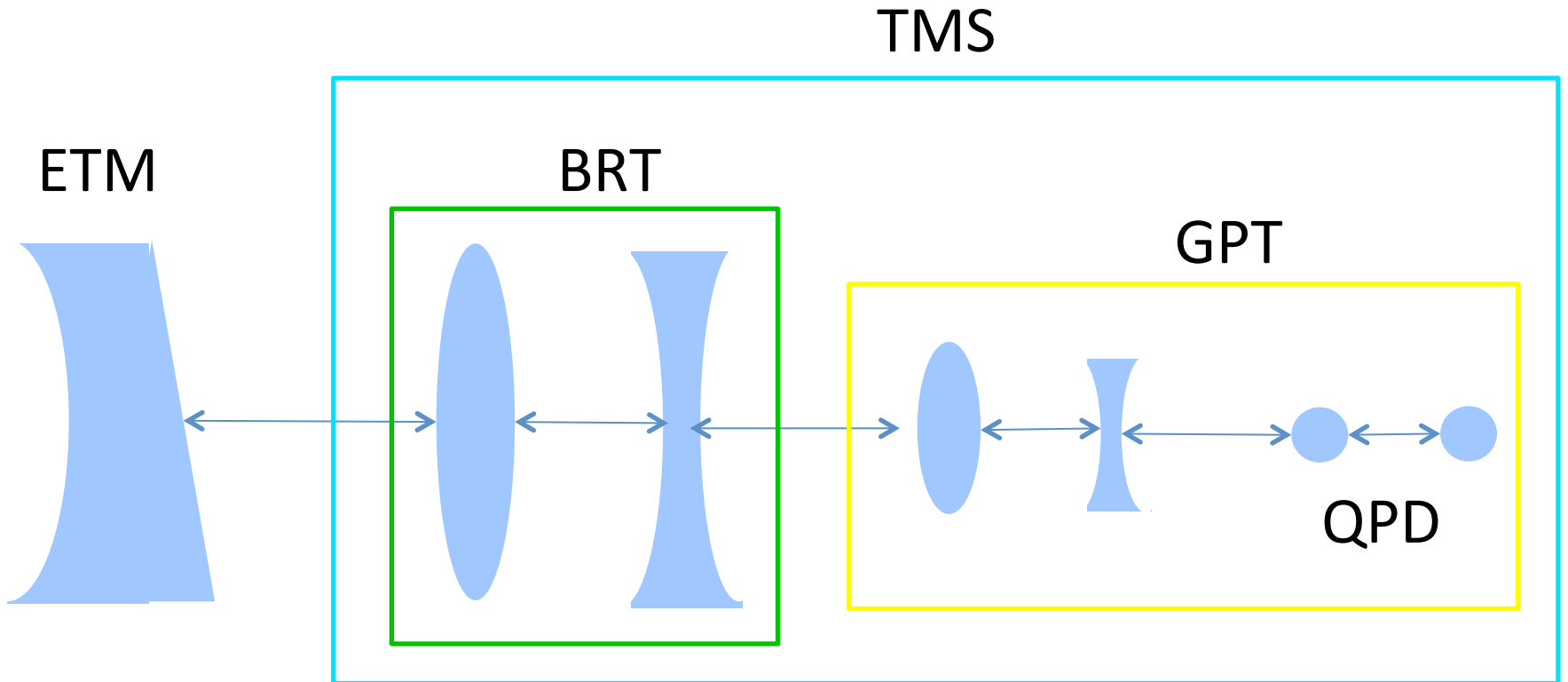


Displacement of BRT

Junko Katayama

Transmission Monitor System



What I did

Lateral and angular motion of BRT cause the noise on QPDs.

I computed those BRT motion noise and shot noise for both SOFT and HARD mode in two cases ;

- TMS table fixed on the ground
- TMS suspended by pendulum

Angular motion

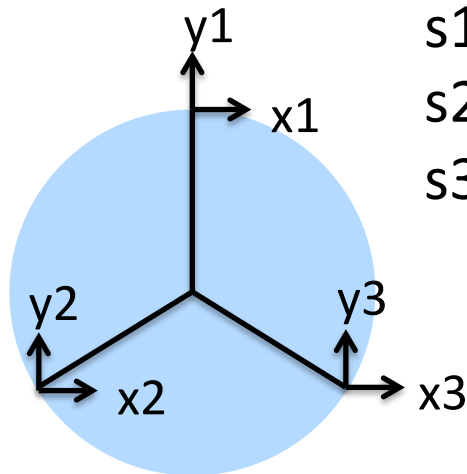
There are two types of angular motion.

1. Surface wave on the ground ($v=5000\text{m/s}$)

$$\Theta = 2\pi f * X_{\text{seis}} / v$$

2. Table motion (simulation data from ATC)

Z-rotation



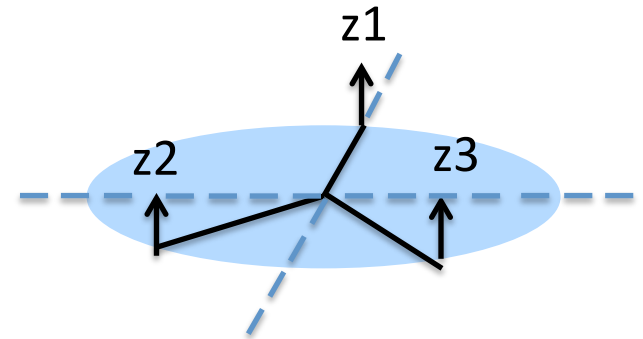
$$s1 = x1$$

$$s2 = -1/2 * x2 + \sqrt{3}/2 * y2$$

$$s3 = -1/2 * x3 - \sqrt{3}/2 * y3$$

$$R_{\theta z} = (s1 + s2 + s3) / 3$$

X,Y-rotation



$$R_{\theta xy} = (((z2 + z3) / 2) * 2 - z1)$$

Angular motion

comparing surface wave & table move

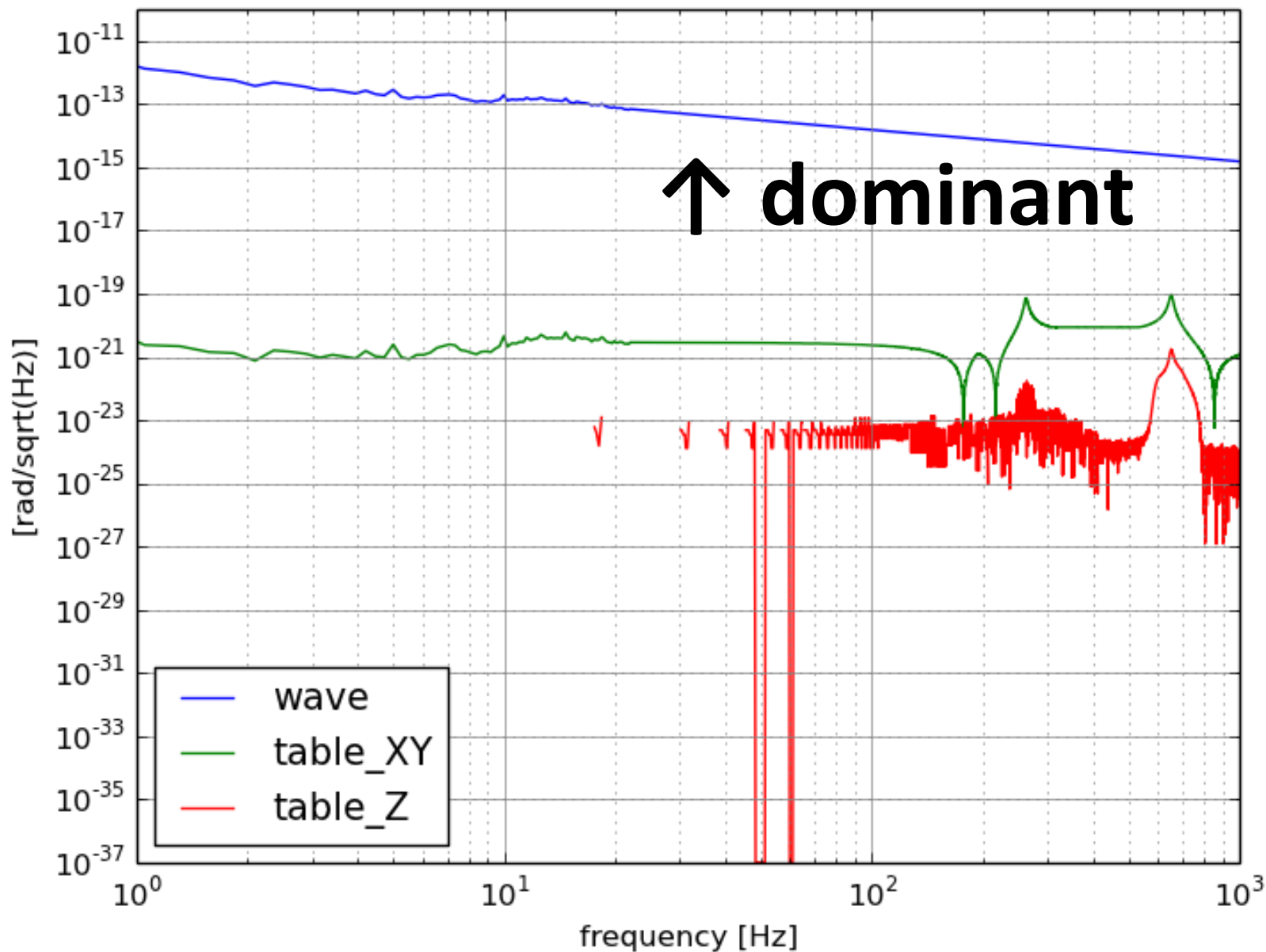


Table motion is quite smaller than surface wave
→ consider only surface wave as the angular motion of BRT

From the next slide,

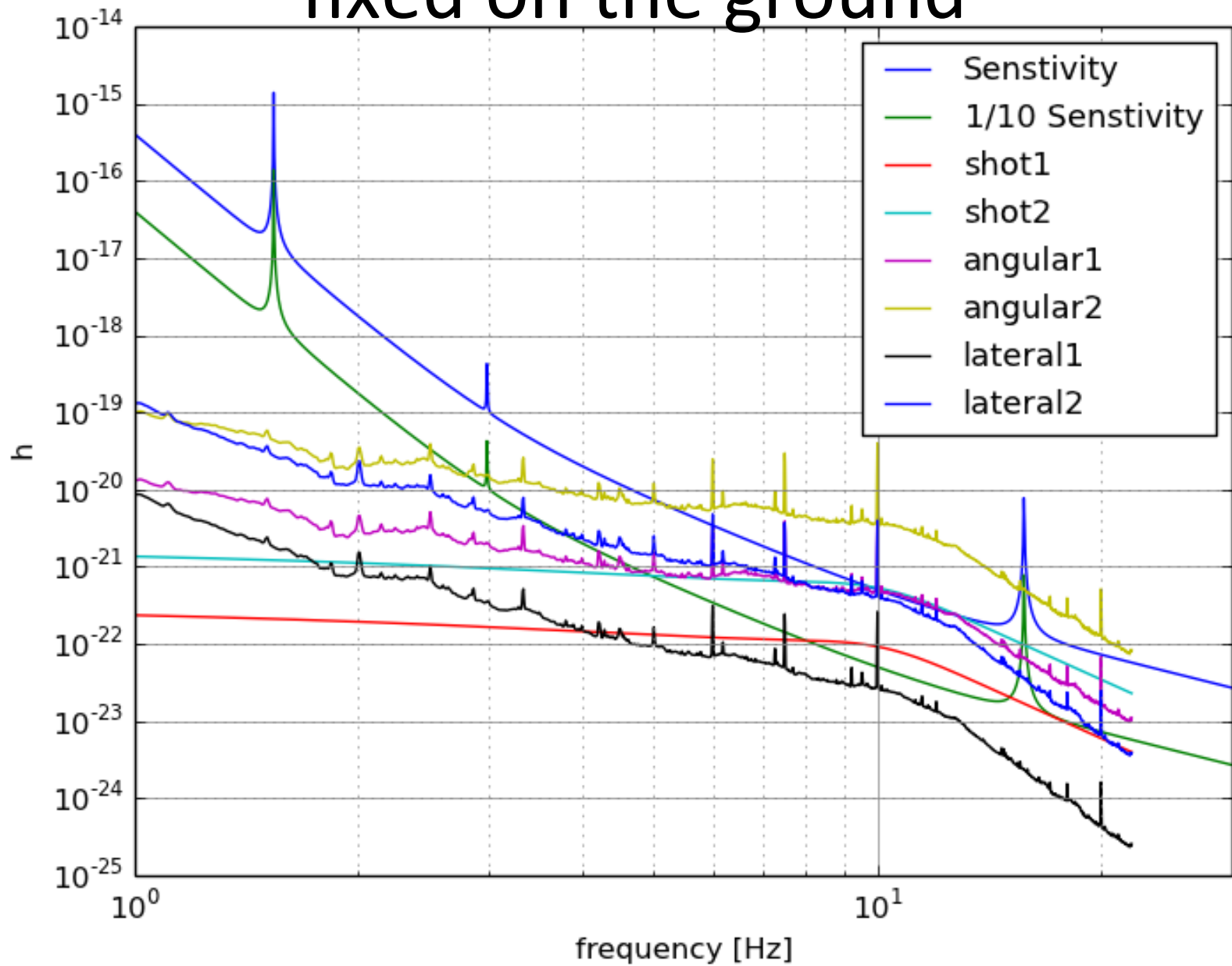
I computed the noise contribution to h for each SOFT and HARD mode.

There are two lines with each noise ;

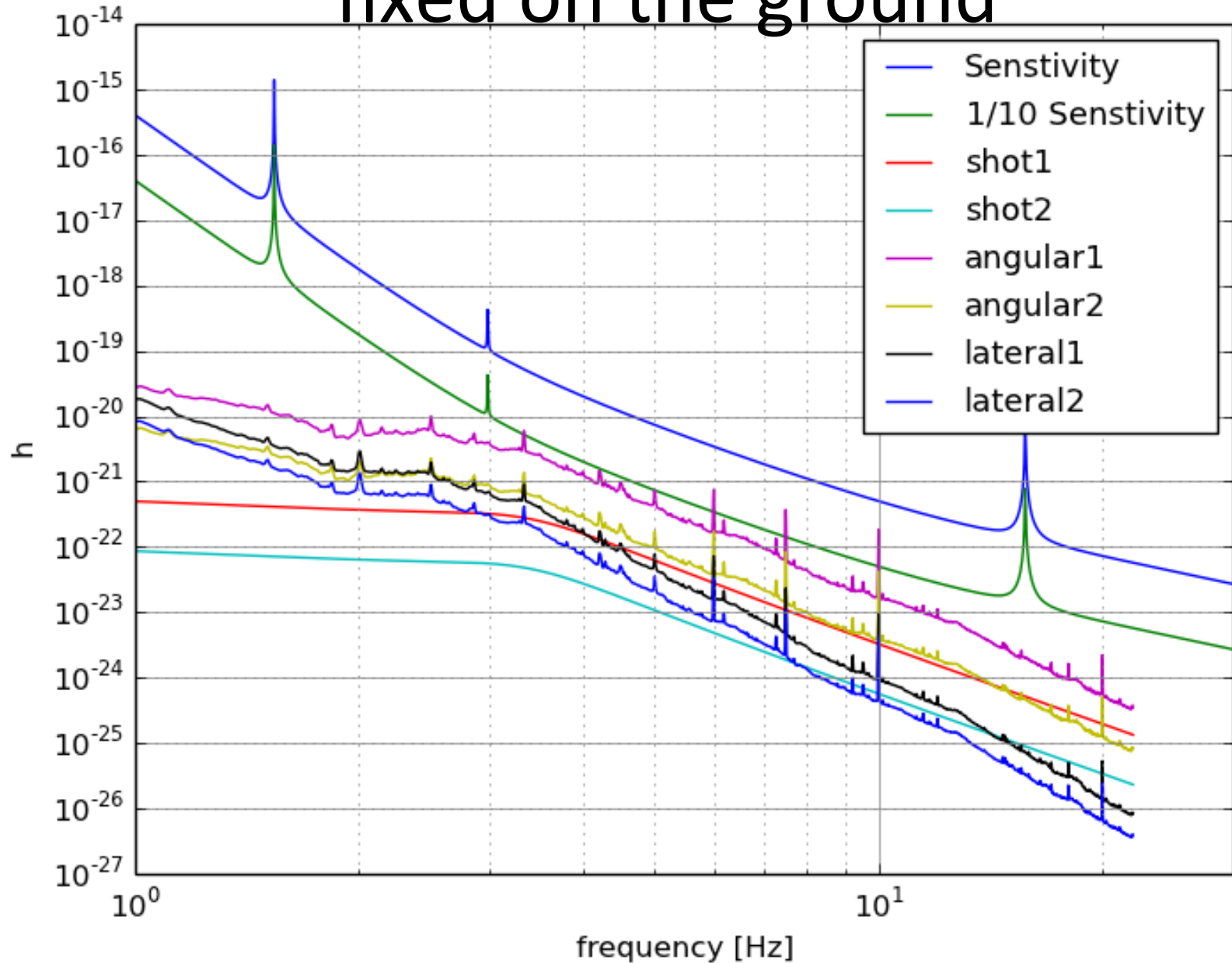
Ex) shot1 : shot noise on QPD1

shot2 : shot noise on QPD2

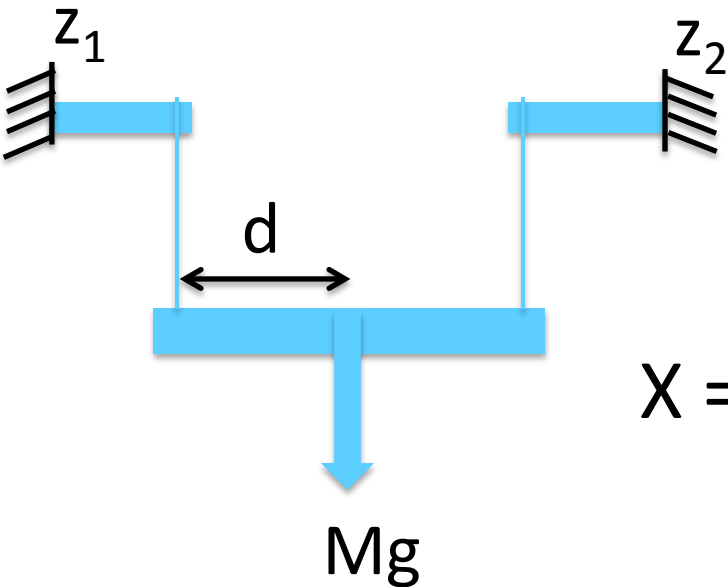
SOFT mode fixed on the ground



HARD mode fixed on the ground



Transfer Function



$$d=1\text{m} , M=200\text{kg}$$

$$X = 1/(1-(\omega/\omega_0)^2+i\omega/Q\omega_0)^* X_{\text{seis}}$$

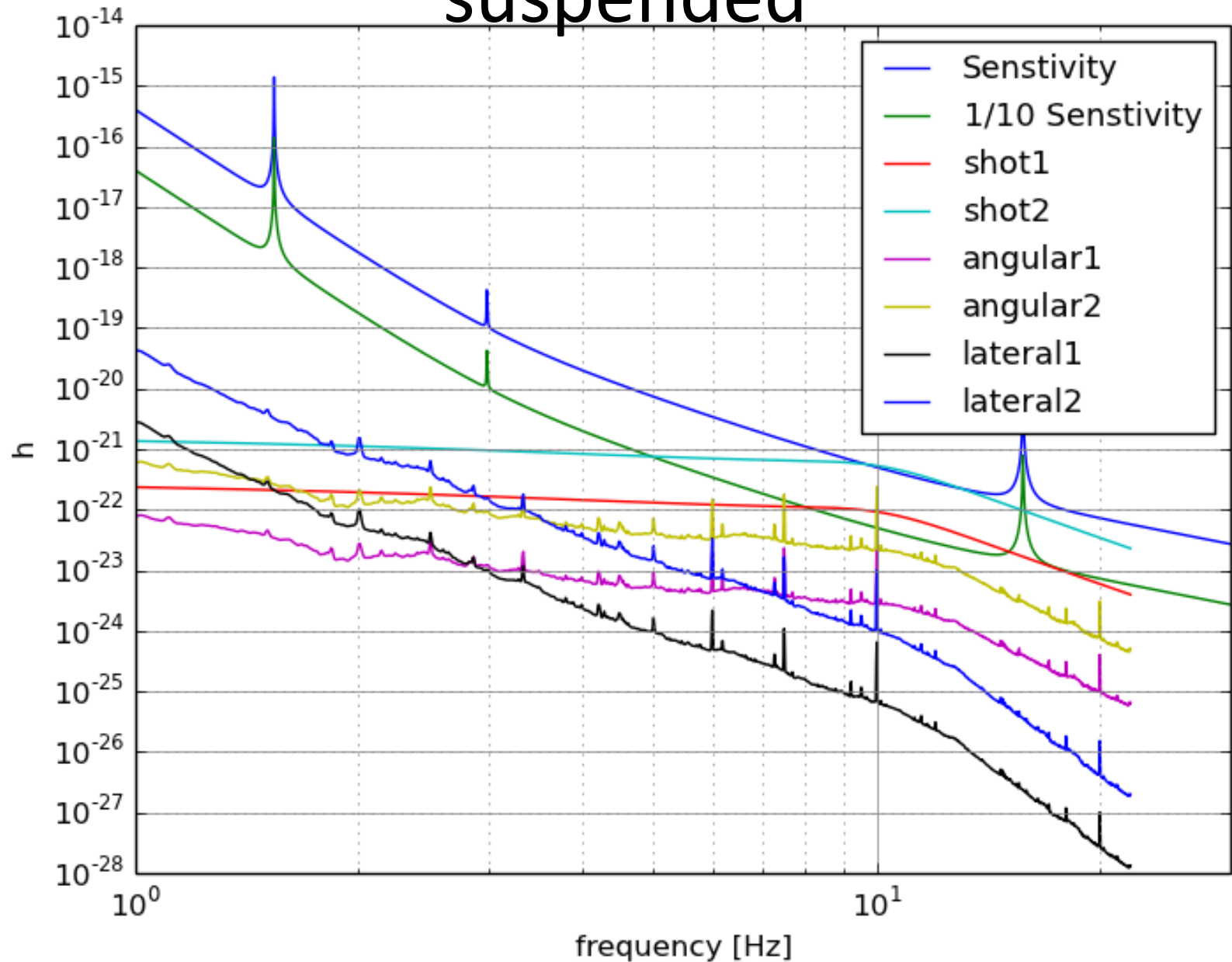
$$\Theta = dk(1\% * X_{\text{seis}})/(-lw^2+2d^2k)$$

$$z_2-z_1=1\% * X_{\text{seis}}$$

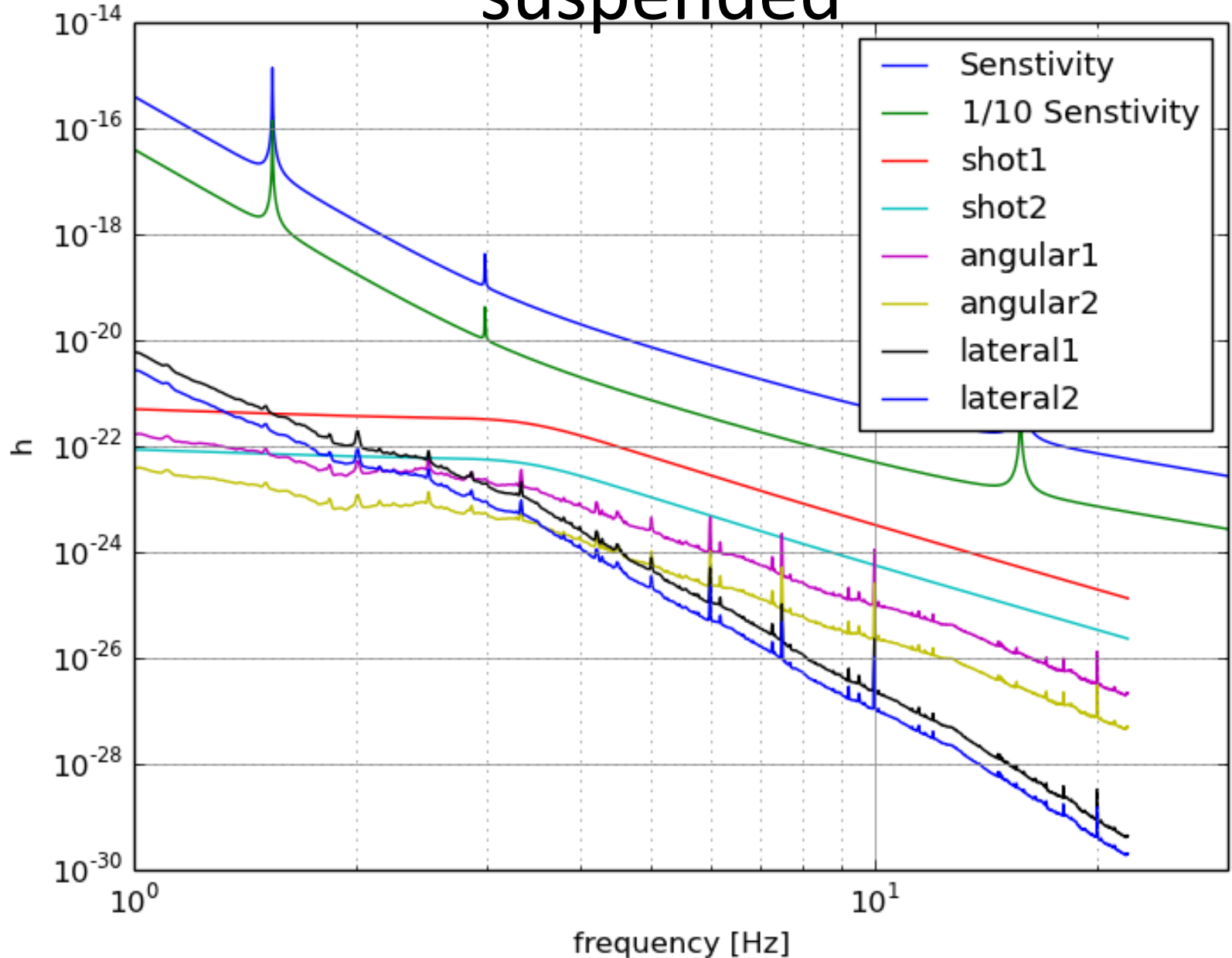
$$I=M(2d)^2/12$$

↑
Suspended by
2 wires

SOFT mode suspended



HARD mode suspended



Conclusion

- rotation of TMS table is not dominant
→ surface wave is dominant
- we can get HARD signal with TMS suspended
...cannot get SOFT because of the shot noise