

# Characterization of the payload of the Type B suspension system for KAGRA according to the prototype experiments at TAMA300

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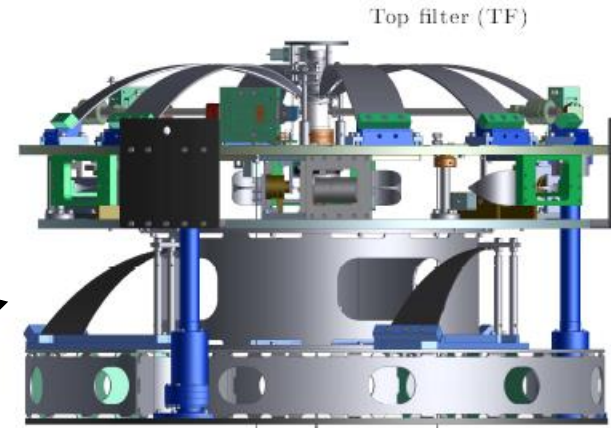
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# Outline

- Description of the payload.
- Description of the OSEM.
- Damping the resonances of the suspension.
- Alignment range.
- Pictures of the assembly.
- Mechanical changes to the payload design.
- Conclusion

# Type B seismic attenuation System

Pre-isolator



Inverted pendulum (IP)

Standard GAS filter



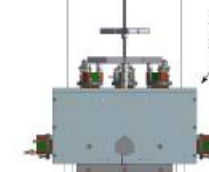
Standard filter (SF)

Bottom GAS filter



Bottom filter (BF)

Payload



Intermediate recoil mass (IRM)

Intermediate mass (IM)

Magnetic damper

Test Mass (TM)

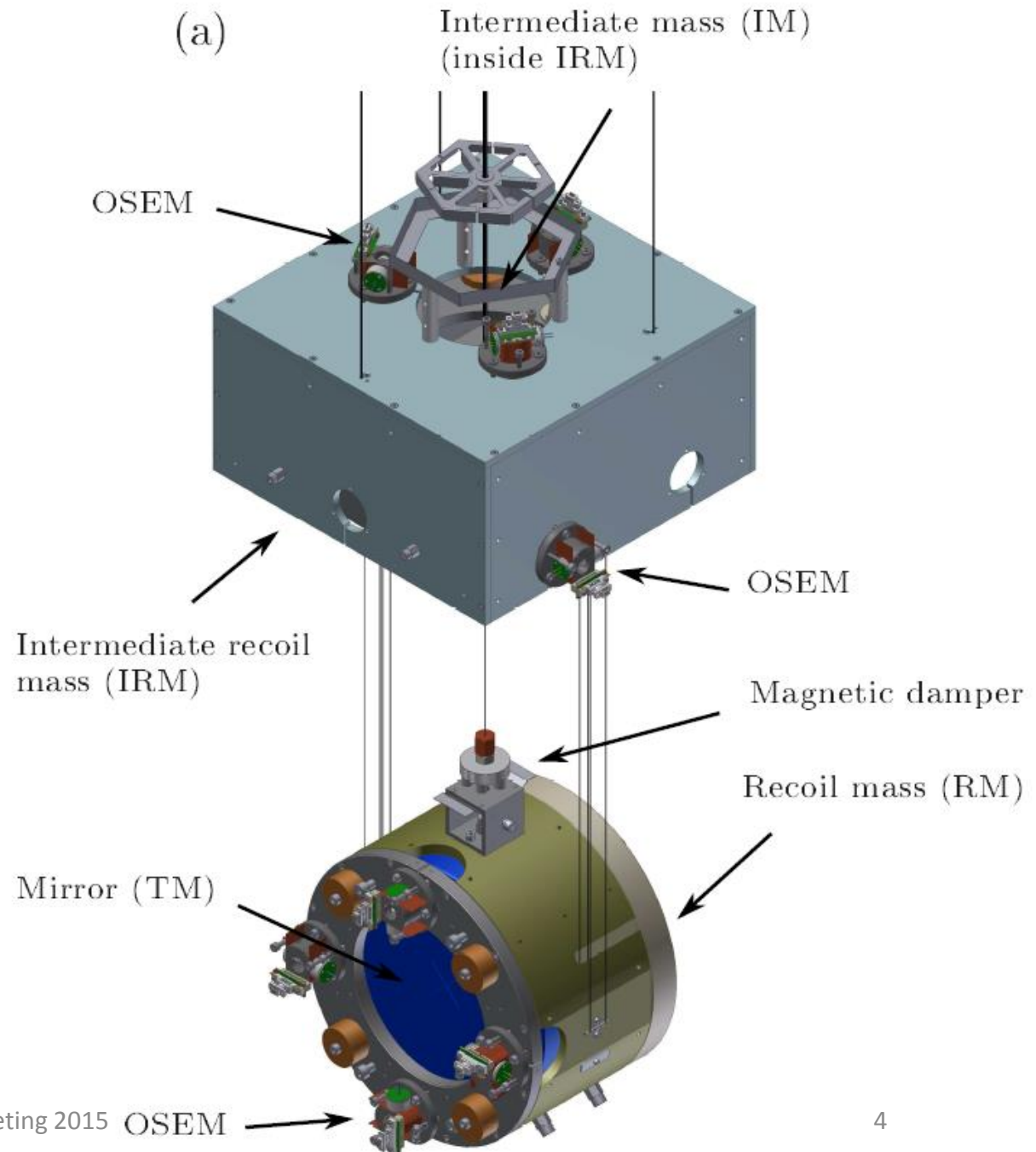
Recoil mass (RM)

# The payload prototype (1)

- Test mass
- Recoil mass
- Intermediate mass (marionette)
- Intermediate recoil mass
- 10 OSEMs

Test mass: 200  $\mu\text{m}$  steel wire.

Recoil mass: 600  $\mu\text{m}$  tungsten wire.



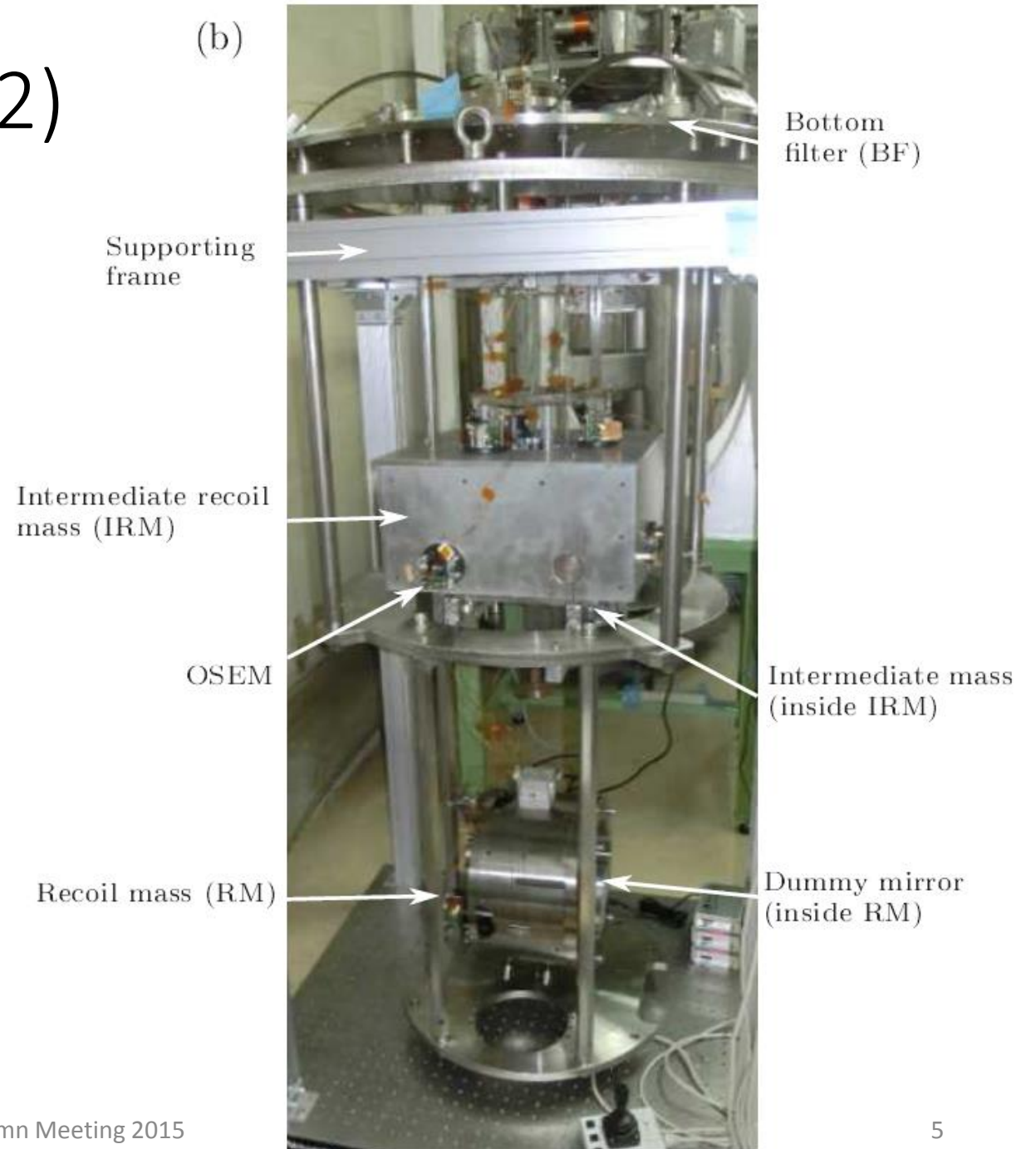
# The payload prototype (2)

- Test mass
- Recoil mass
- Intermediate mass (marionette)
- Intermediate recoil mass
- 10 OSEMs

Test mass: 200  $\mu\text{m}$  steel wire.

Recoil mass: 600  $\mu\text{m}$  tungsten wire.

(b)

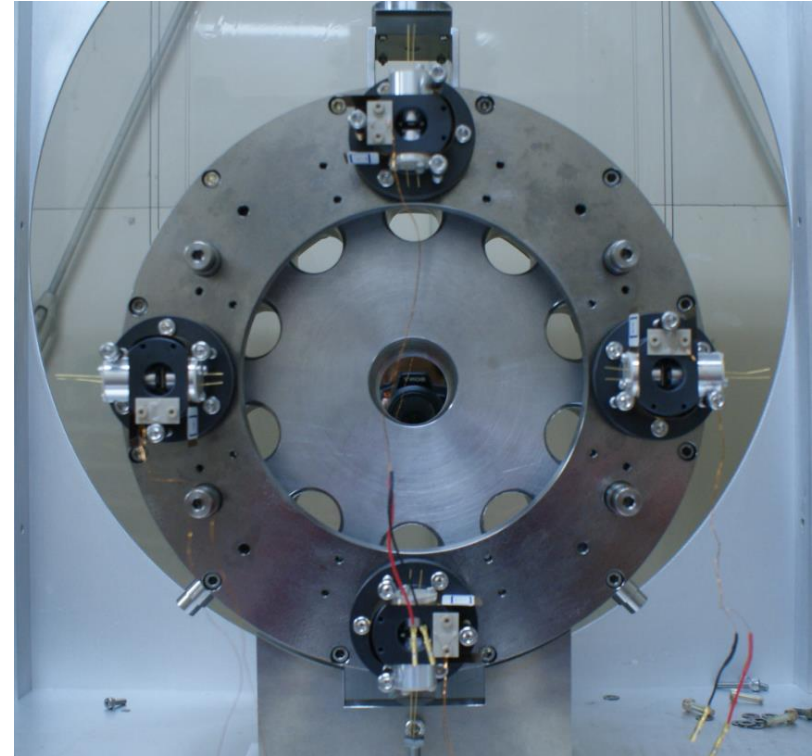


# The payload prototype (3)

- Test mass
- Recoil mass
- Intermediate mass (marionette)
- Intermediate recoil mass
- 10 OSEMs

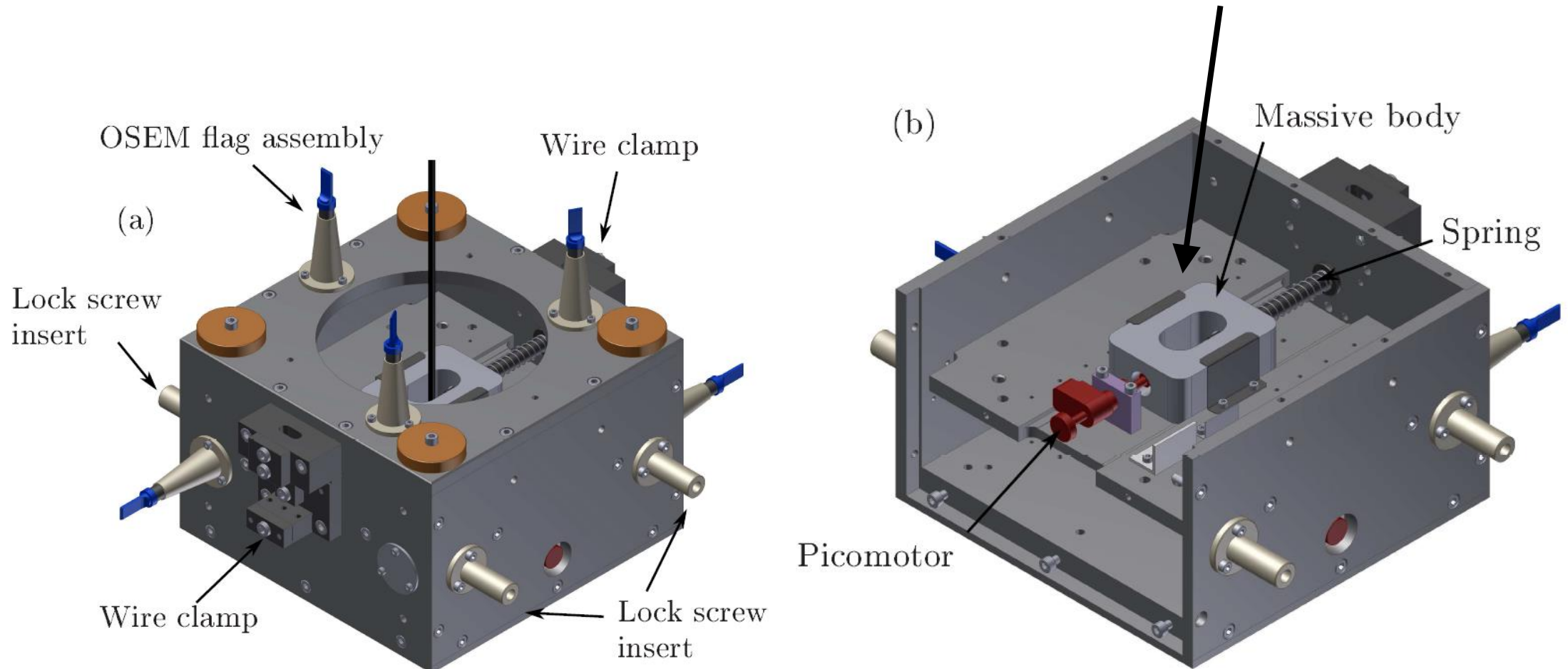
Test mass: 200  $\mu\text{m}$  steel wire.

Recoil mass: 600  $\mu\text{m}$  tungsten wire.

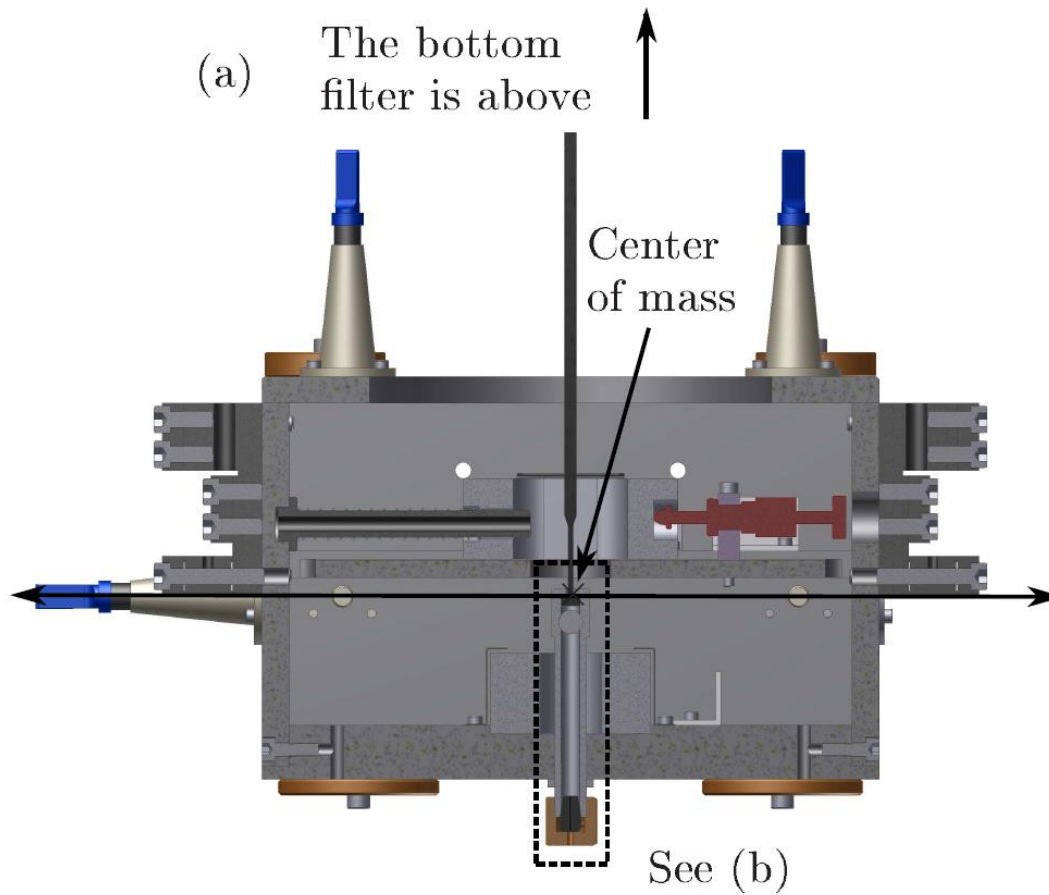


# Intermediate mass (1)

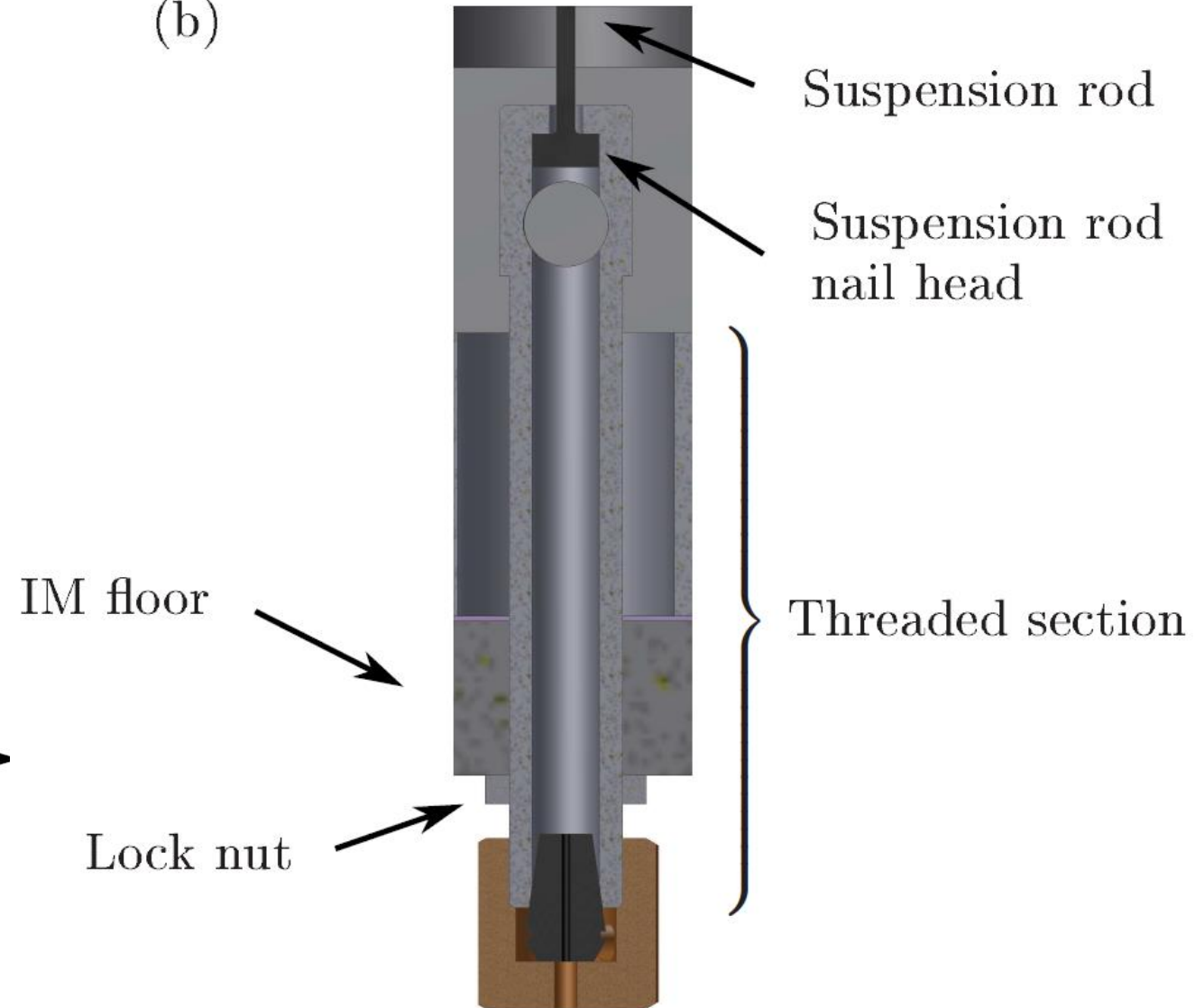
It was calculated that this system provides roll and pitch adjustment of approximately  $\pm 2.5$  degrees.



# Intermediate mass (2)



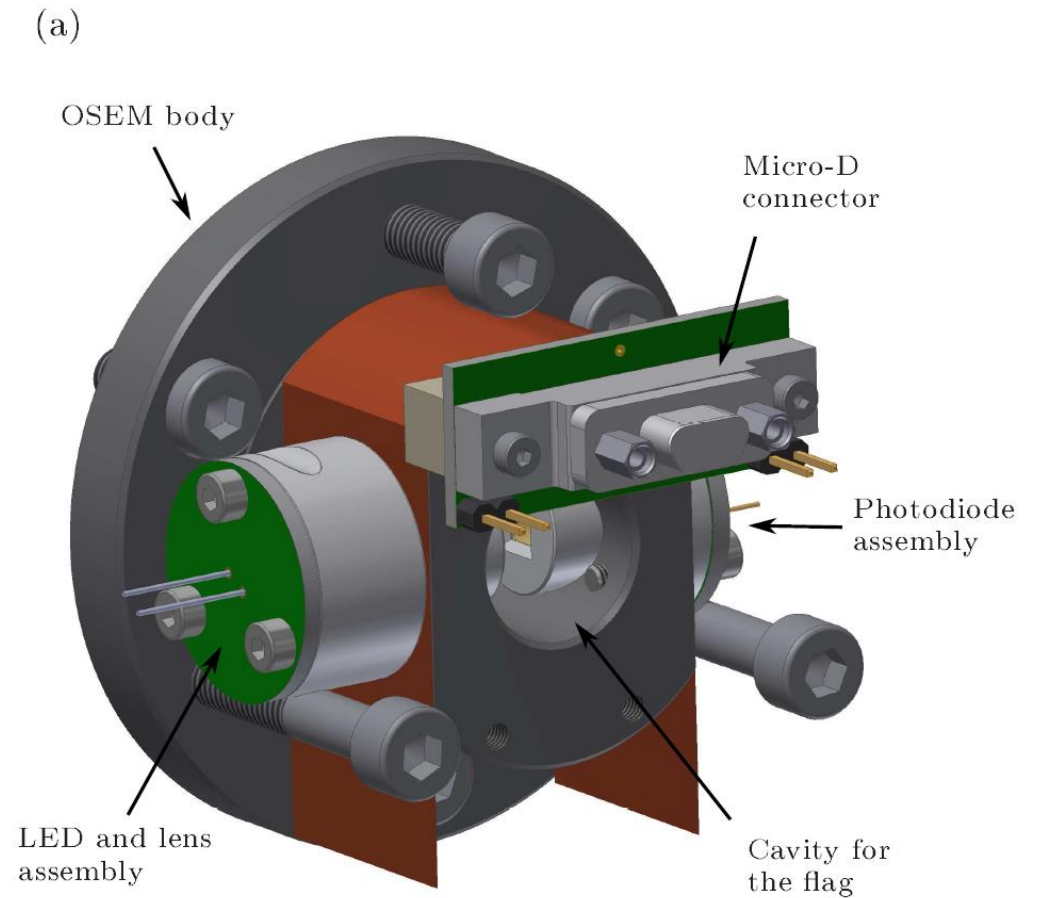
(b)





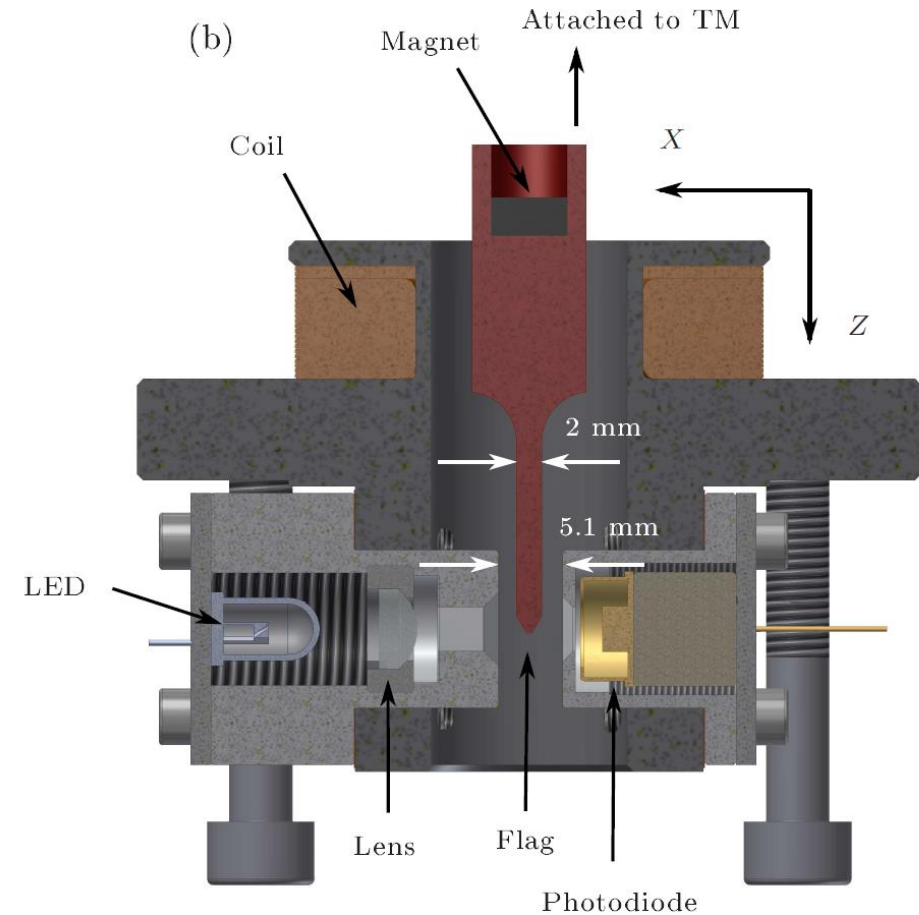
# OSEM (1)

- OSEM: Optical sensor and electromagnetic actuator.
- shadow sensor.
- Coil-magnet actuator.

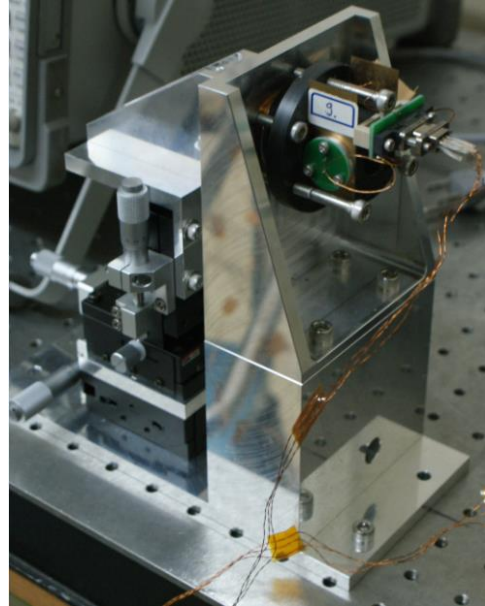
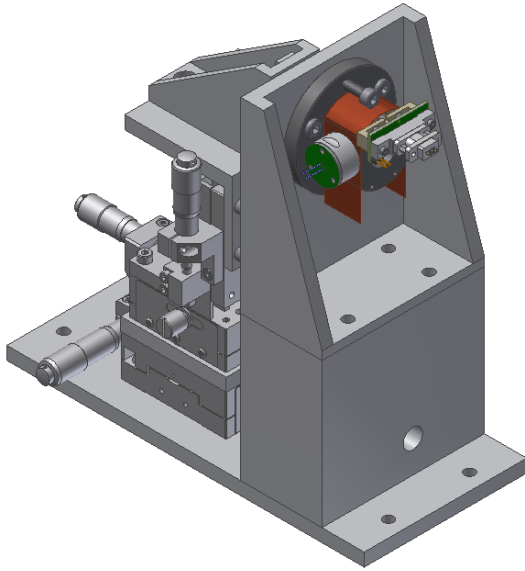


# OSEM (2)

- OSEM: Optical sensor and electromagnetic actuator.
- shadow sensor.
- Coil-magnet actuator.

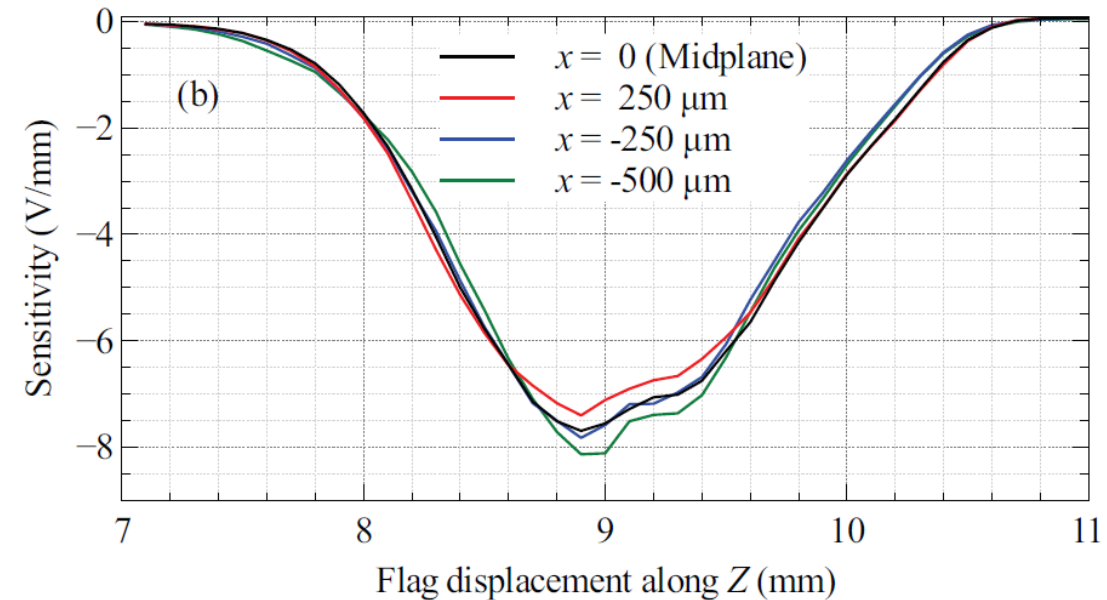
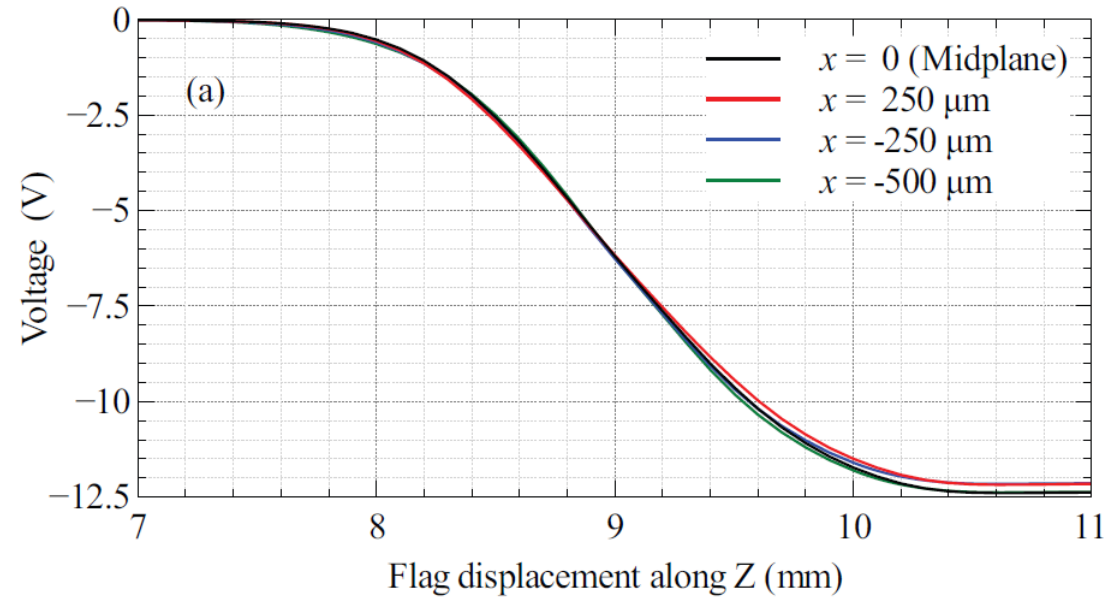


# OSEM calibration

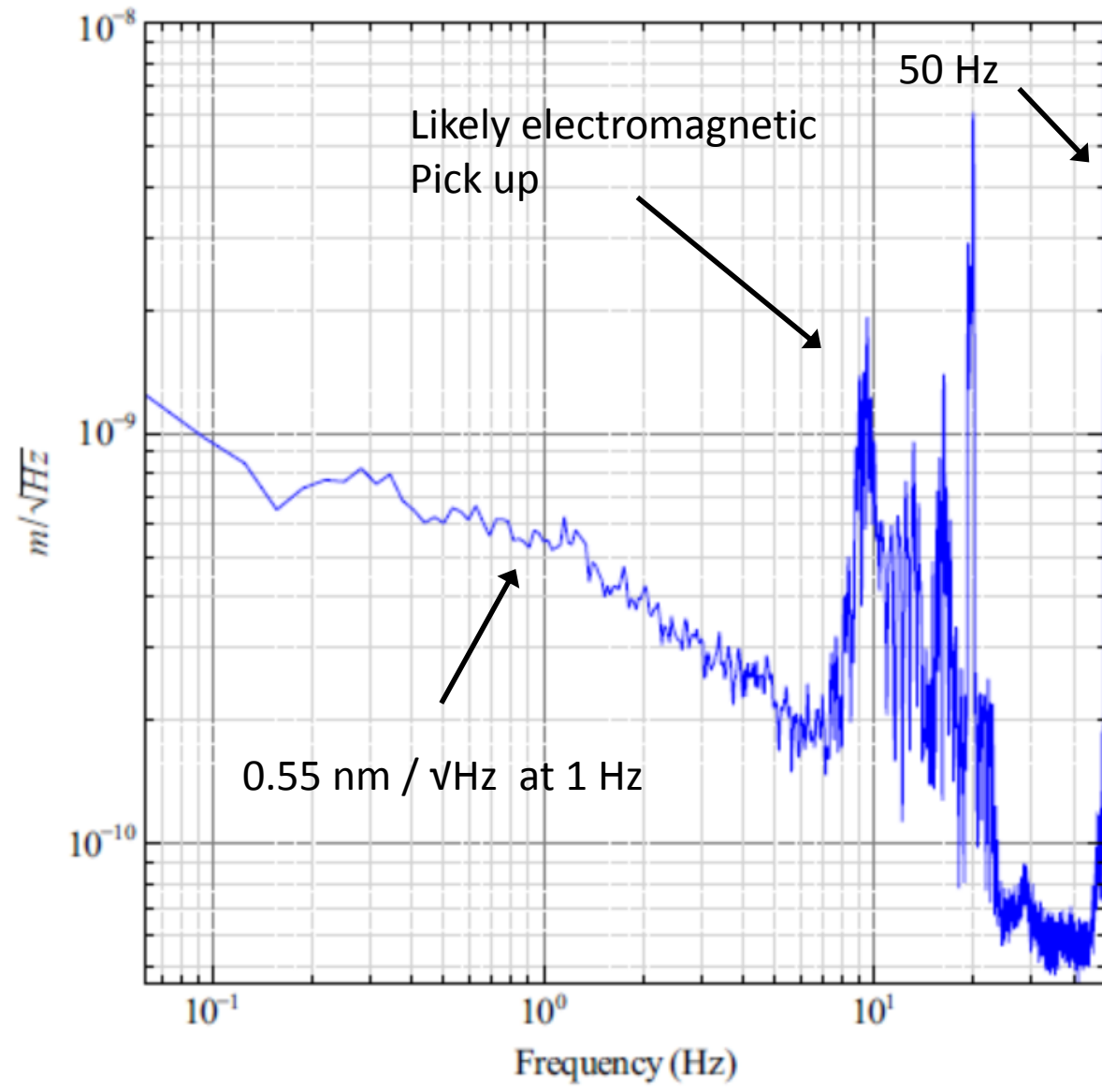


Measurement range (linear regime along  $Y$ ): **1 mm**.

Alignment tolerance (along  $X$ ):  **$\pm 400 \mu\text{m}$**  for a  **$\pm 5\%$**  error.



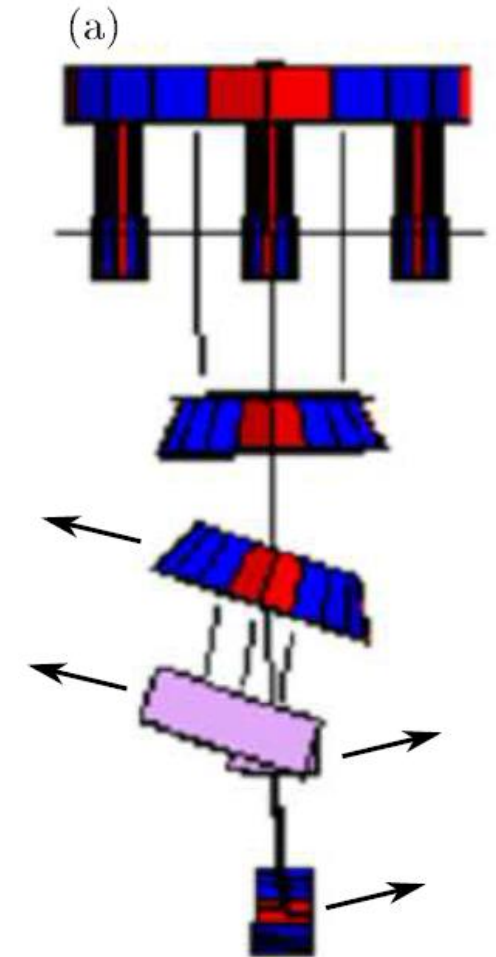
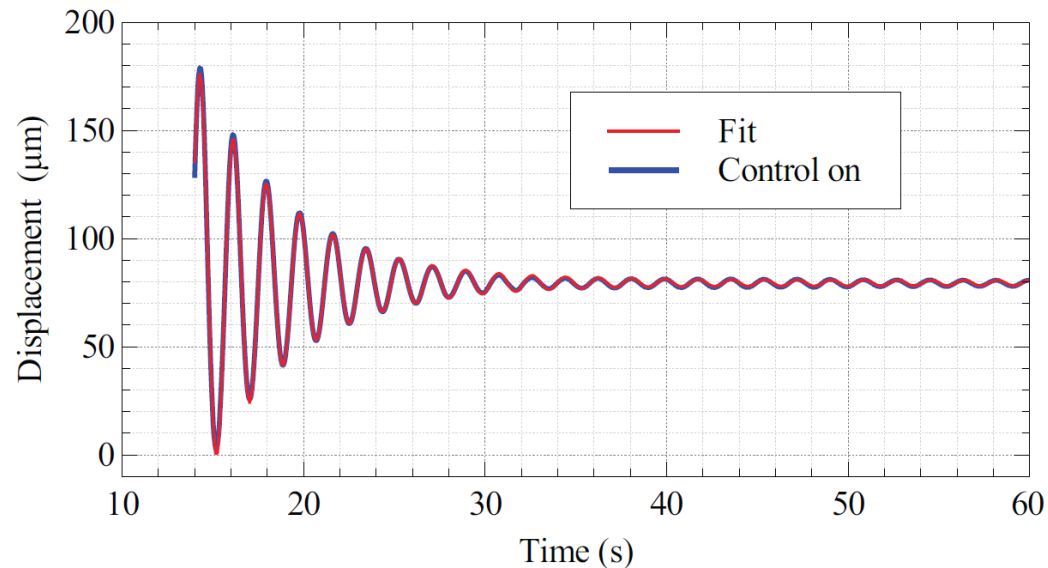
# OSEM sensitivity



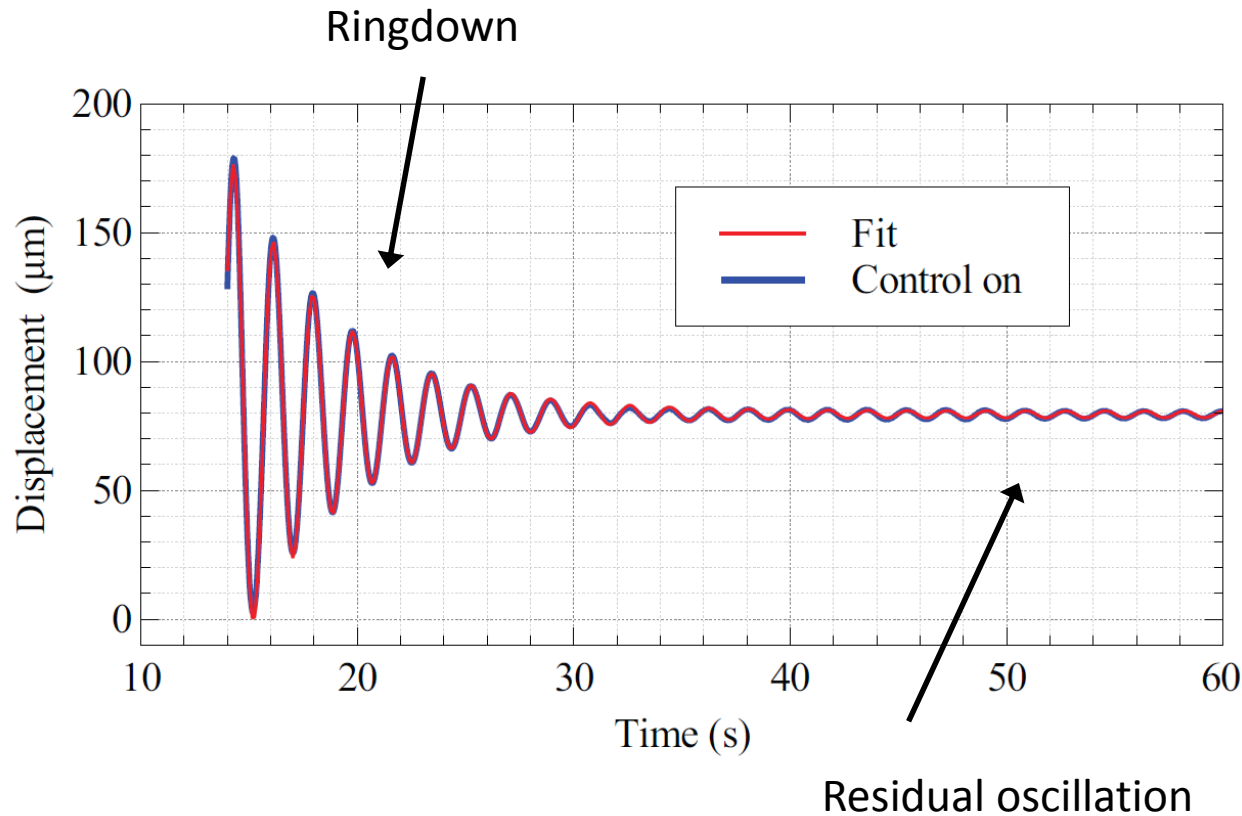
# Damping the suspension resonances (1)

We used the traditional method:

1. The modes were excited separately using the OSEMs.
2. An exponentially damped sinusoidal function was fitted to the ringdown.
3. The quality factor was calculated as  $Q = \pi f_0 \tau$ .

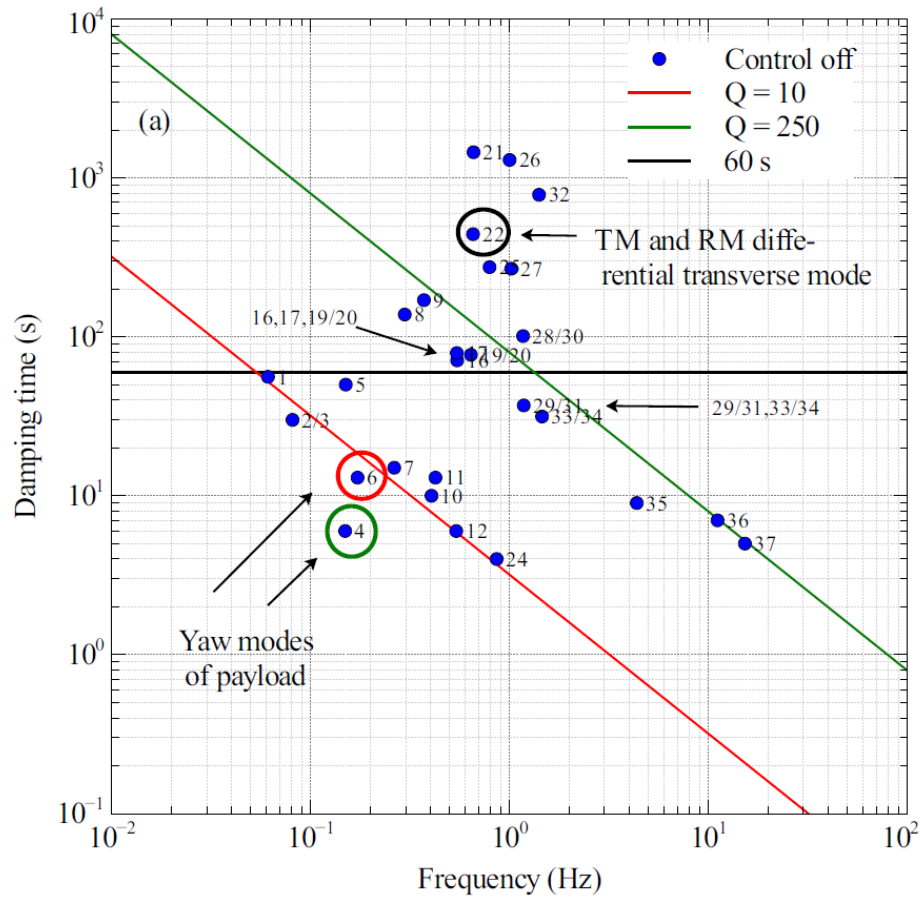


# Damping the suspension resonances (2)

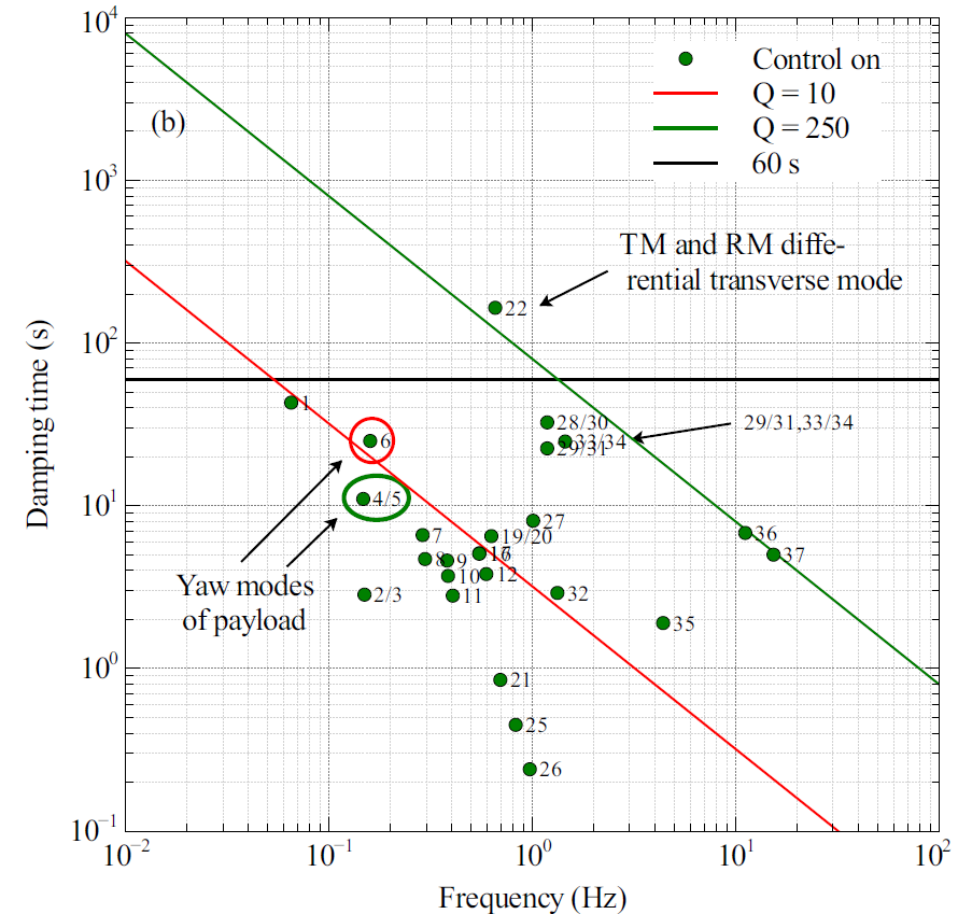


- The residual oscillation may be seismic motion not filtered by the chain.
- However, that requires other frequencies to be present in the residual movement because the resonant peak becomes wider.
- More investigation is needed.

# Damping the suspension resonances (3)

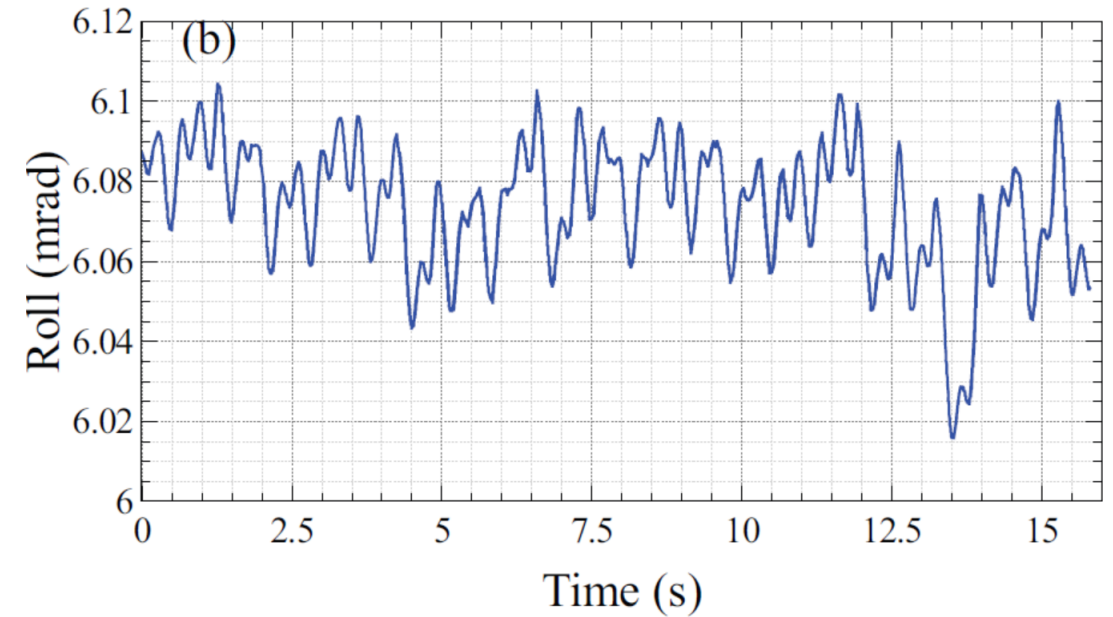
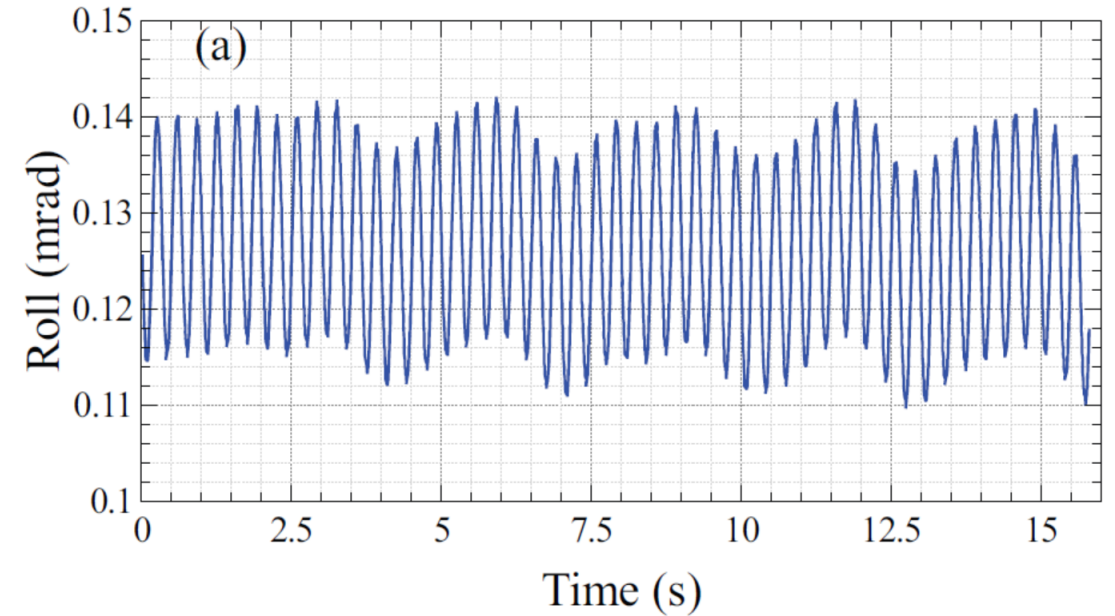


Vacuum broken



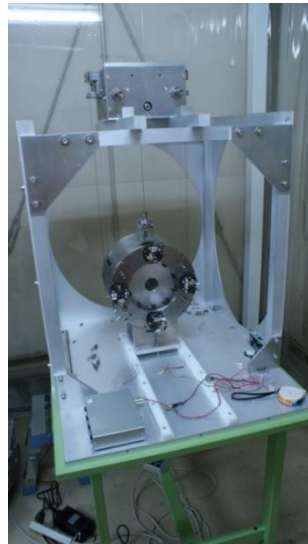
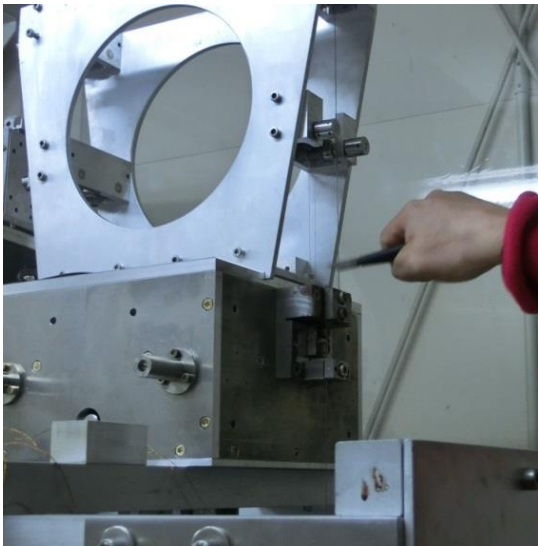
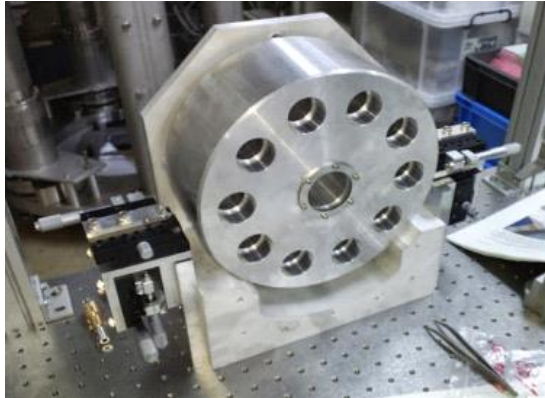
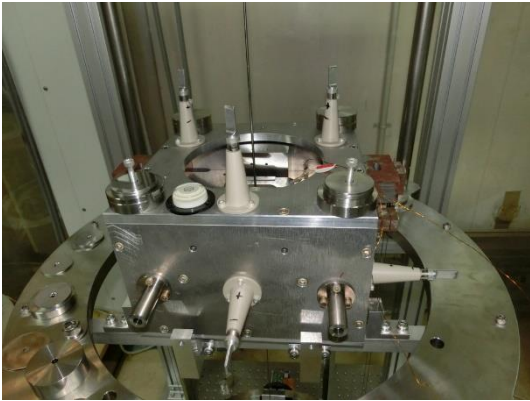
# Alignment range

DOF	Minimum (mrad)	Maximum (mrad)
Roll	-4.7	5.9
Pitch	-5.0	5.0
Yaw	-1.8	3.5

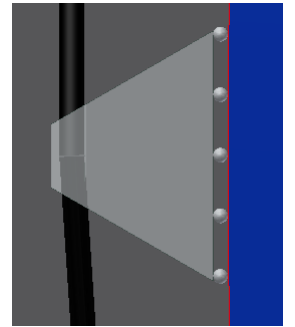
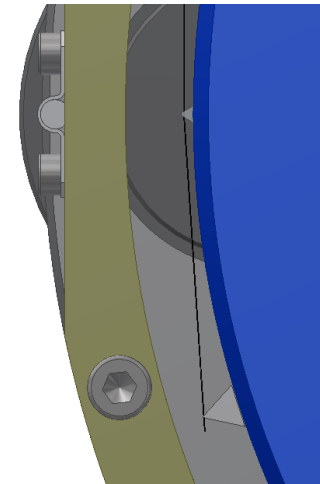
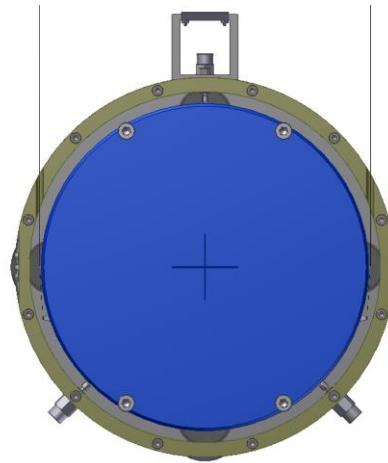
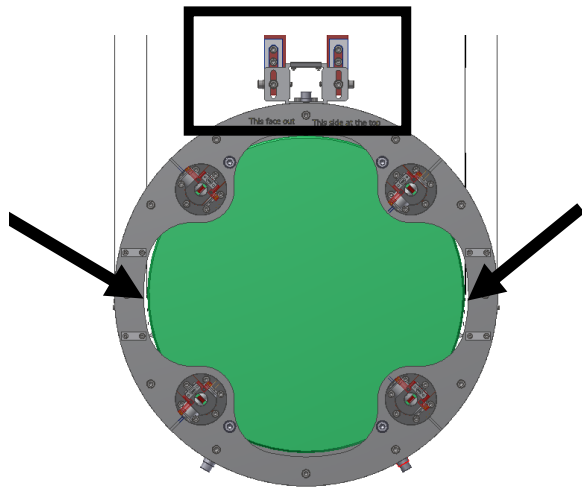
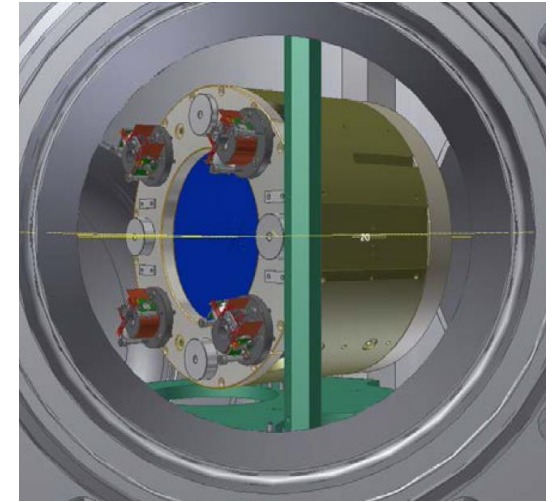
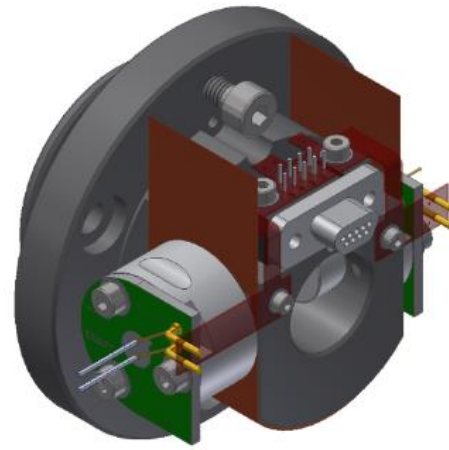
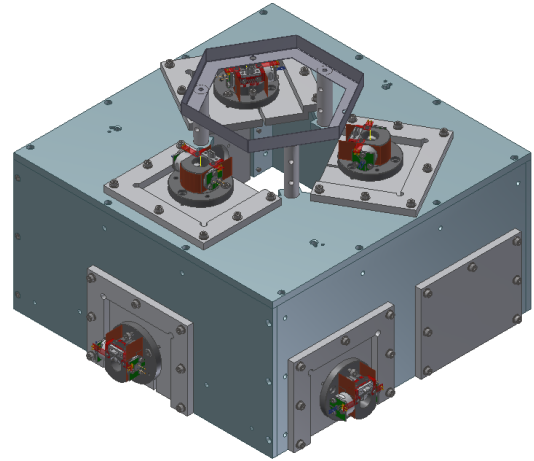
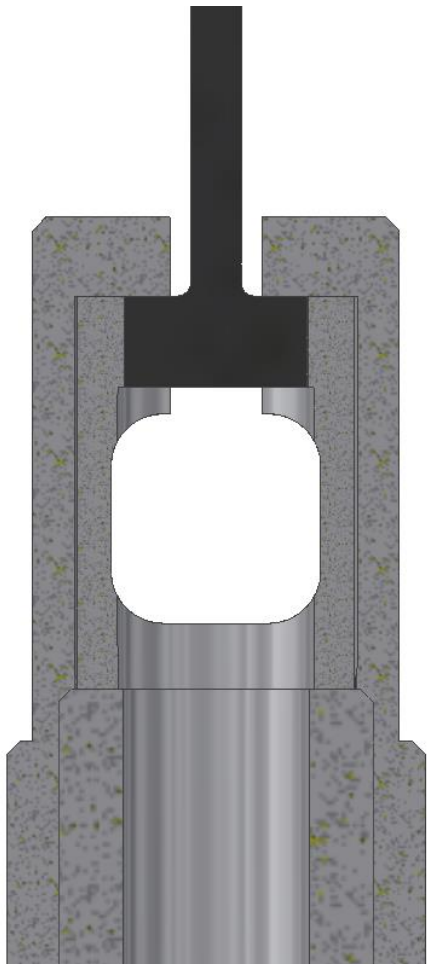




# Assembly of the payload



# Changes in the payload



# Conclusions and future work

- The payload prototype was assembled and tested at NAOJ.
- Values of quality factors were given with the active control on:
  - We require to increase the stiffness of the damper suspension (mode #22).
  - The filter has to be checked (modes #4 and #6).
- Alignment range of the payload was given.
- The mechanical design was changed in order to ease the assembly.
- Installation work at Kamioka will begin soon.