF

