

Alignment Sensing and Control for the KAGRA Interferometer

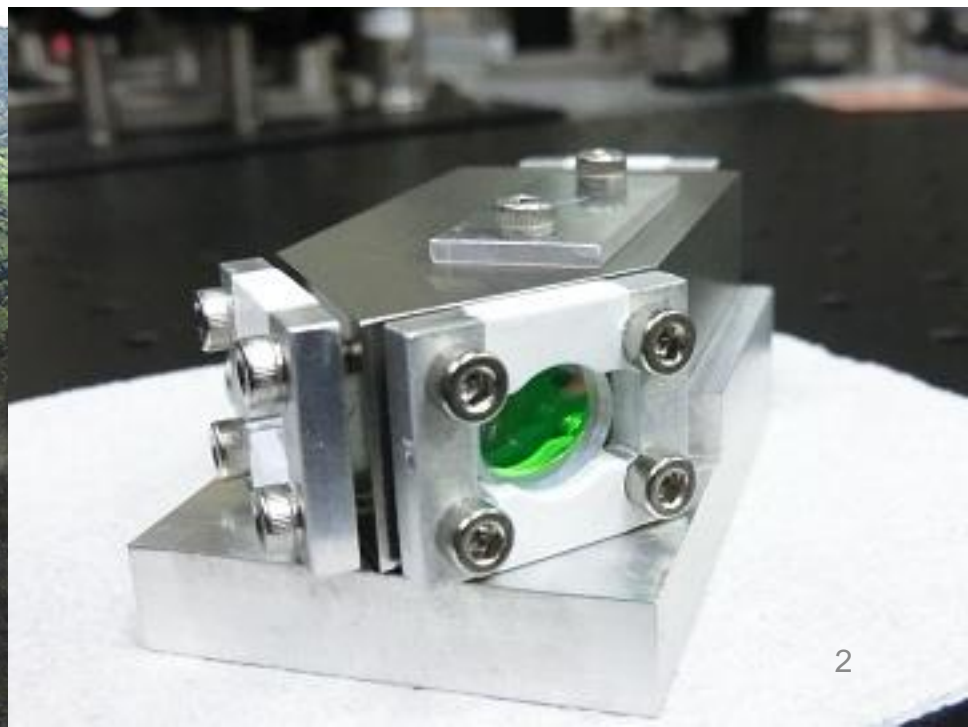
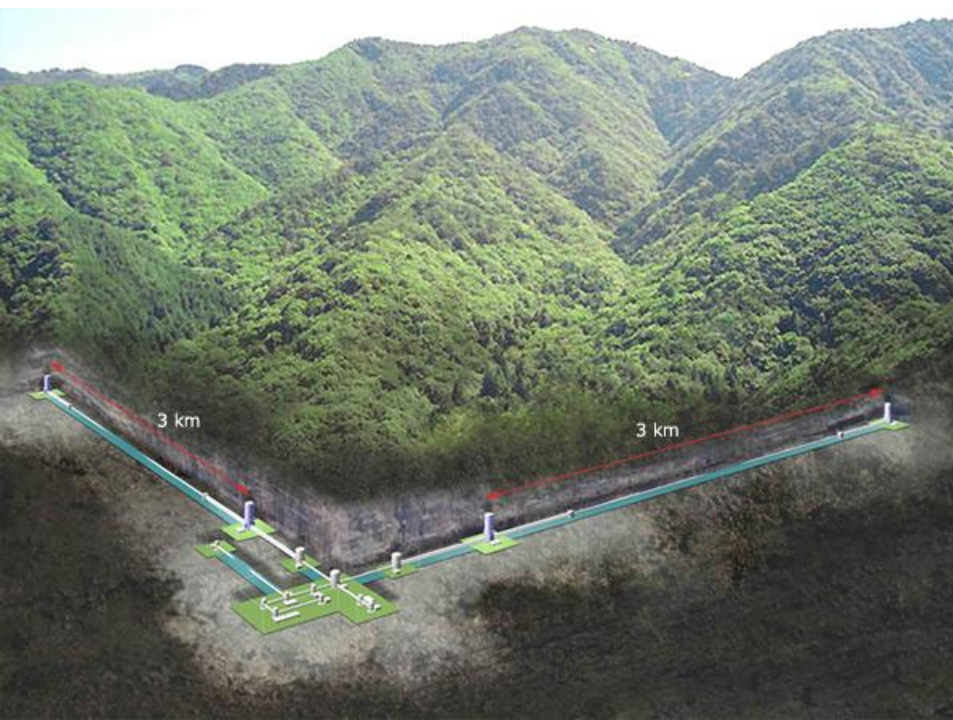
Yuta Michimura

Ando Group

Department of Physics, University of Tokyo

Self introduction

- Yuta Michimura (道村唯太 みちむらゆうた)
- Department of Physics, University of Tokyo
- Relativity-related experiment using some optics
 - designing KAGRA interferometer
 - light speed anisotropy search



Outline

- Introduction to interferometric GW detection
 - KAGRA interferometer
 - basic principle of GW detection
 - importance of length and alignment control
 - signal extraction of mirror motions
- Modeling alignment sensing and control scheme in KAGRA
 - difficulties
 - current status

References

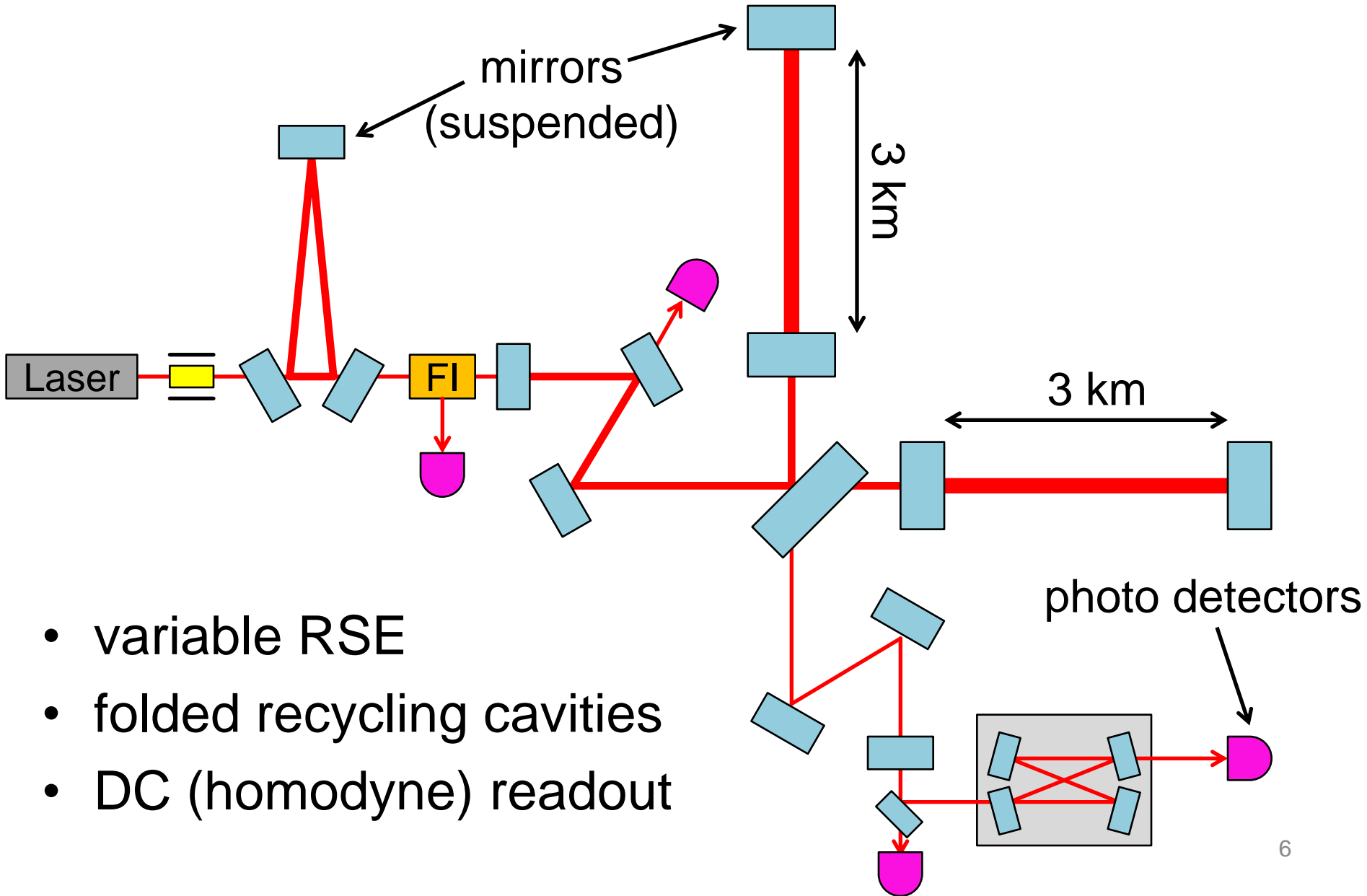
- Educational papers:
 - E. D. Black & R. N. Gutenkunst:
[Am. J. Phys. 71, 365 \(2003\)](#)
 - H. Kogelnik & T. Li:
[Appl. Opt. 5, 1550 \(1996\)](#)
- KAGRA specific:
 - Y. Aso, Y. Michimura, K. Somiya+:
[arXiv:1306.6747](#) (PRD accepted)
 - K. Somiya, KAGRA Collaboration:
[Classical Quantum Gravity 29, 124007 \(2012\)](#)

KAGRA

- cryogenic interferometric GW detector
- operation in full configuration ~2017

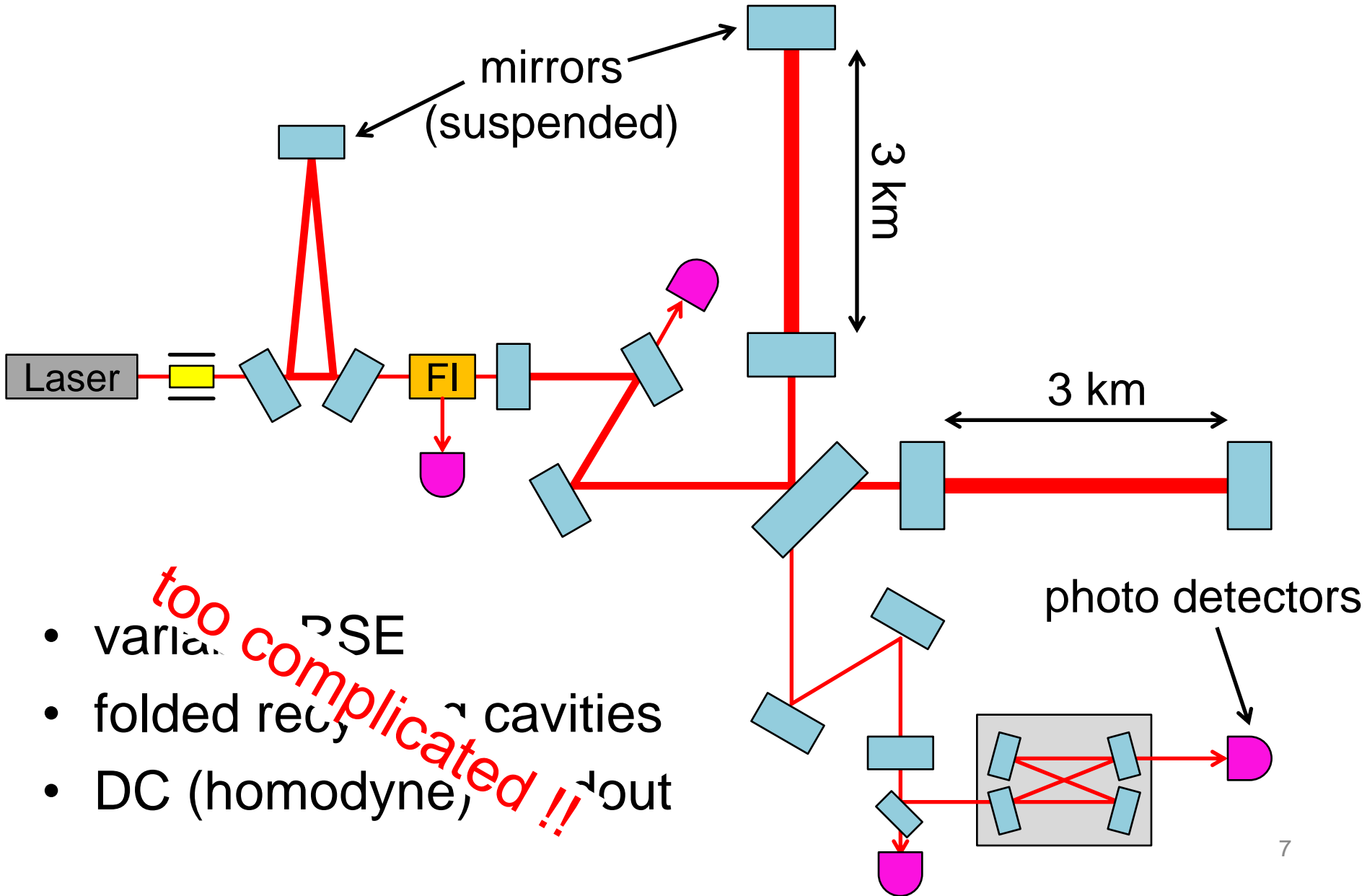


KAGRA interferometer



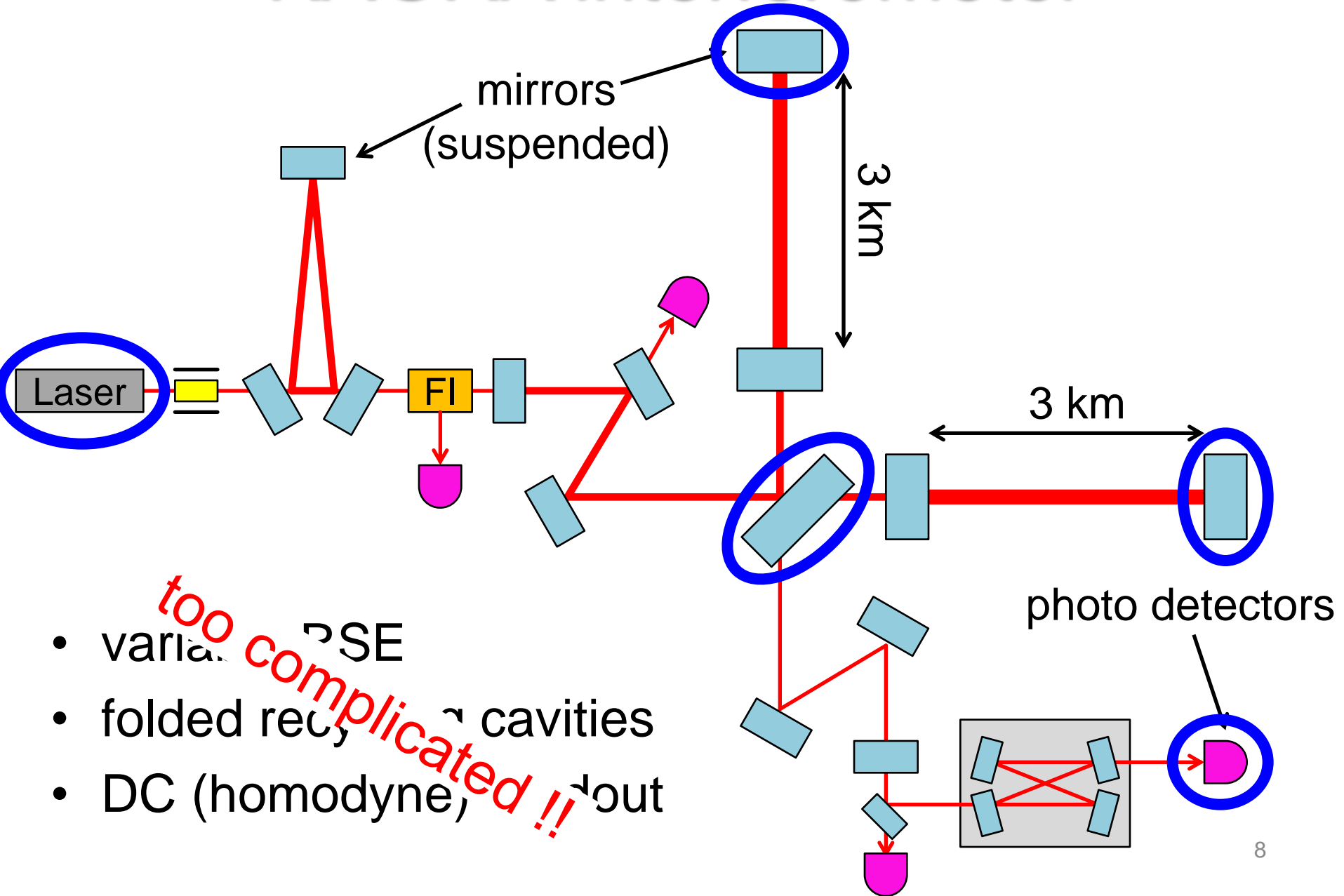
- variable RSE
- folded recycling cavities
- DC (homodyne) readout

KAGRA interferometer



- variable phase
 - folded recirculating cavities
 - DC (homodyne) output
- too complicated !!*

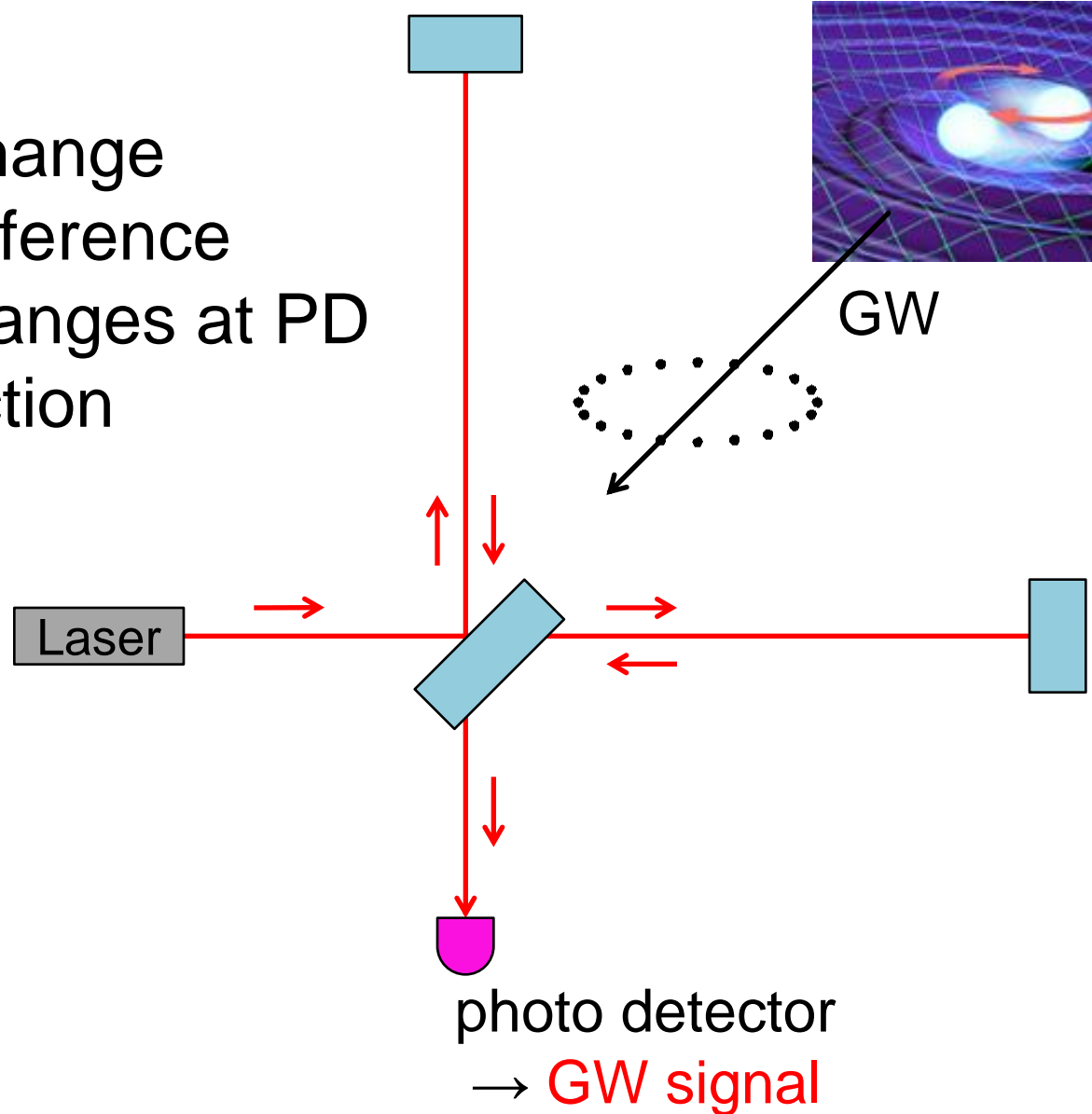
KAGRA interferometer



- variable phase
- folded recirculating cavities
- DC (homodyne) output

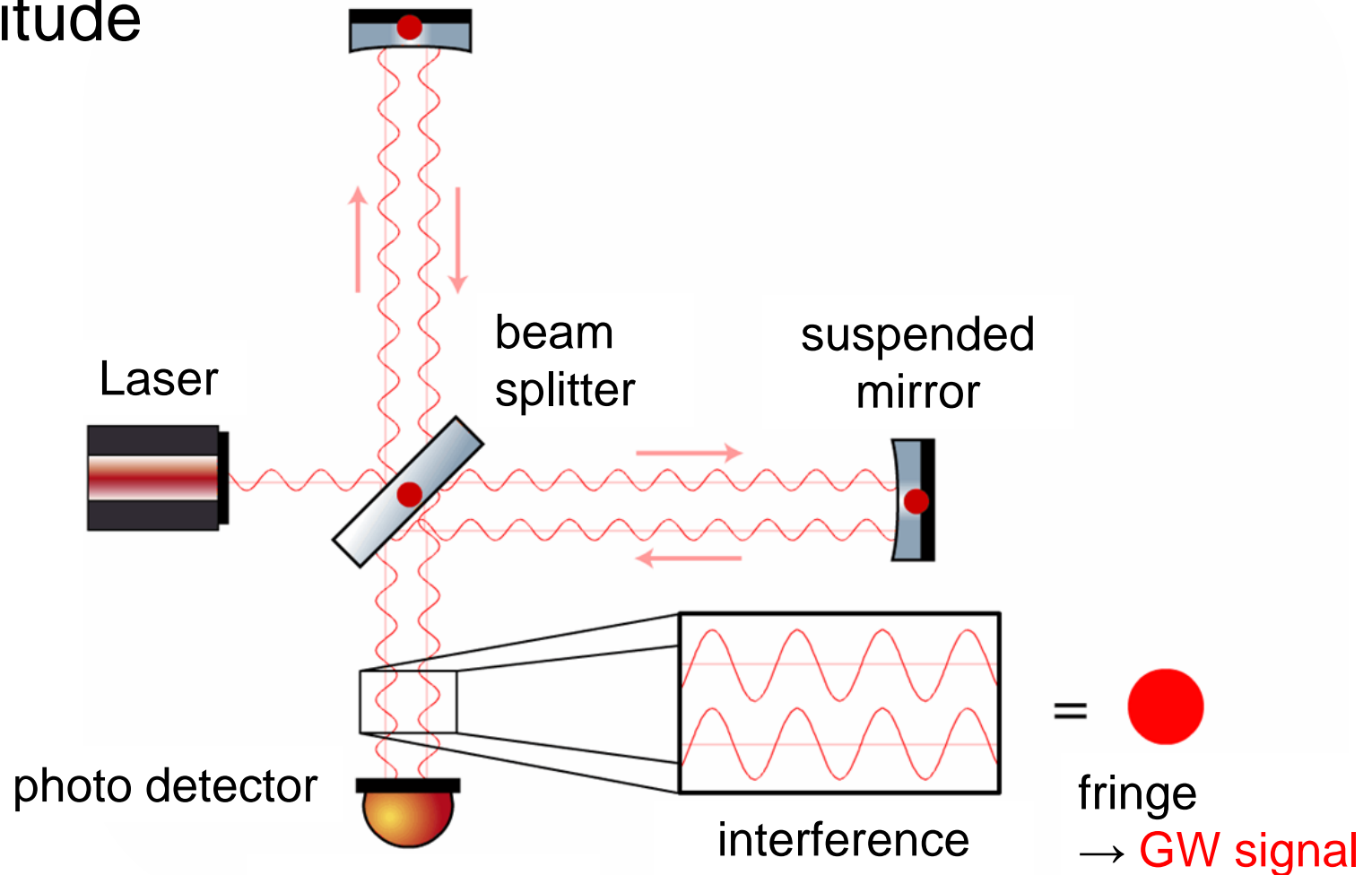
Michelson interferometer

- GW comes
 - lengths change
 - laser interference
 - fringe changes at PD
 - GW detection



MI as a GW detector

- fringe gives GW signal, but it is not linear to GW amplitude

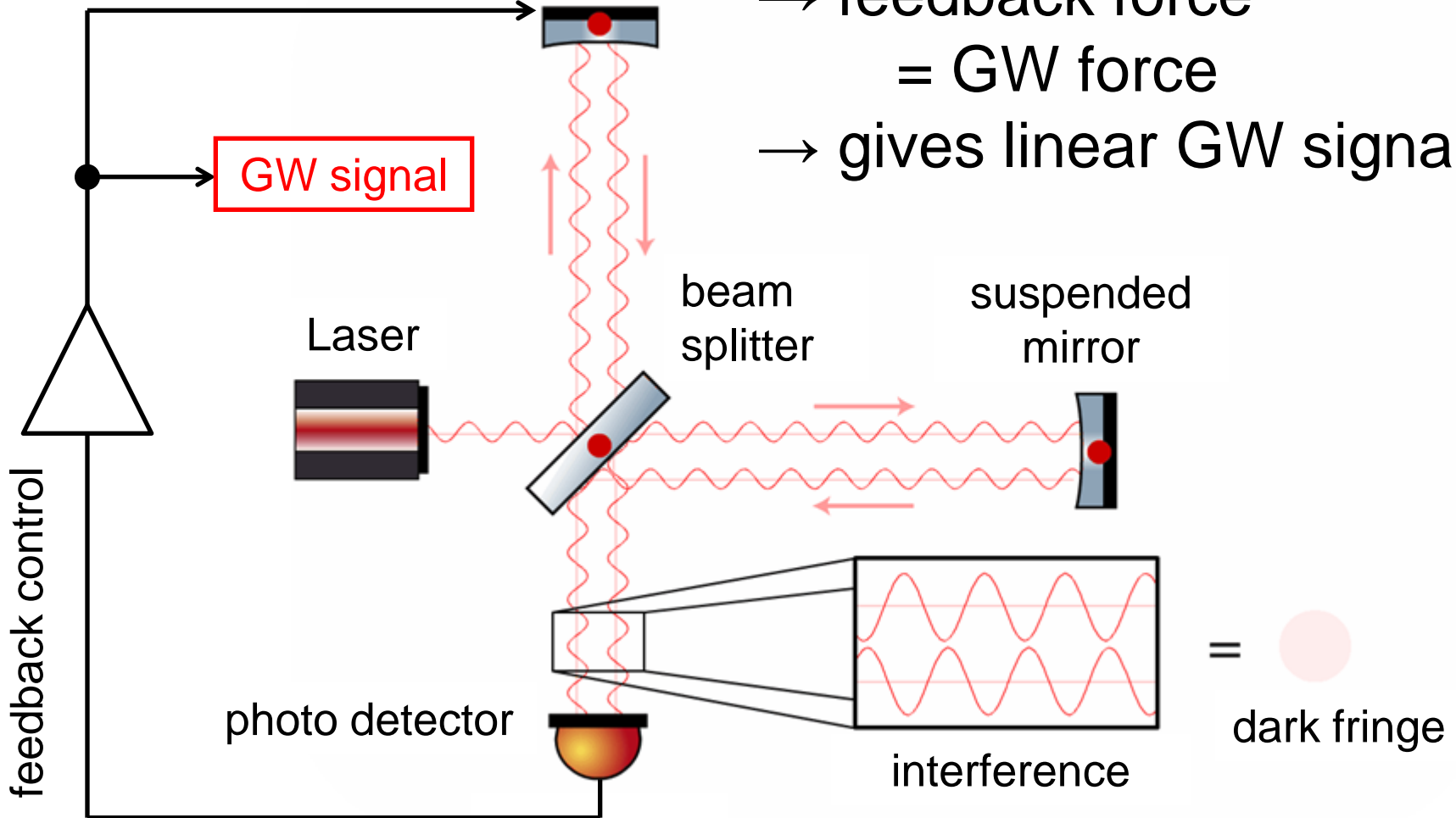


Controlling the interferometer

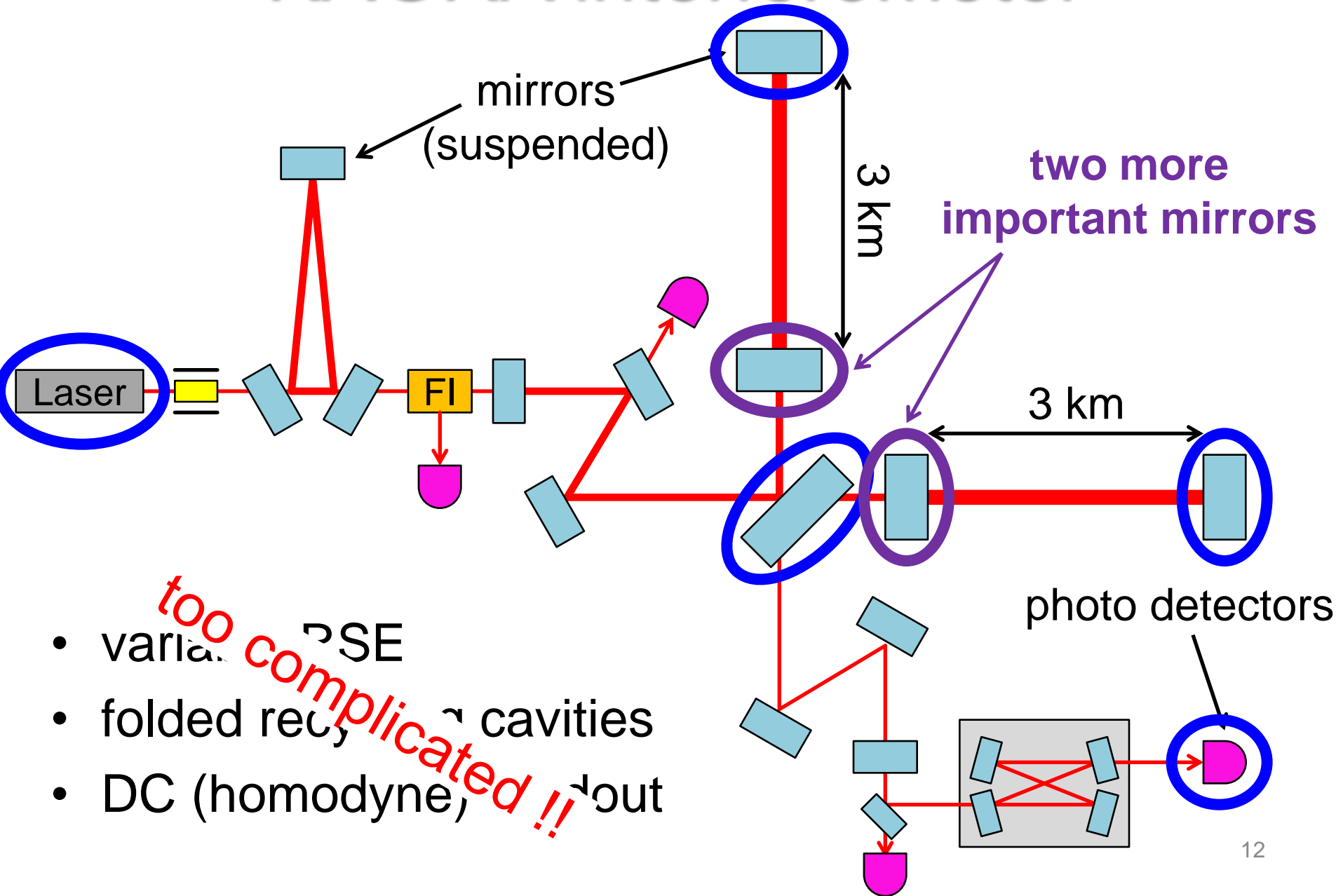
- control mirror motion so that fringe doesn't change

→ feedback force
= GW force

→ gives linear GW signal



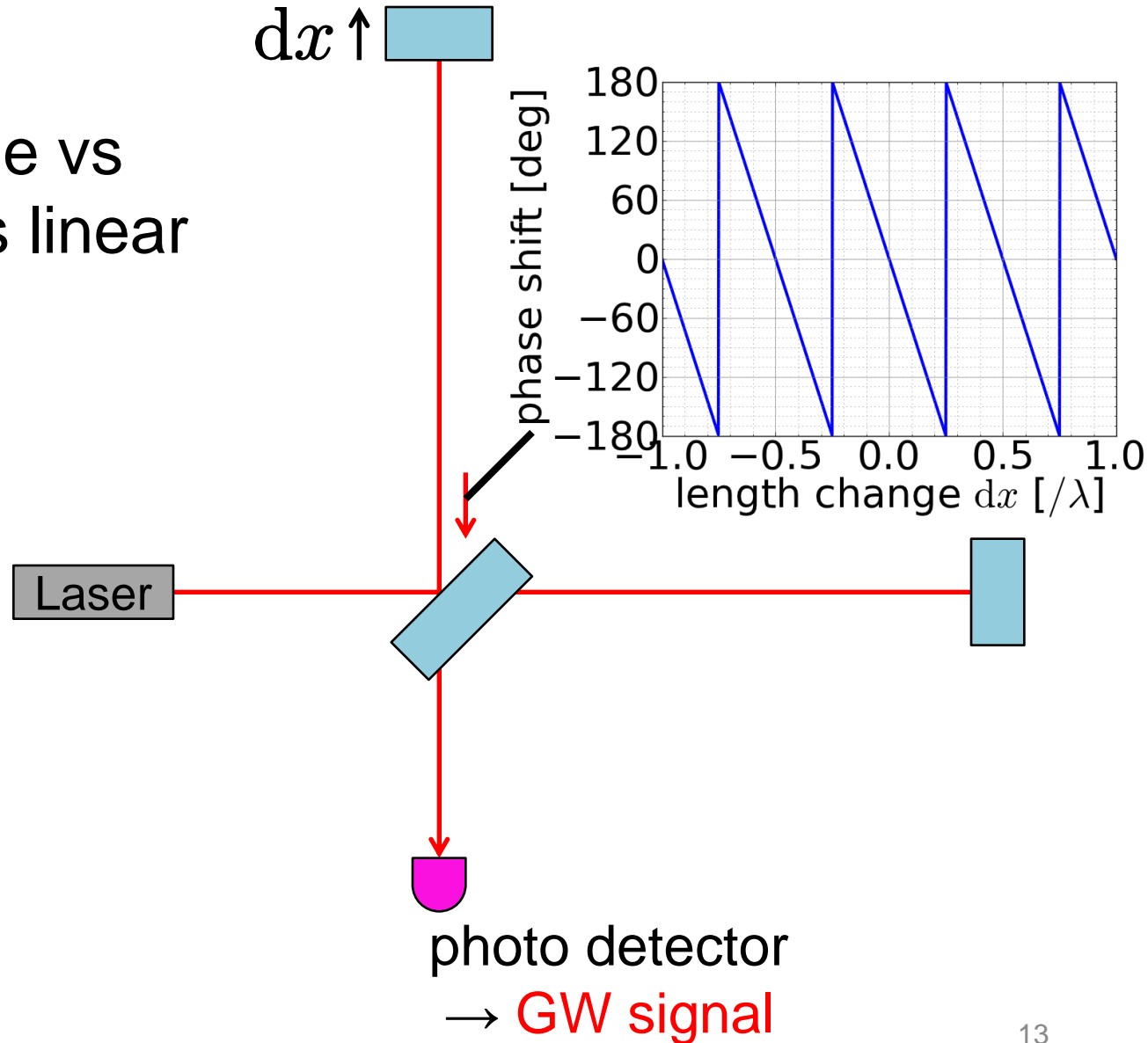
KAGRA interferometer



- variable phase
 - folded recirculating cavities
 - DC (homodyne) output
- too complicated !!*

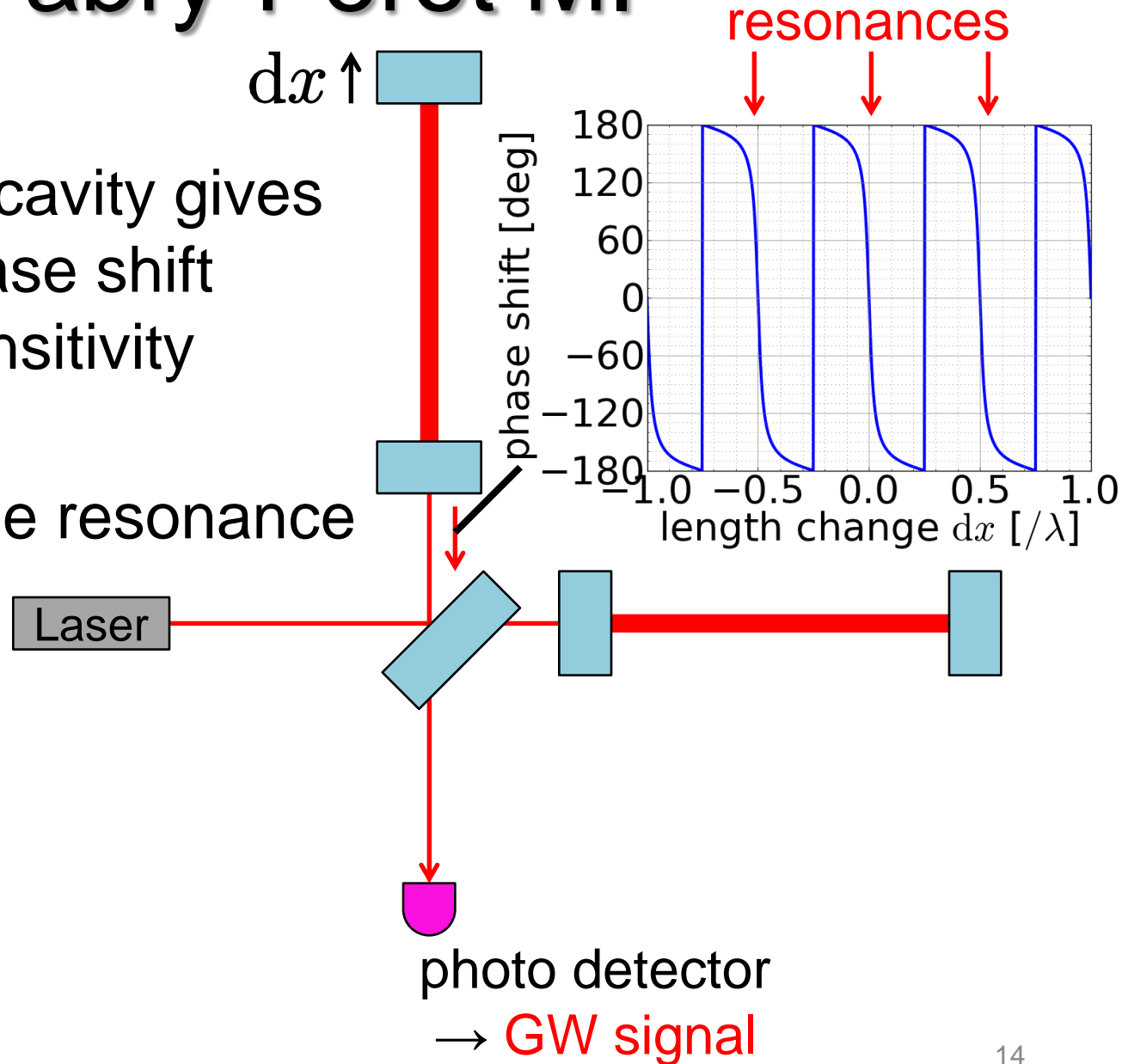
Michelson interferometer

- length change vs phase shift is linear



Fabry-Perot MI

- Fabry-Perot cavity gives enlarged phase shift
→ better sensitivity to GW
- but only at the resonance

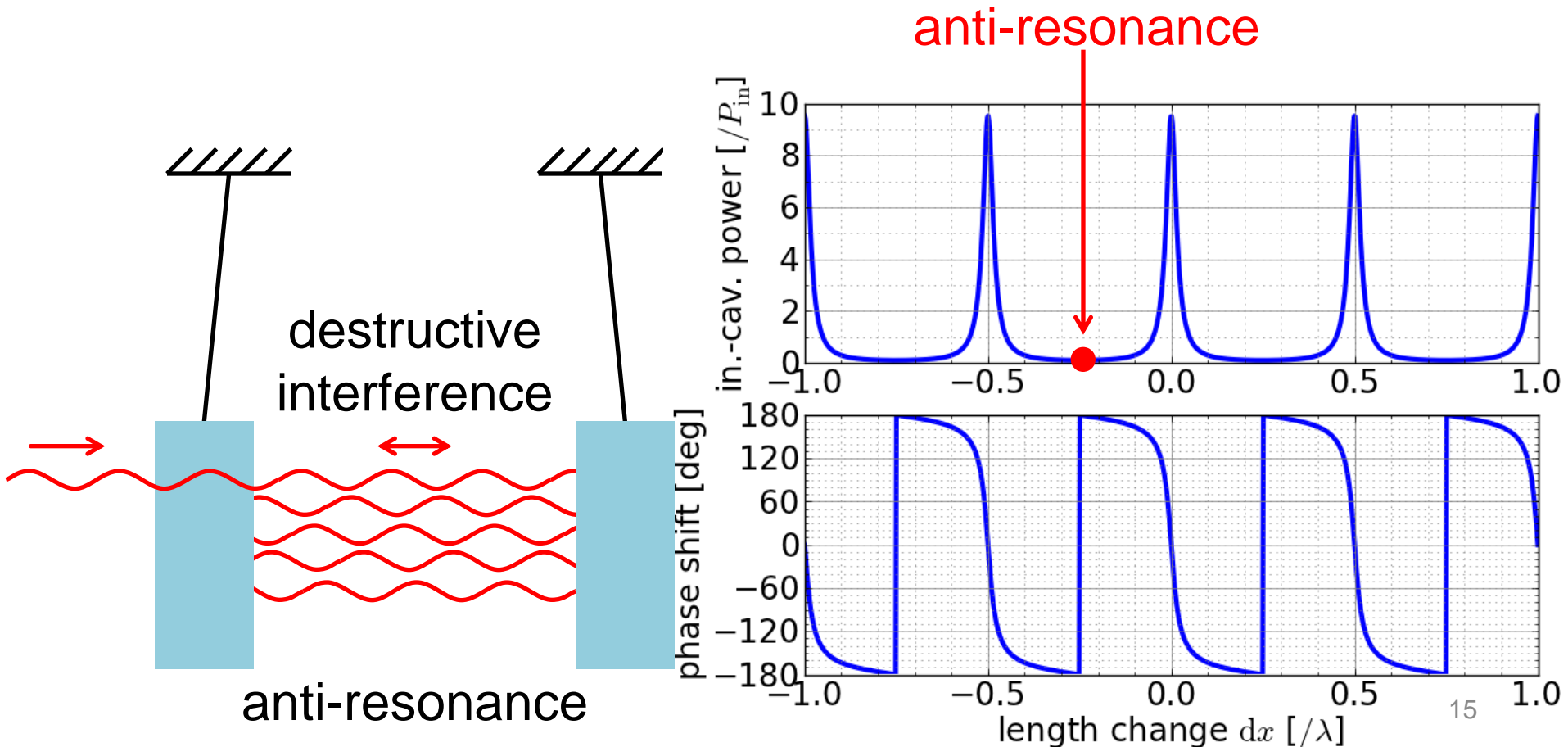


Resonance of FP cavity

- laser beam resonates when

$$2L = m\lambda \quad (m \text{ is an integer})$$

- intra-cavity power builds up at resonance

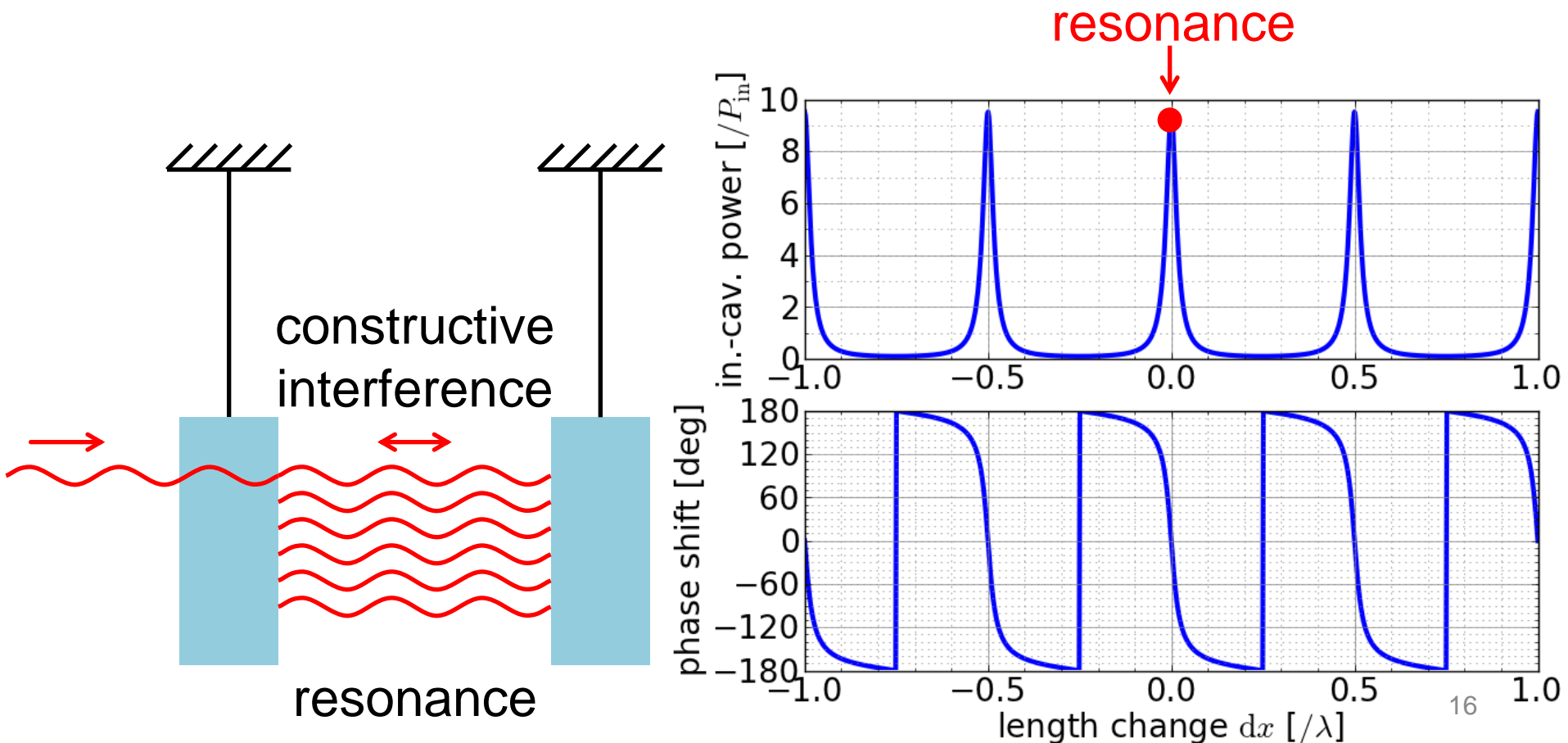


Resonance of FP cavity

- laser beam resonates when

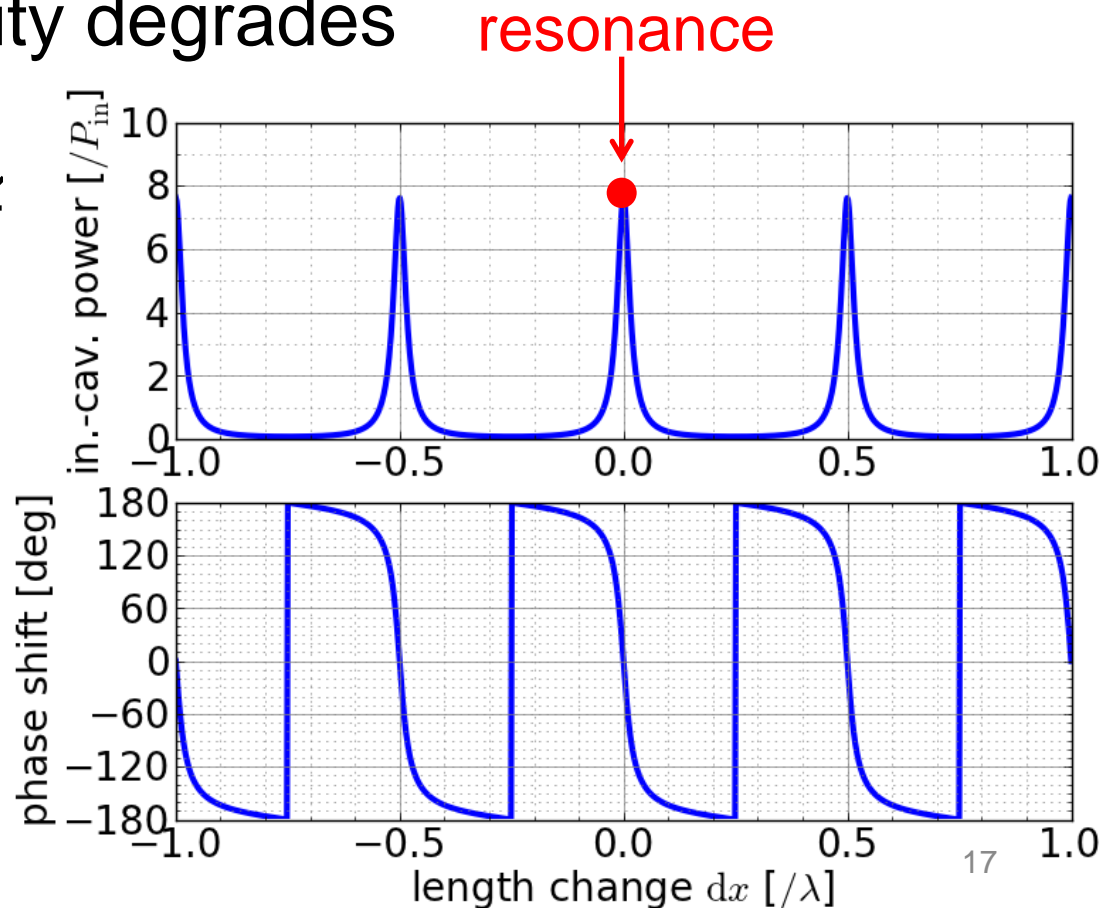
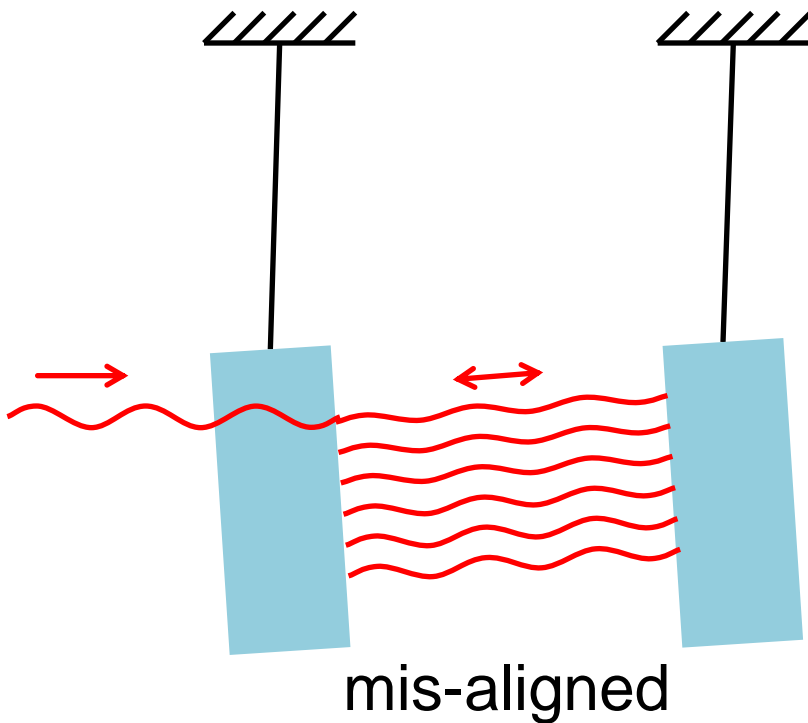
$$2L = m\lambda \quad (m \text{ is an integer})$$

- intra-cavity power builds up at resonance



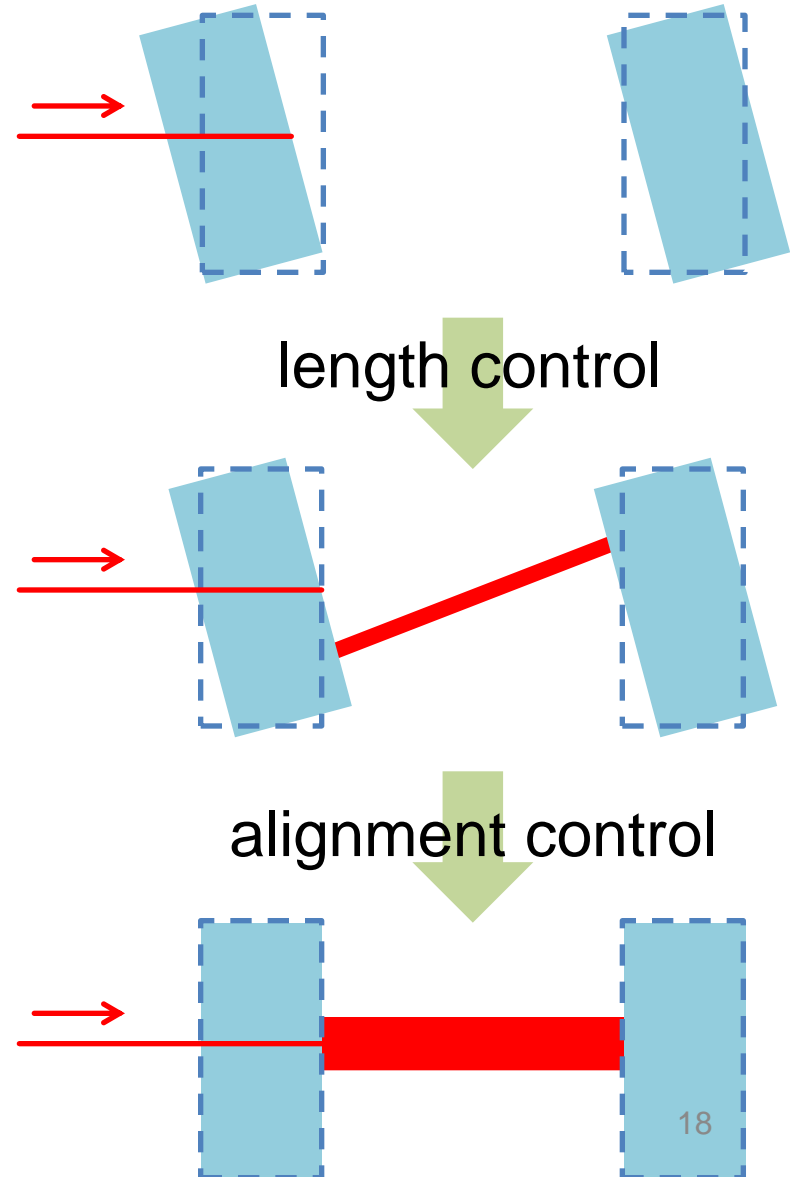
Alignment of FP cavity

- mis-alignment degrades coupling of incident beam and FP cavity
 - intra-cavity power degrades
 - phase sensitivity degrades



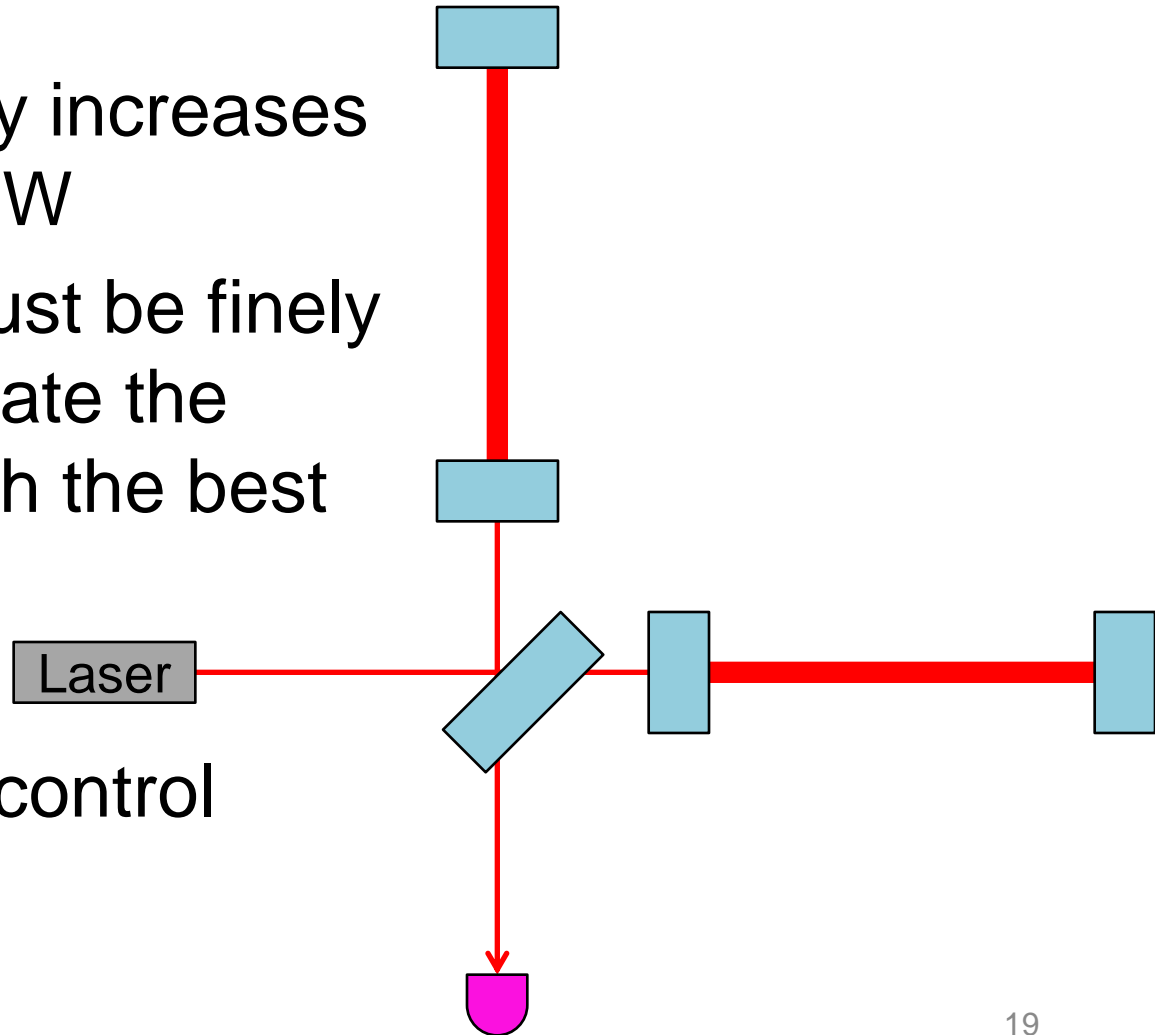
Operating point of FP cavity

- length control (LSC)
 - keeps FP at resonance
($\sim 1 \mu\text{m} \rightarrow < 0.1 \text{ nm}$)
- alignment control (ASC)
 - keeps coupling of FP
and incident beam
at maximum
($\sim 1 \text{ urad} \rightarrow < 10 \text{ nrad}$)
- length control and
alignment control is
essential for GW detection



Summary 1/3

- Interferometric GW detector is basically Michelson interferometer
- Fabry-Perot cavity increases its sensitivity to GW
- Mirror motions must be finely controlled to operate the interferometer with the best sensitivity
- Then how do we control them?



Well, it's pretty complicated

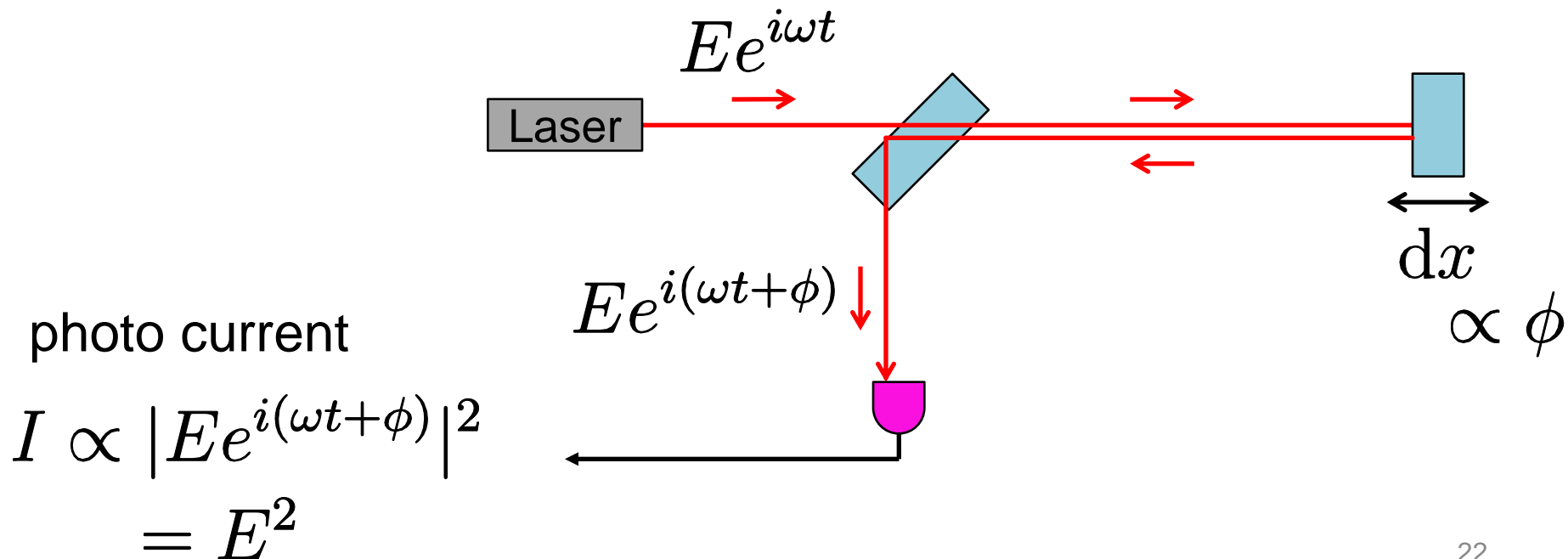
- I'm not sure if you want to know how

Well, it's pretty complicated

- I'm not sure if you want to know how
- But I will try to explain how anyway
- You will learn about
 - homodyne phase detection and heterodyne phase detection
 - phase modulation of laser beam
 - Gaussian beam

GW detection is phase detection

- GW changes length
→ phase of laser beam (EM wave) changes
- but photo detector is not sensitive to the phase of the laser beam
- Photo detector is sensitive to amplitude



Reference beam is needed

- if there's a reference beam, you can convert phase change to amplitude change
- that's why we need interferometry

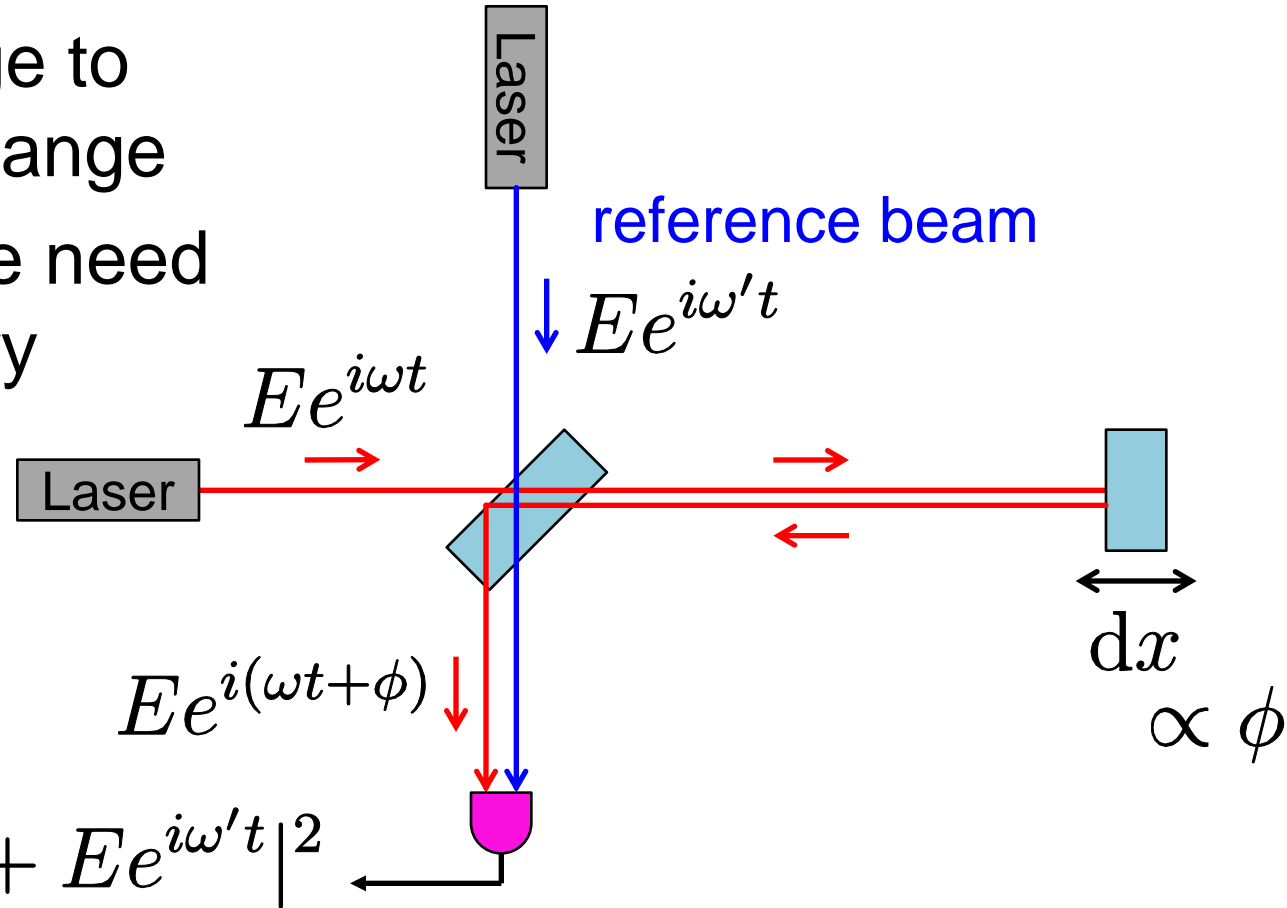


photo current

$$I \propto |Ee^{i(\omega t + \phi)} + Ee^{i\omega' t}|^2$$

$$= 2E^2 [1 + \cos((\omega - \omega')t + \phi)]$$

Homodyne and heterodyne

- if $\omega - \omega' = 0$

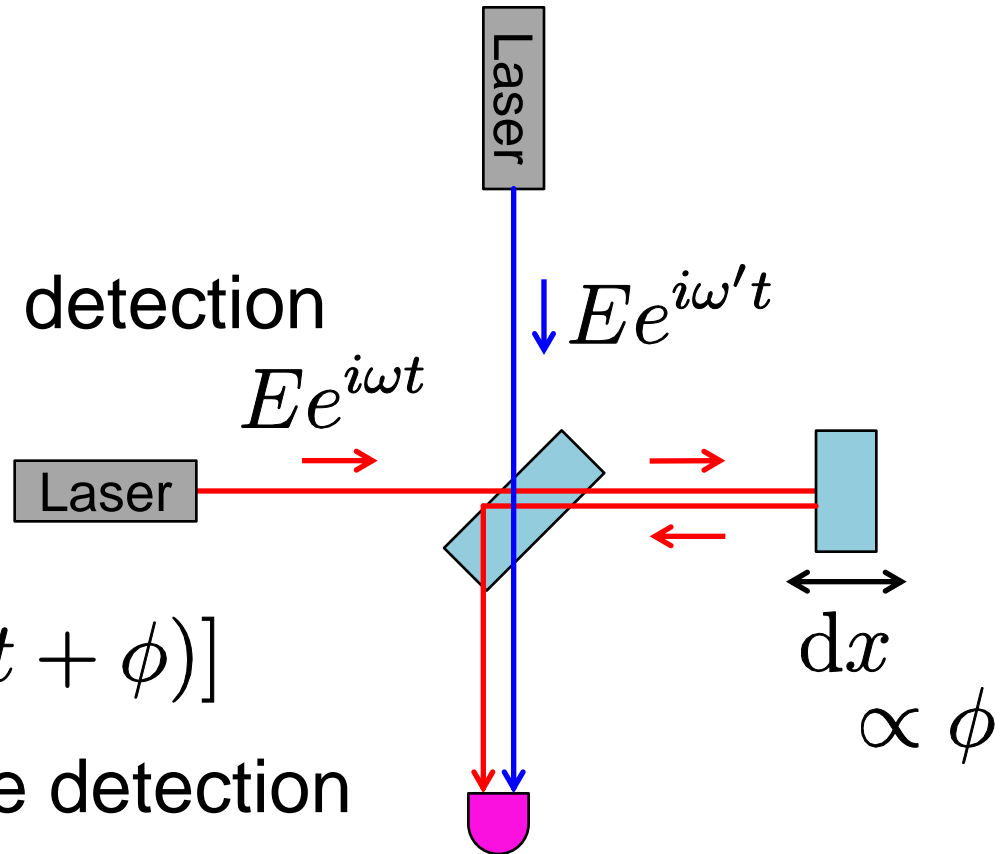
$$I \propto 2E^2[1 + \cos \phi]$$

→ homodyne phase detection

- if $\omega - \omega' = \Omega$

$$I \propto 2E^2[1 + \cos(\Omega t + \phi)]$$

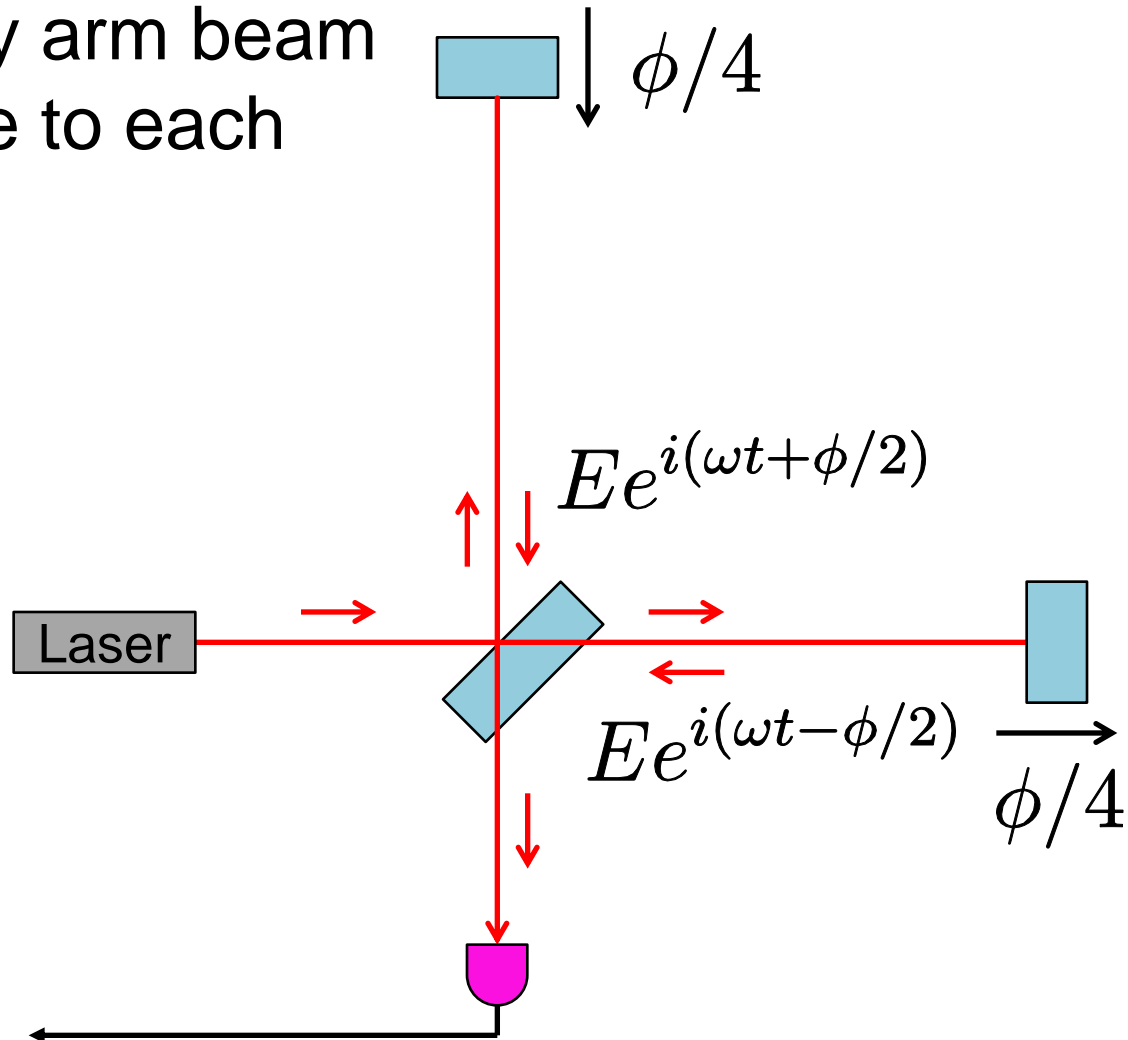
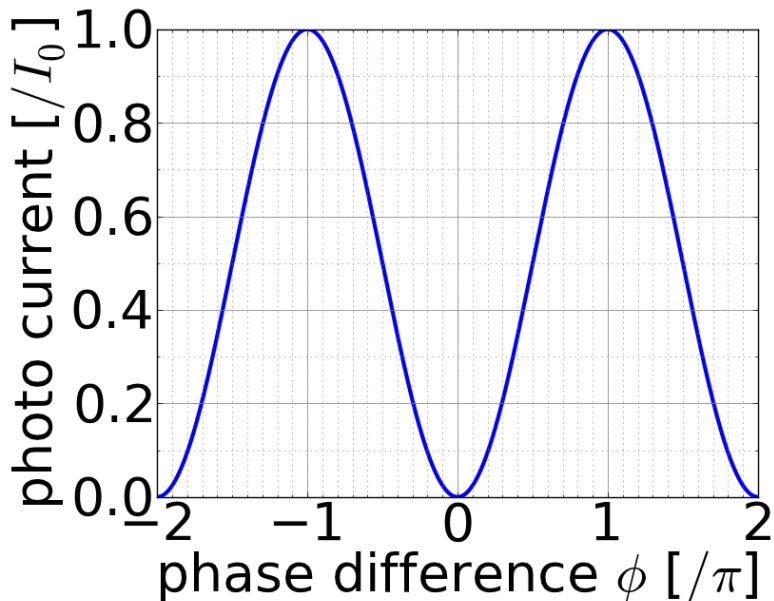
→ heterodyne phase detection



Michelson is homodyne

- x arm beam and y arm beam act as a reference to each other

$$I \propto \frac{1}{2} E^2 (1 - \cos \phi)$$

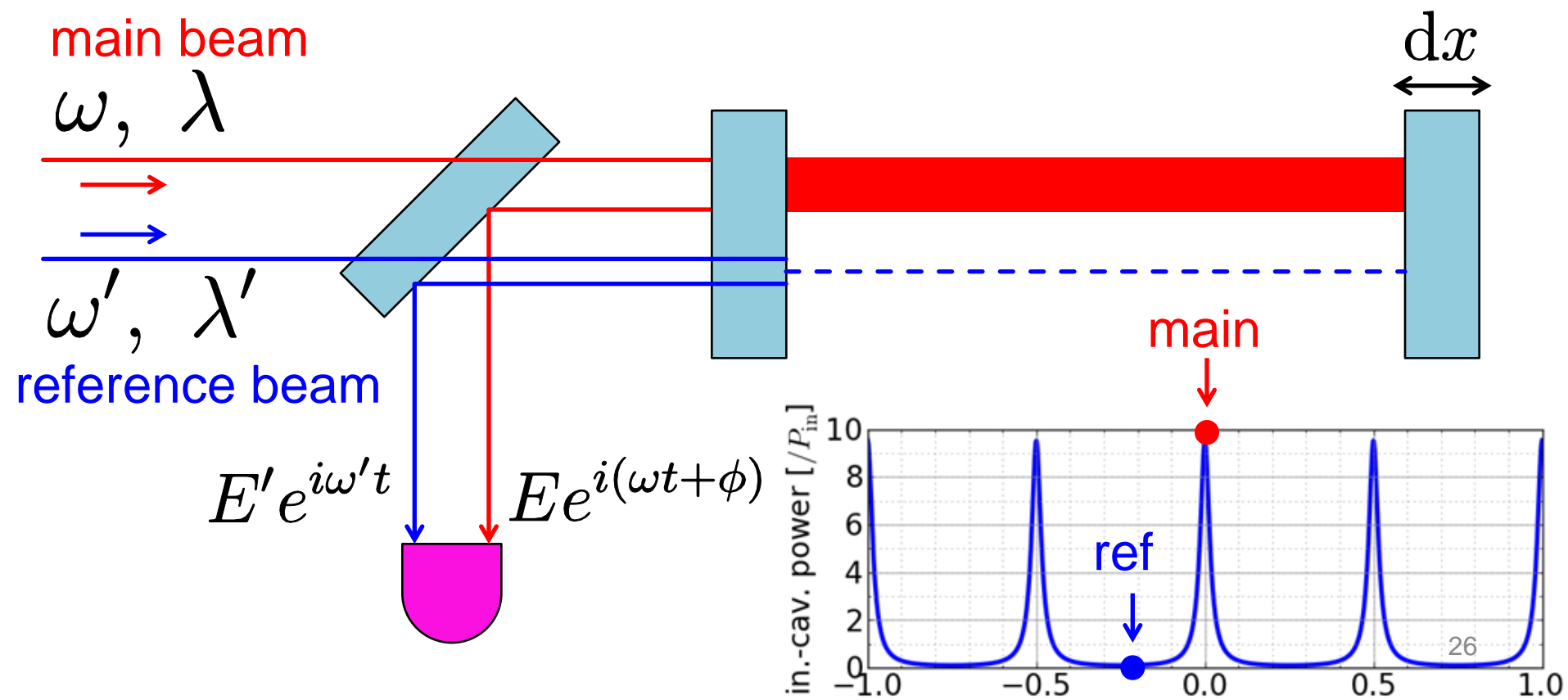


Heterodyne for Fabry-Perot cavity

- put 2 beams with different frequencies
- main beam resonates, but reference beam doesn't

$$2L = m\lambda$$

$$2L \neq m\lambda'$$



Phase modulation

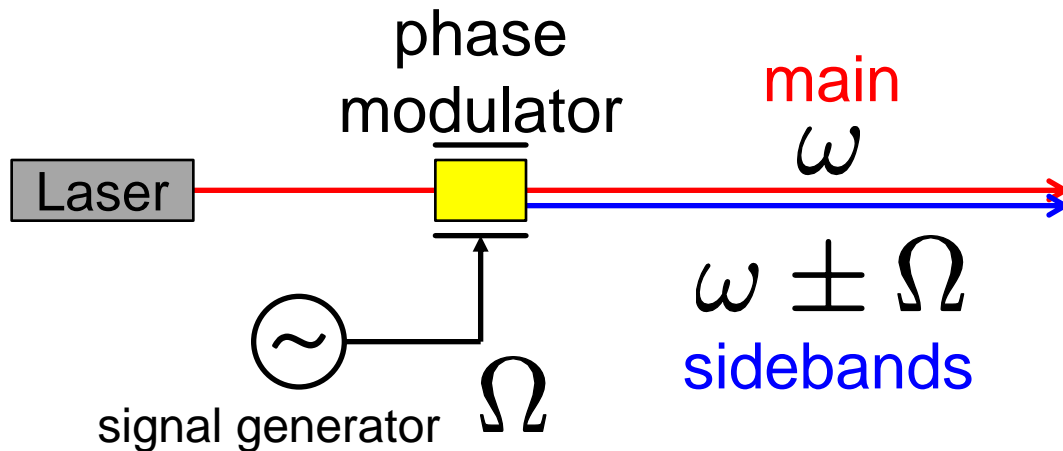
- electric field of a laser beam (plane wave)

$$E = E_0 e^{i\omega t}$$

- phase modulation creates sidebands

$$E = E_0 e^{i(\omega t + \beta \sin \Omega t)}$$

$$\simeq E_0 \left[\underbrace{J_0(\beta)}_{\text{main}} e^{i\omega t} + \underbrace{J_1(\beta)}_{\text{upper sideband}} e^{i(\omega + \Omega)t} - \underbrace{J_1(\beta)}_{\text{lower sideband}} e^{i(\omega - \Omega)t} \right]$$



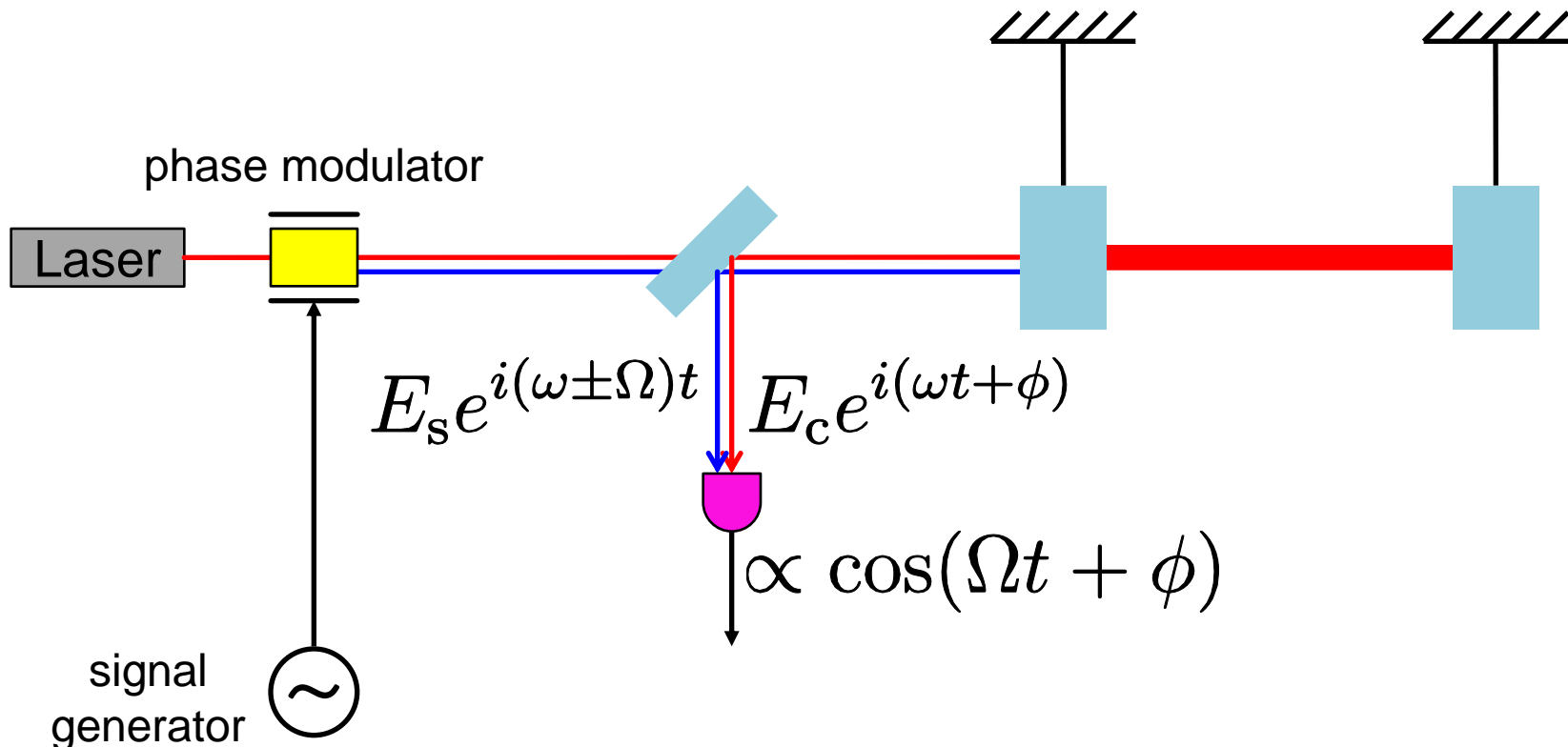
electro-optic phase modulator



- sidebands work as reference beam

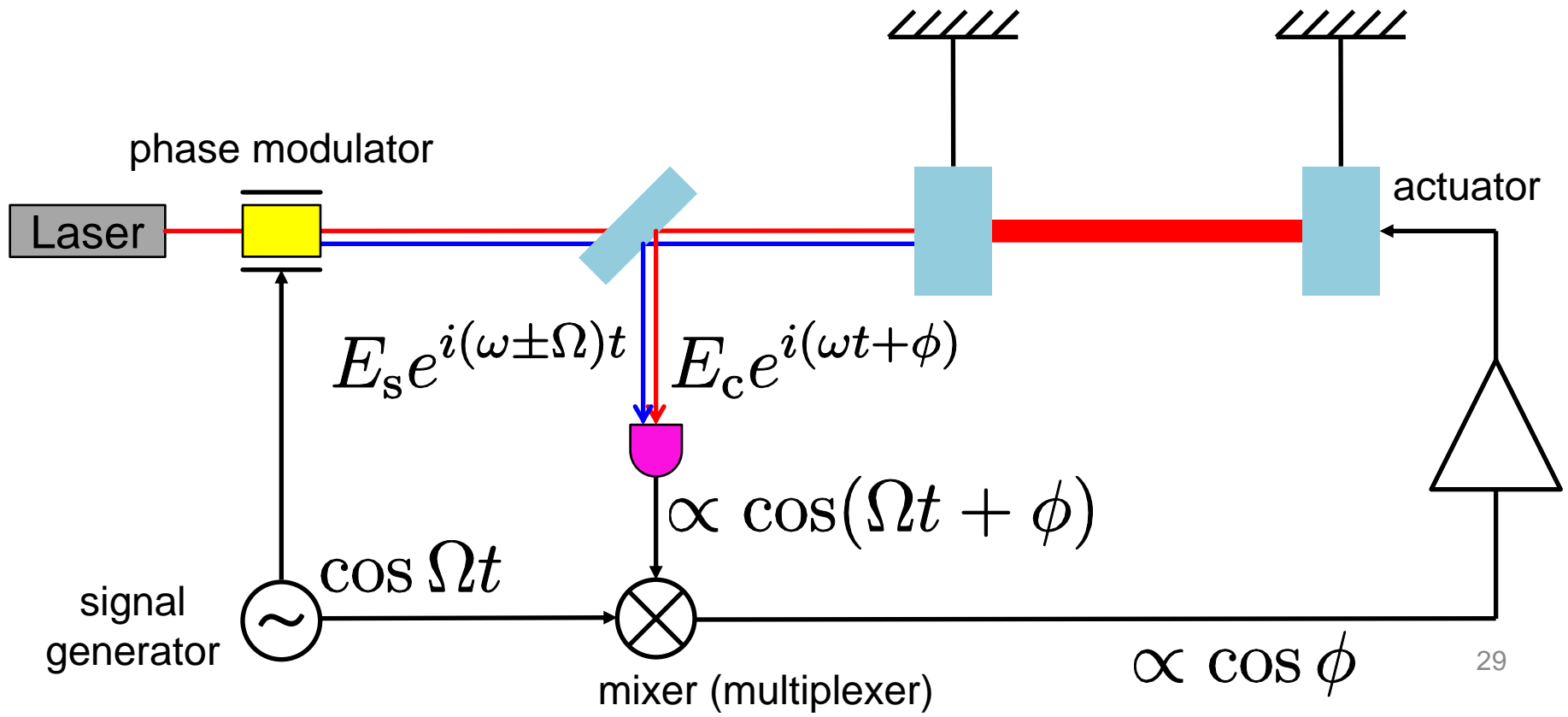
Length sensing of FP cavity

- interference between
 - sidebands (reference)
 - main beam (carries cavity length info.)
- called Pound-Drever-Hall method



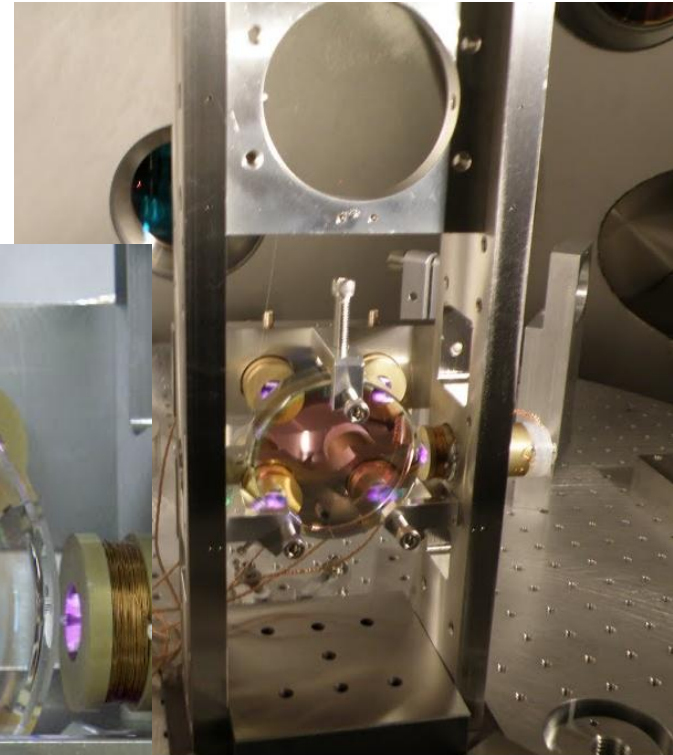
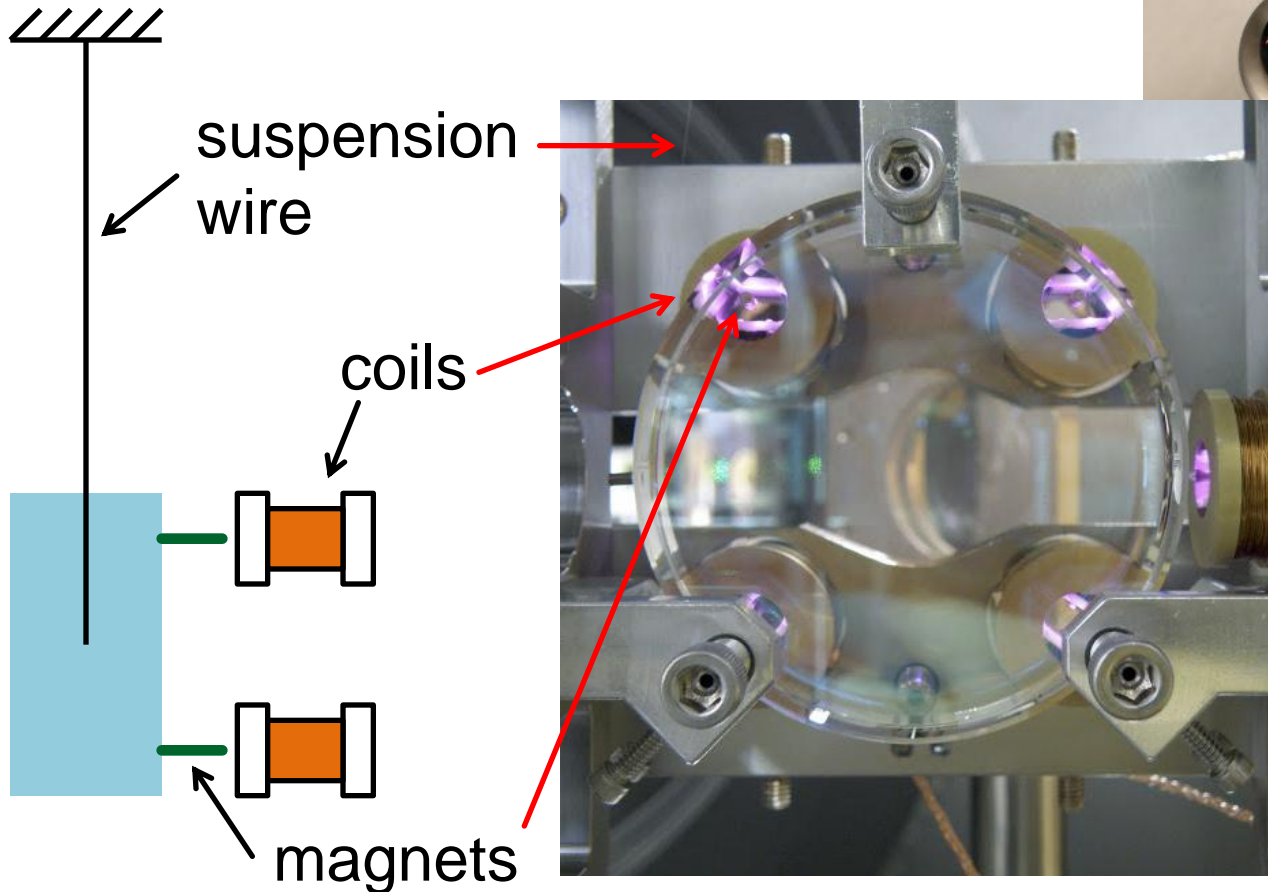
Length control of FP cavity

- demodulate photo detector output
- feedback to actuators attached on mirrors



Coil-magnet actuator

- current in coils \rightarrow creates magnetic field
 \rightarrow magnetic force acts on a mirror

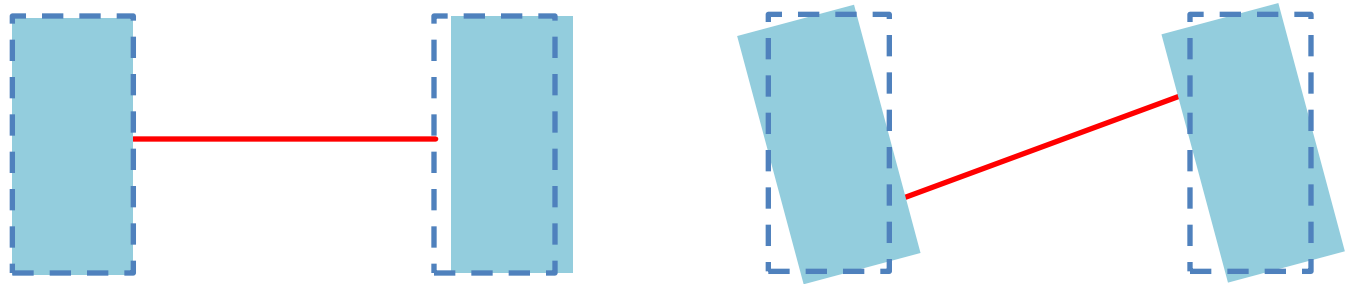


Caltech 40m ETMY

Caltech 40m SRM

Alignment control?

- So far, we have only considered about the length control



- Length control can be understood by plane wave approximation

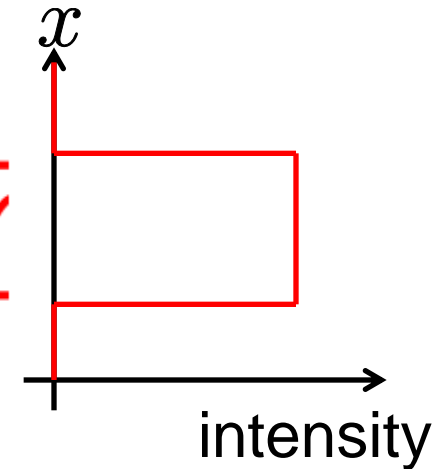
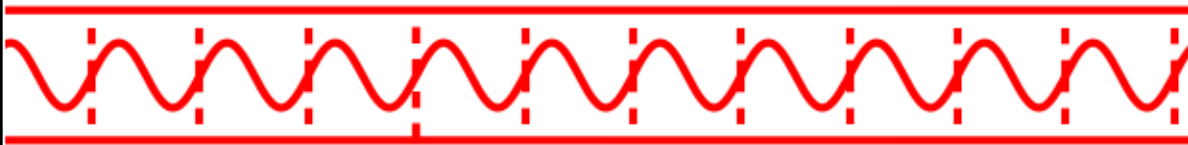
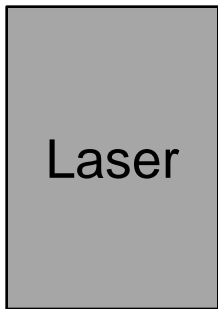
$$E = E_0 e^{i\omega t}$$

- But laser beams are not plane wave, actually
- They are Gaussian beam
- You need to know about Gaussian beam for understanding alignment control

Gaussian beam

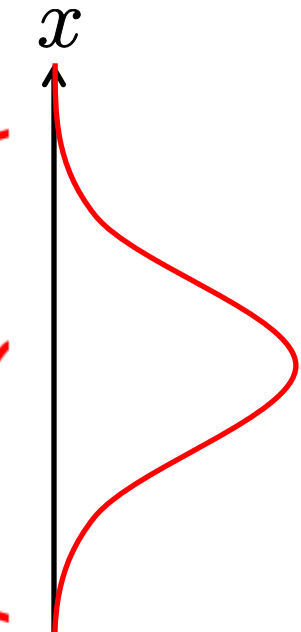
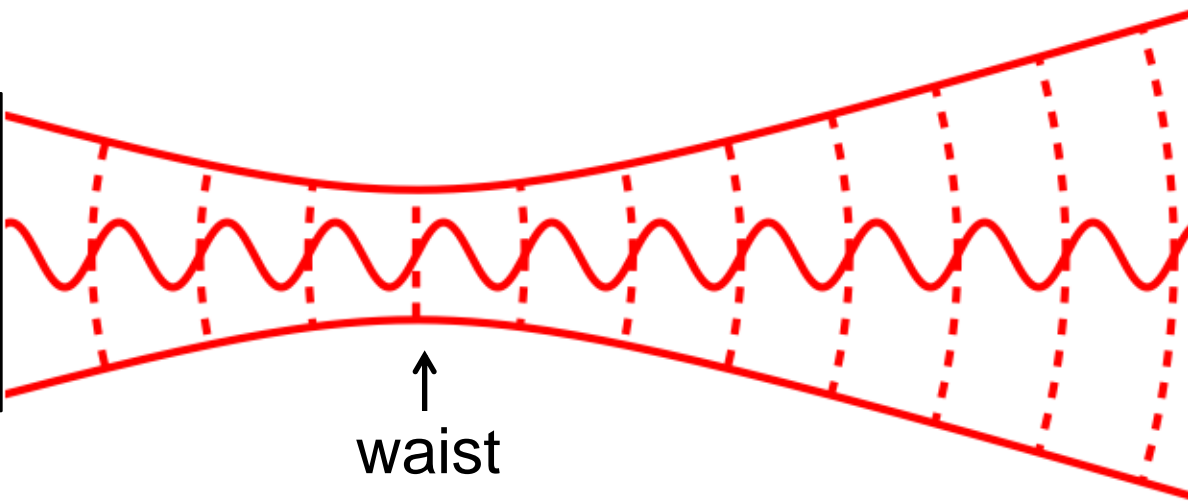
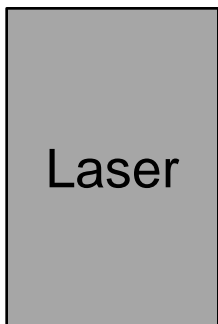
- "ideal" plane wave

$$E = E_0 R(x, y) e^{i(\omega t - kz)}$$



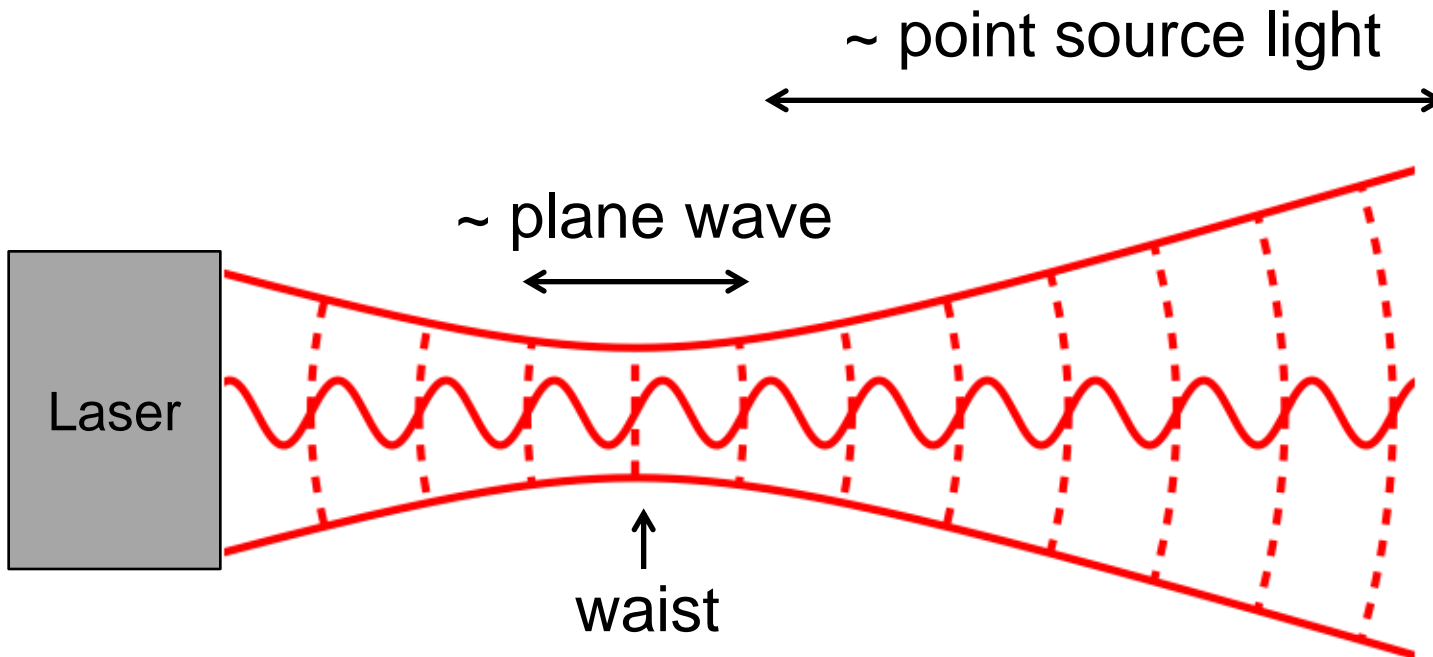
- Gaussian beam

$$E = E_0 U_{00}(x, y, z) e^{i(\omega t - kz + \eta(z))}$$



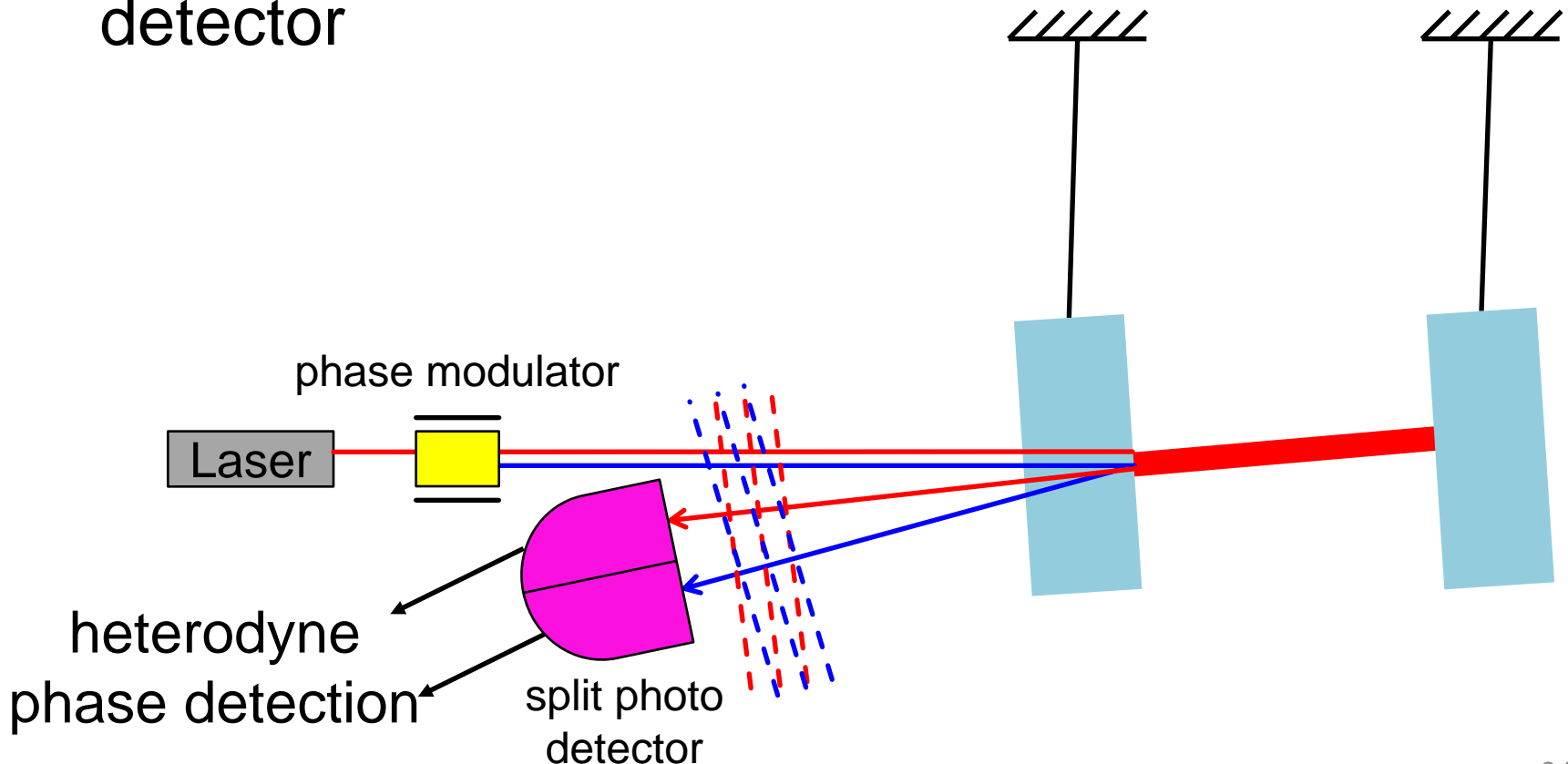
Near field and far field

- Gaussian beam is like
 - plane wave light near the waist
 - point source light far from the waist



Wavefront sensing

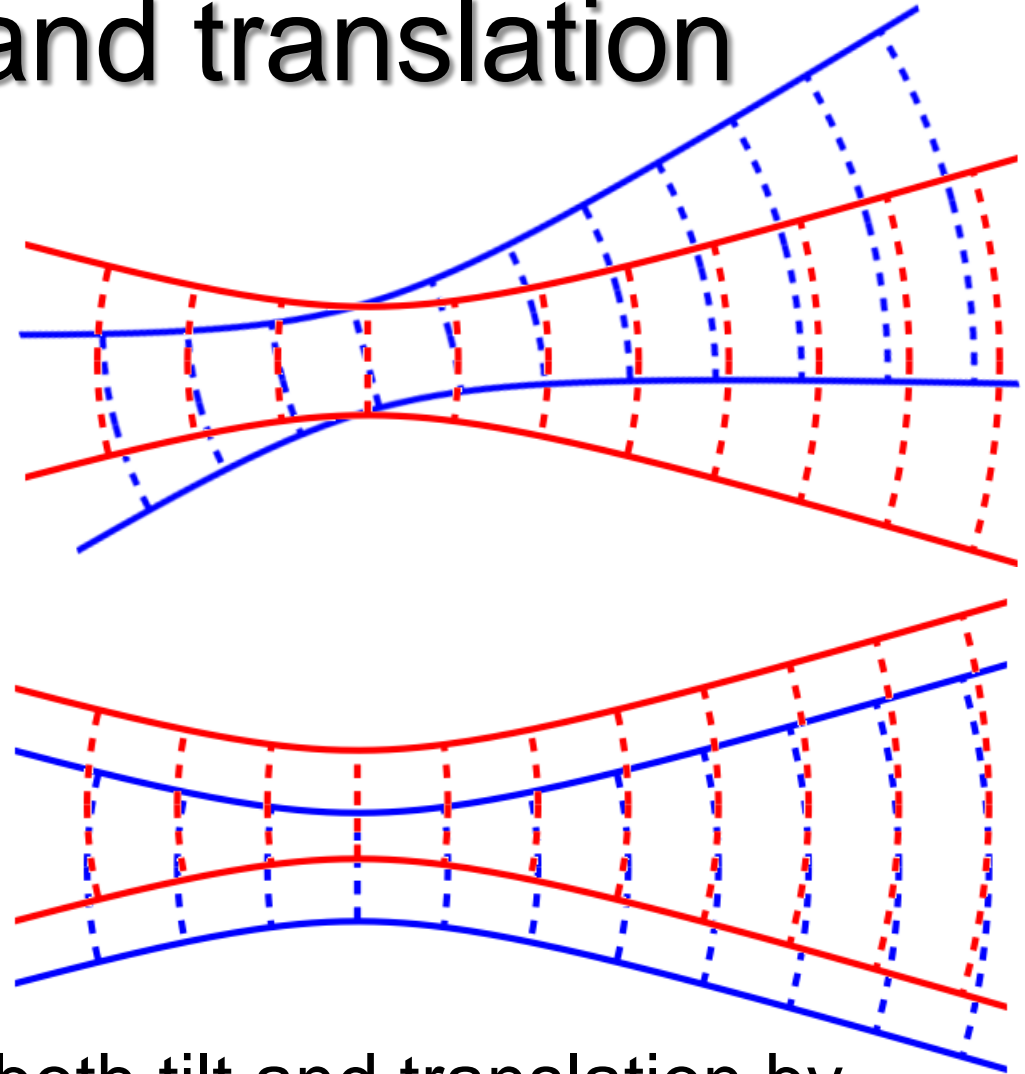
- wavefront of resonating main beam and cavity reflected sidebands are different
- this difference can be detected by split photo detector



Beam tilt and translation

- sensitivity to beam tilt is high at near field

- sensitivity to beam translation is high at far field



- thus, we can sense both tilt and translation by placing split photo detector at different places
→ we can align mirrors

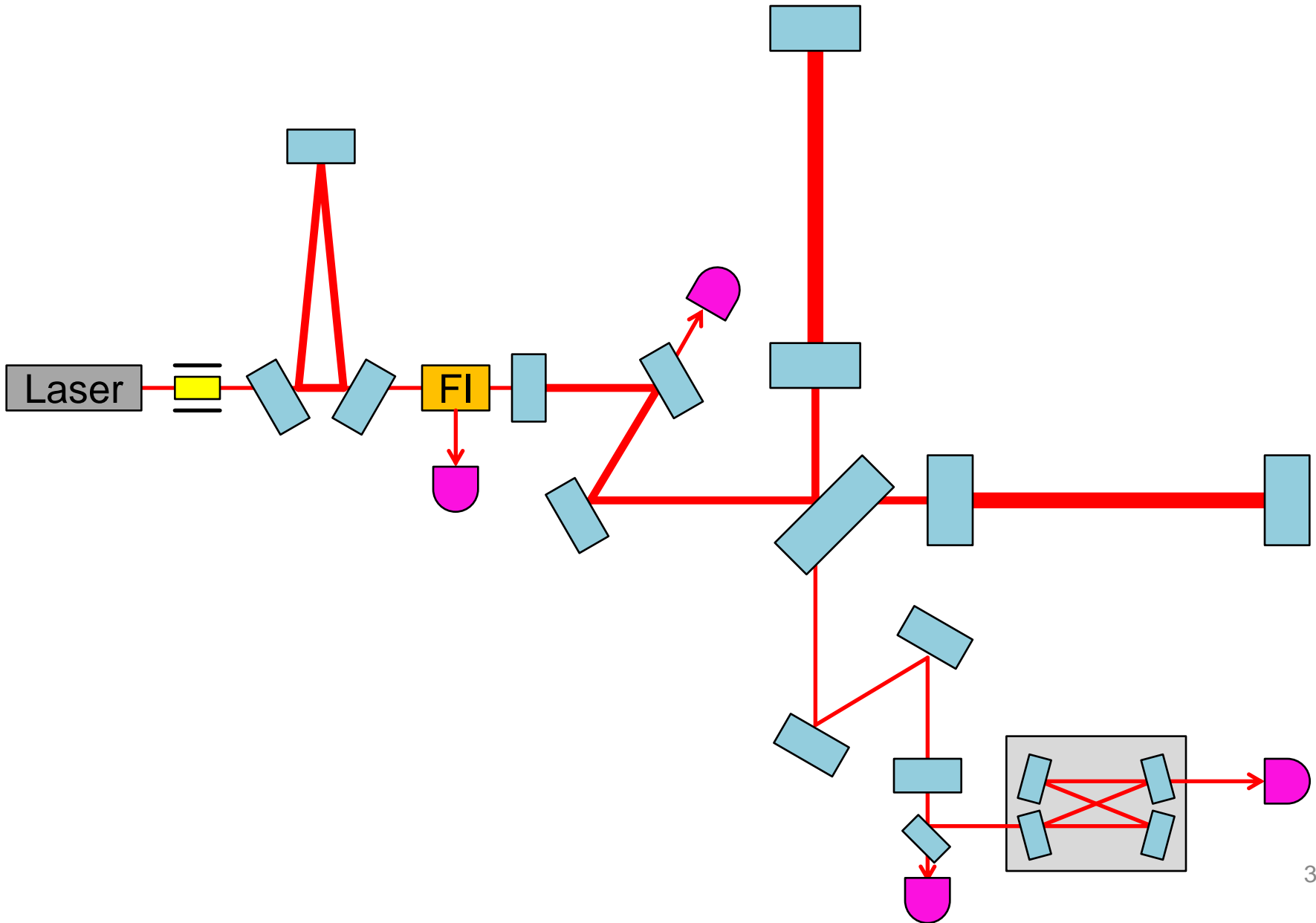
Summary 2/3

- Phase detection is key for GW detectors
- For phase detection, you always need reference beam
- Phase modulation of beam creates sidebands, which work as reference beam
- Interference of main beam and sidebands gives length signal and alignment signal
- For alignment sensing, wavefront sensing technique is used
- Then what's the situation in KAGRA?

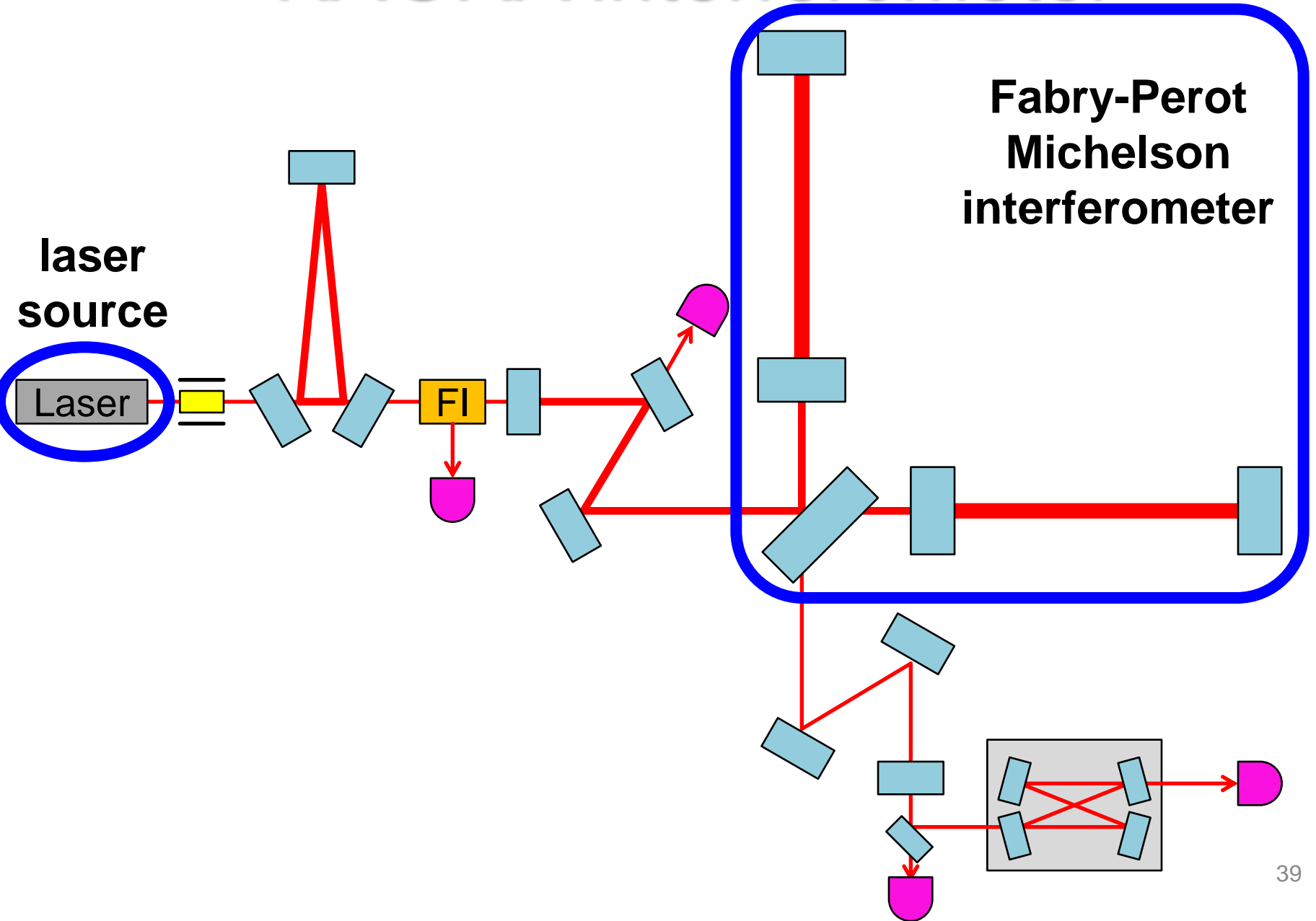
Headache.....

- I will briefly explain
 - further technologies used in KAGRA interferometer (and aLIGO, AdVirgo)
 - what I do for KAGRA

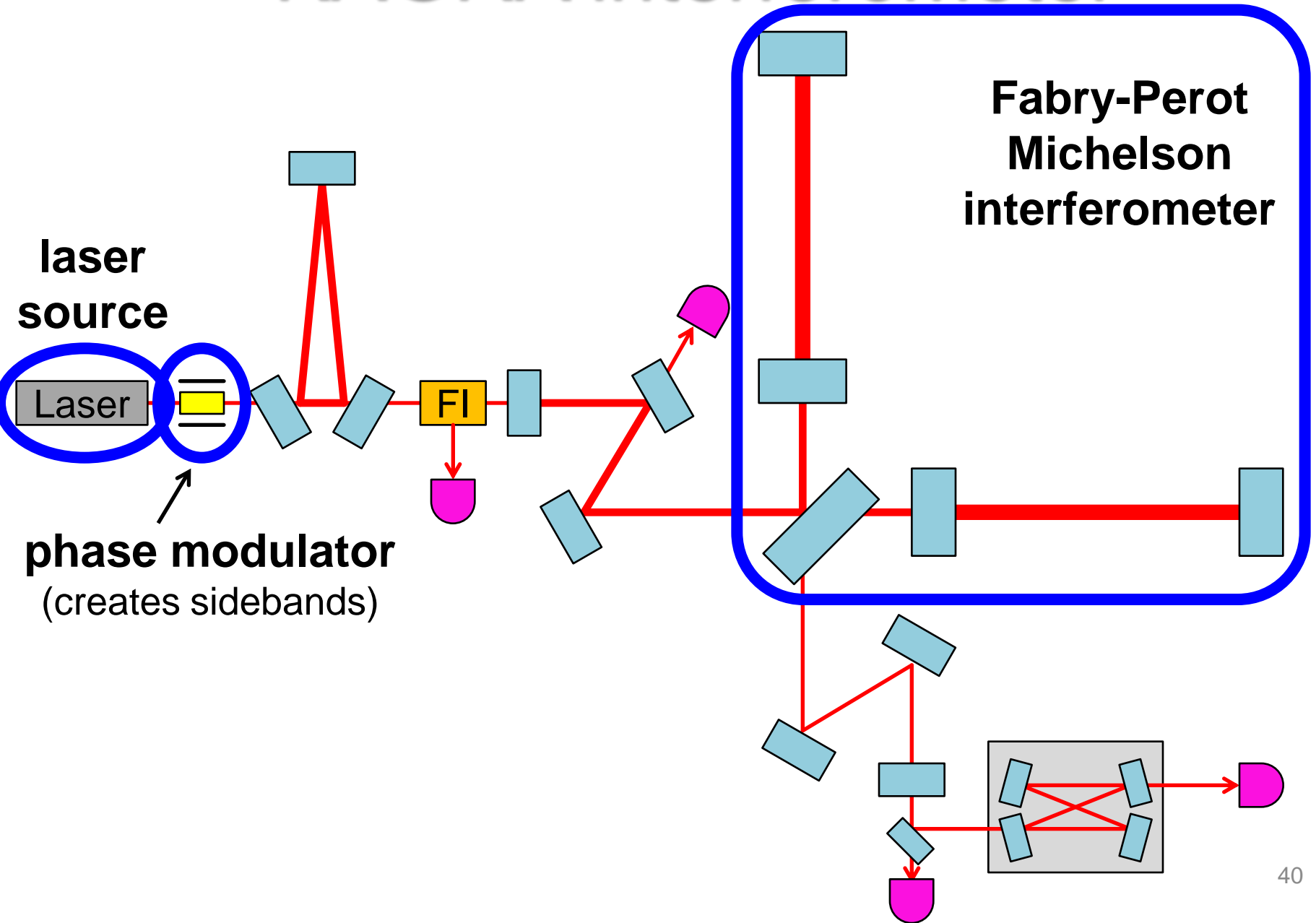
KAGRA interferometer



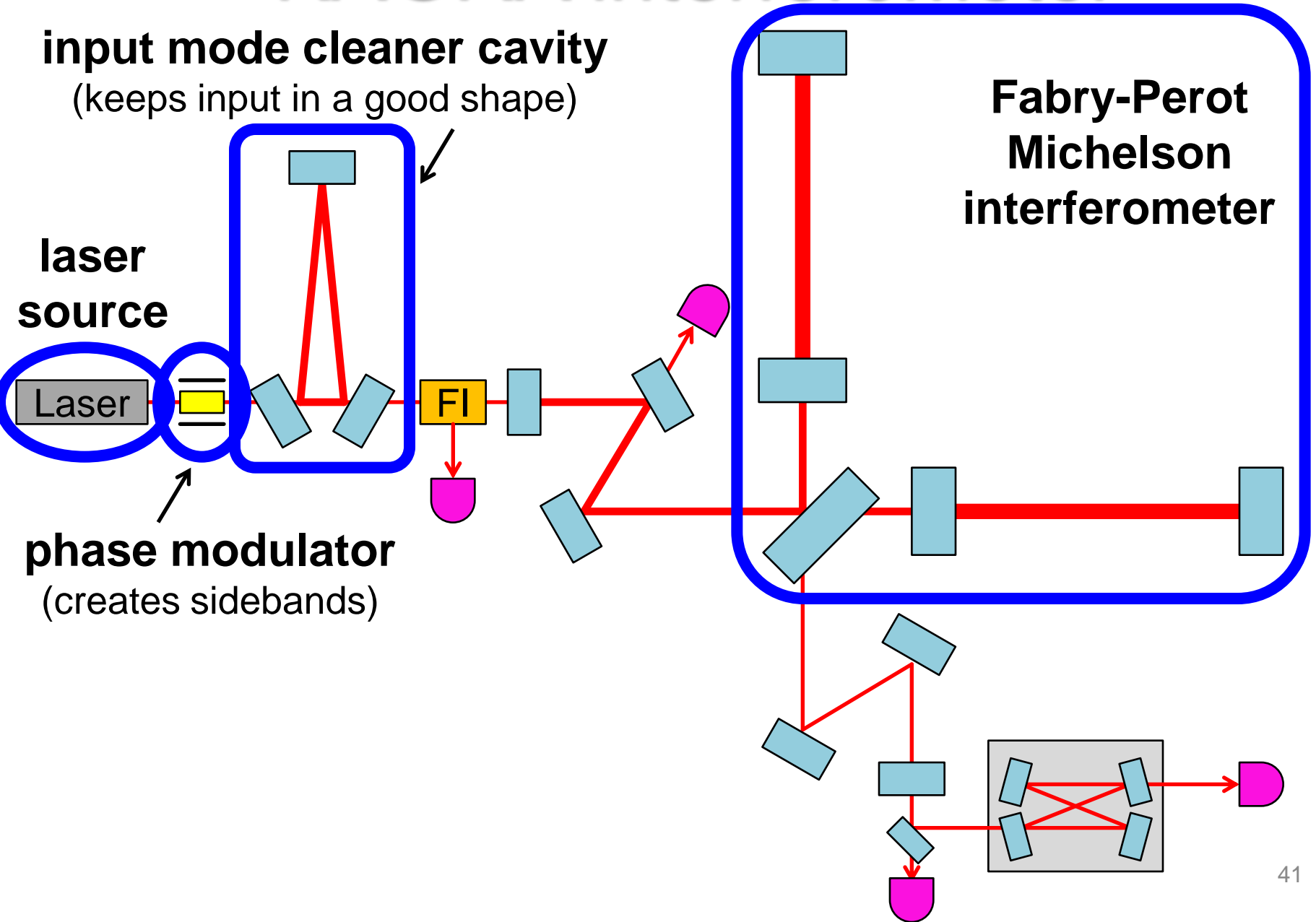
KAGRA interferometer



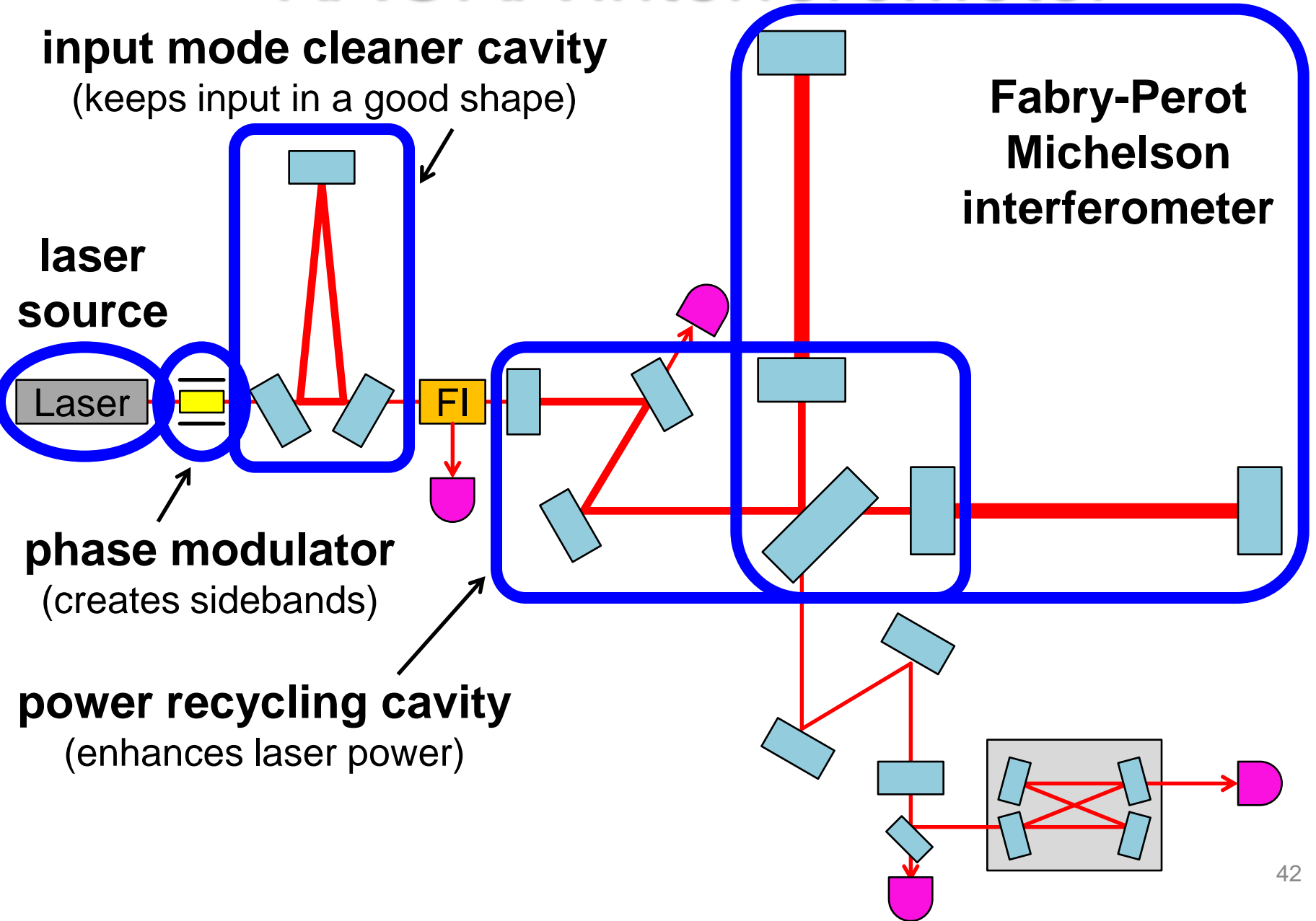
KAGRA interferometer



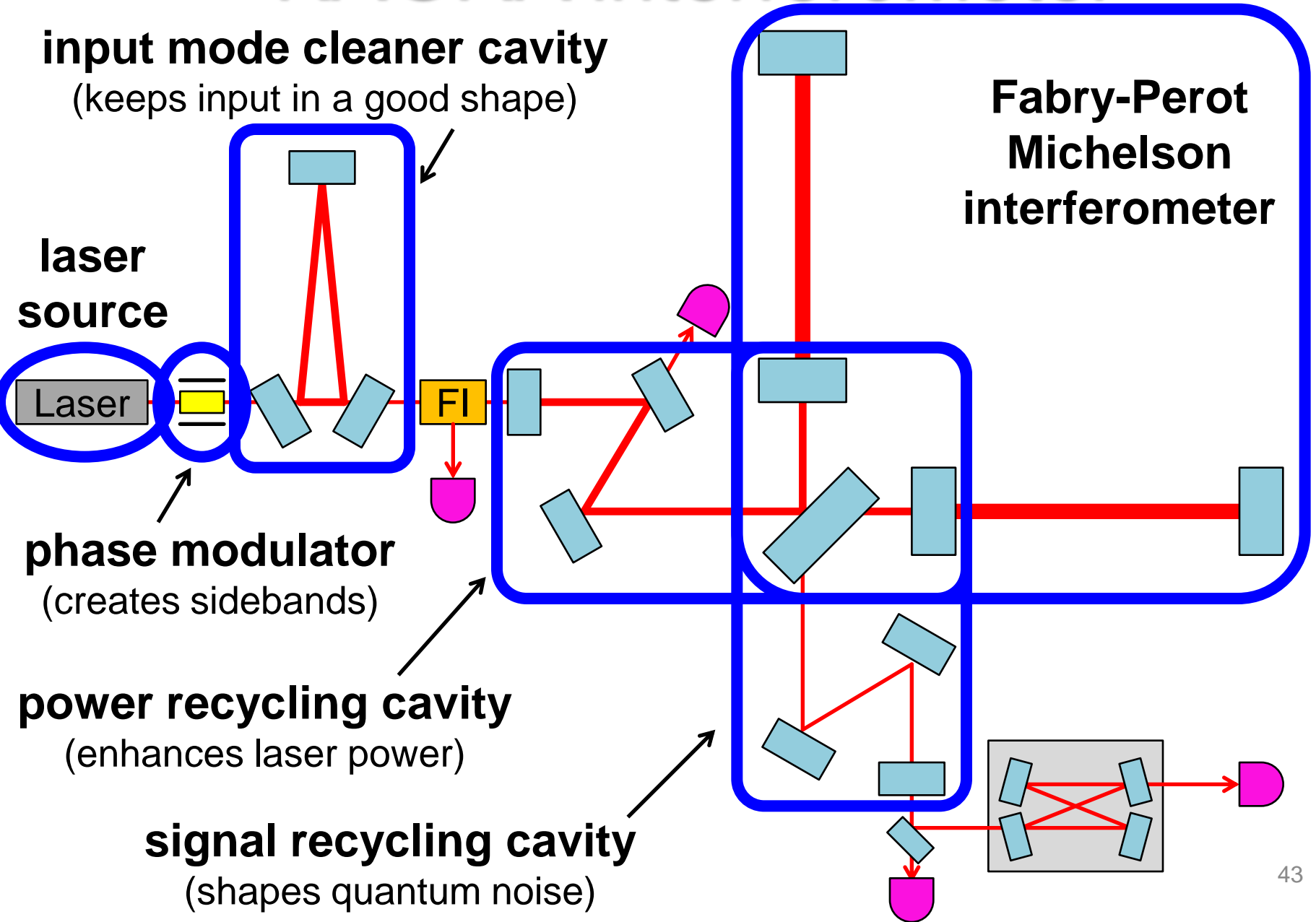
KAGRA interferometer



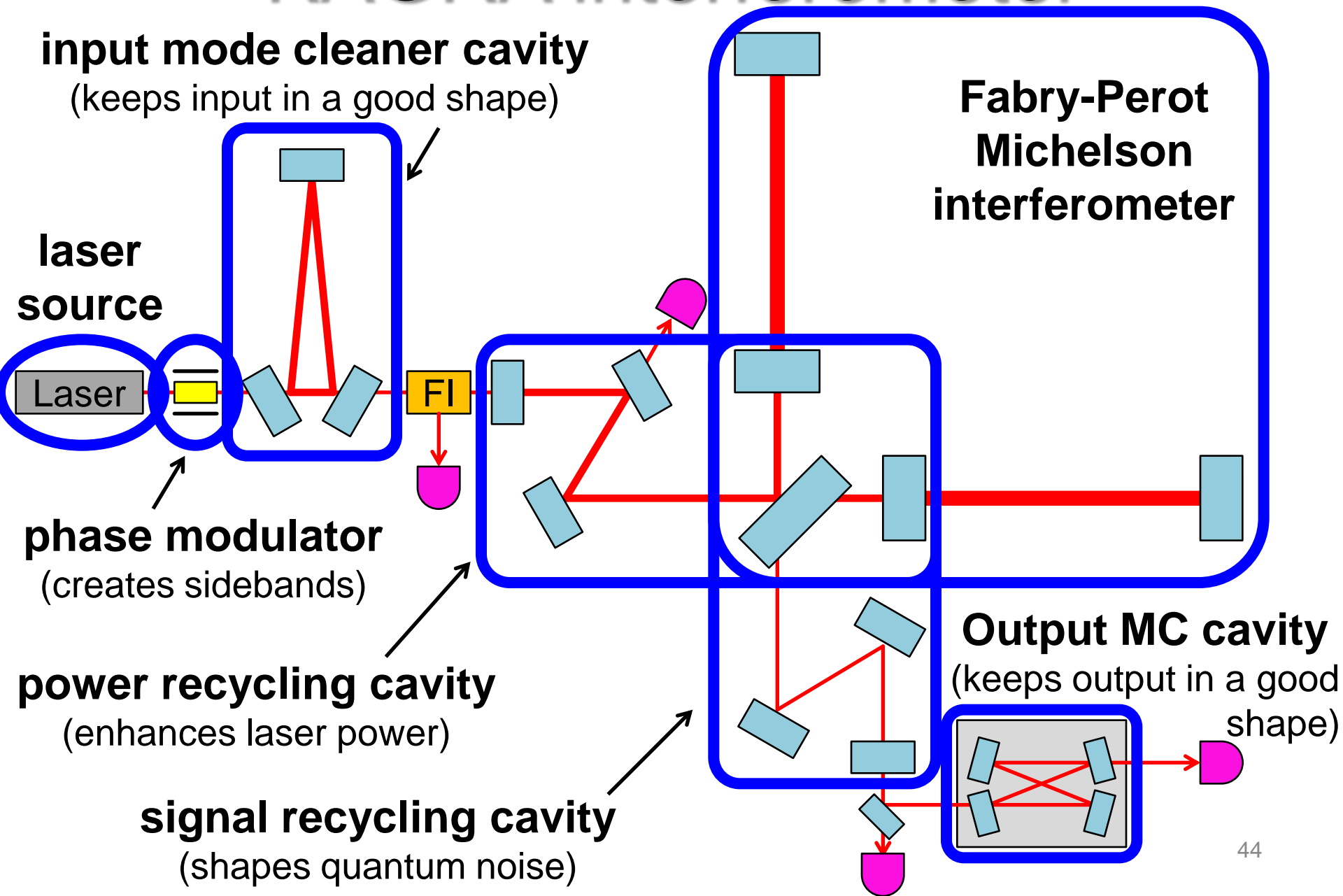
KAGRA interferometer



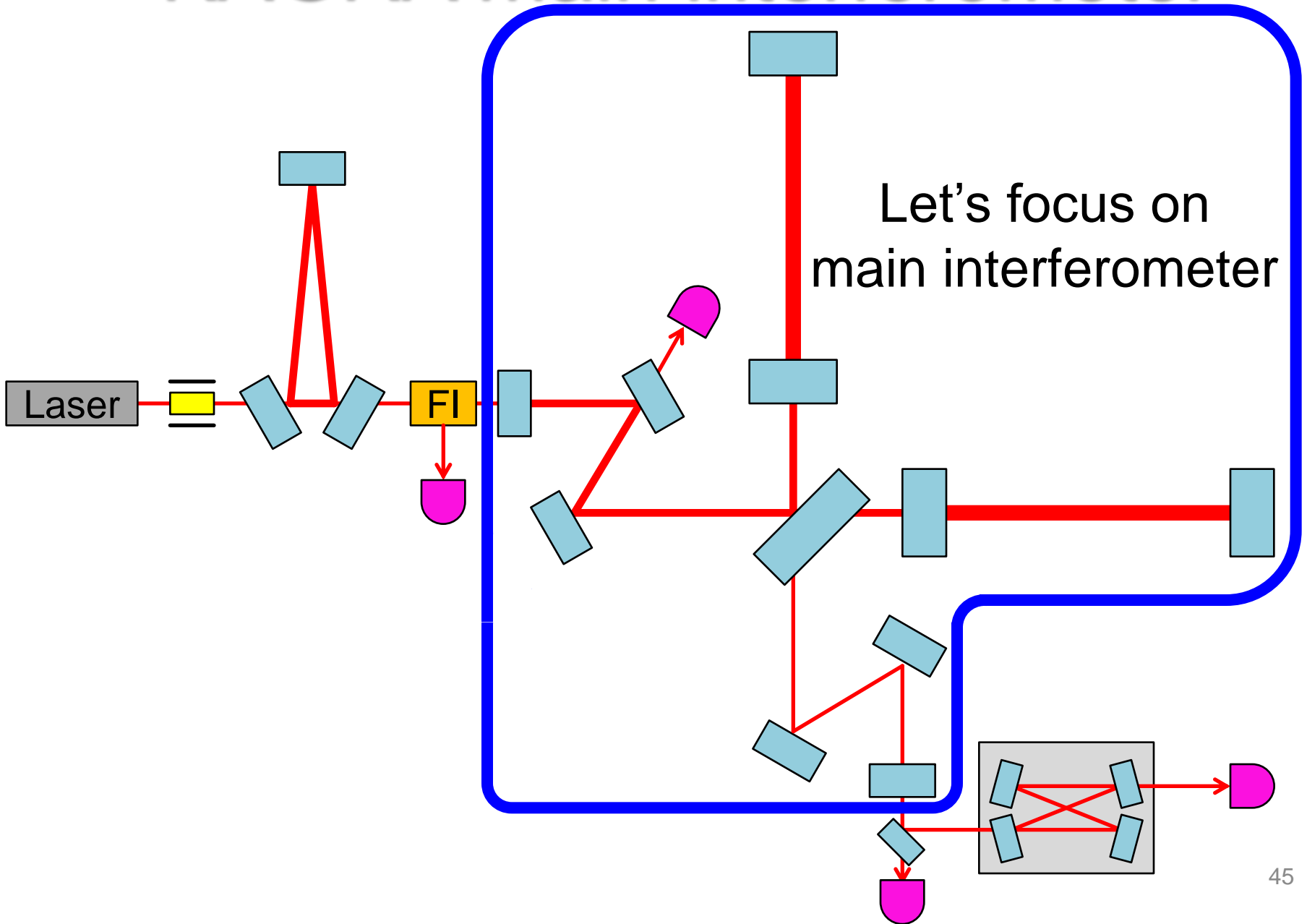
KAGRA interferometer



KAGRA interferometer

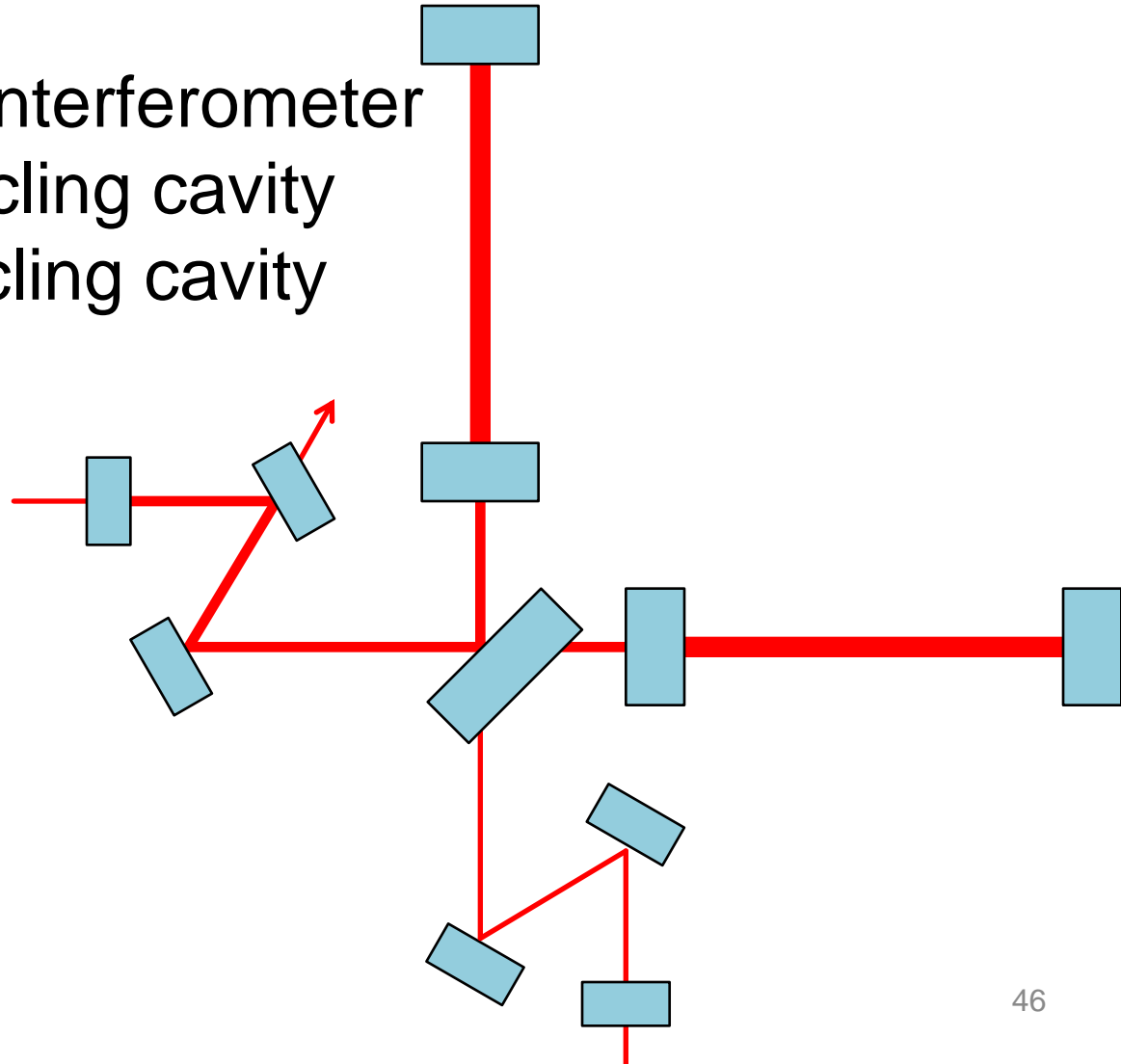


KAGRA main interferometer



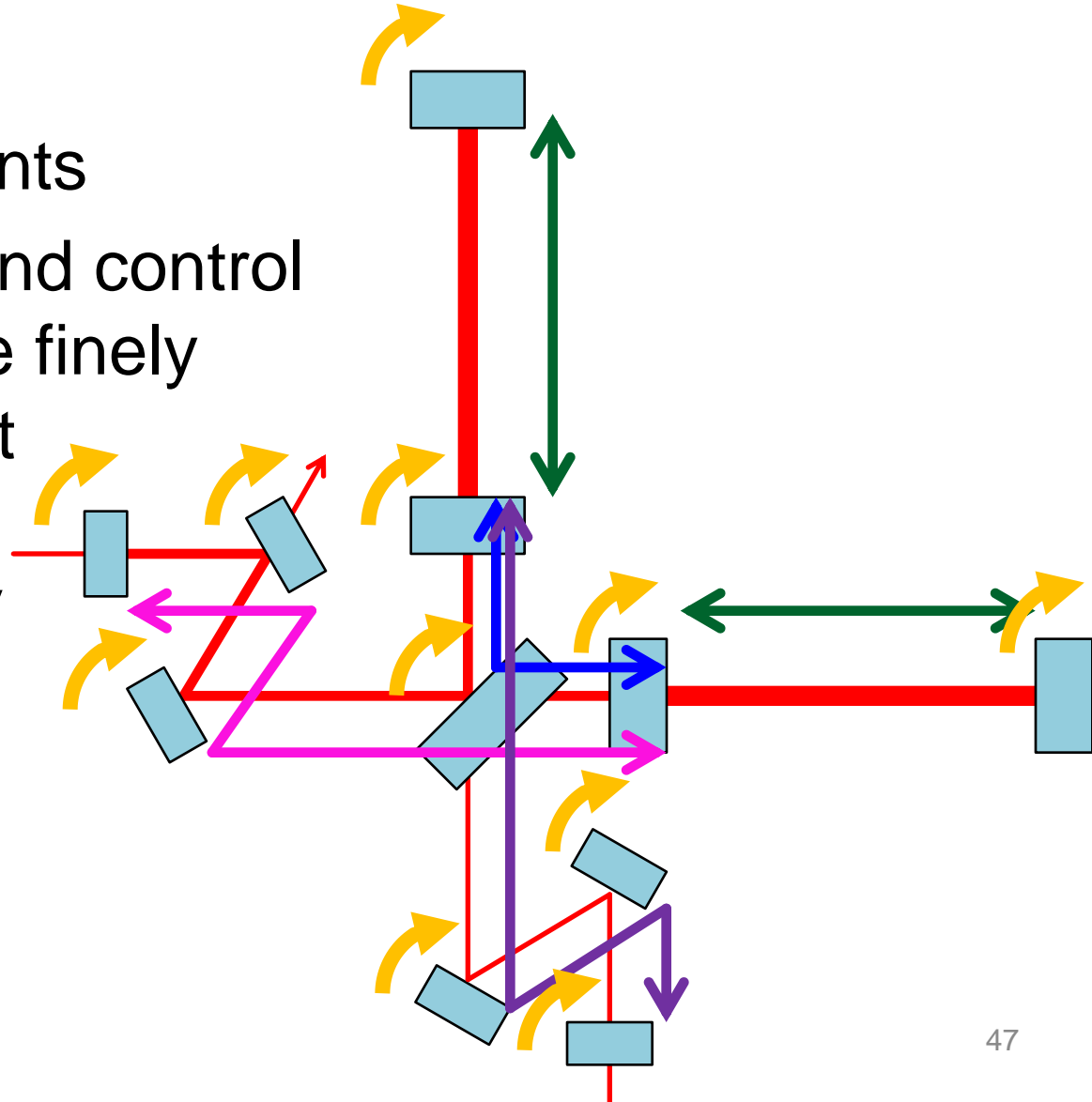
KAGRA main interferometer

- contains
 - 2 FP cavities
 - 1 Michelson interferometer
 - 1 power recycling cavity
 - 1 signal recycling cavity
- in total
 - 11 mirrors
 - 4 FP cavities
 - 1 Michelson



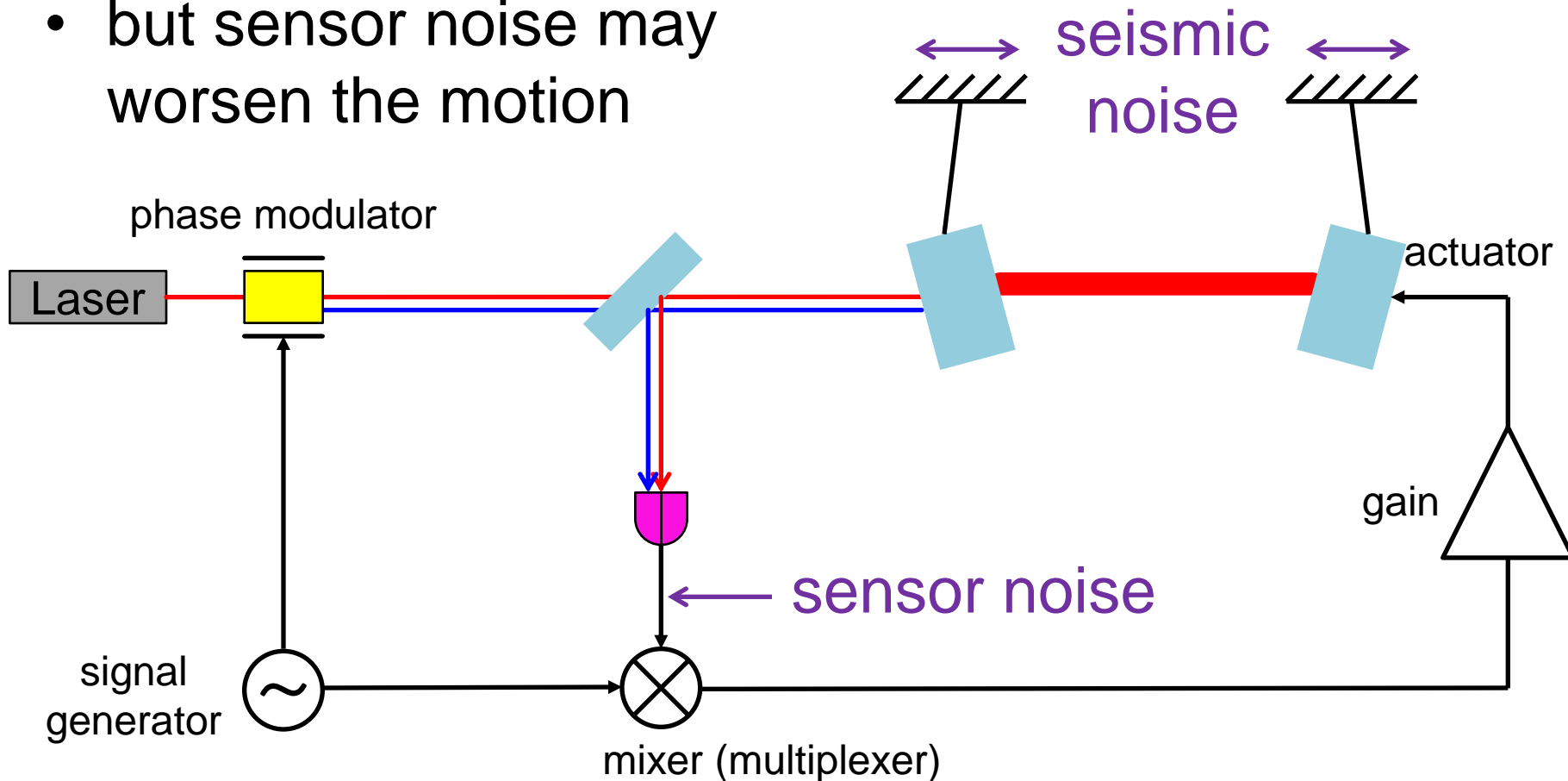
Degrees of freedom to control

- in total
 - 5 lengths
 - 11x2 alignments
- interferometer and control scheme must be finely designed so that KAGRA meets target sensitivity

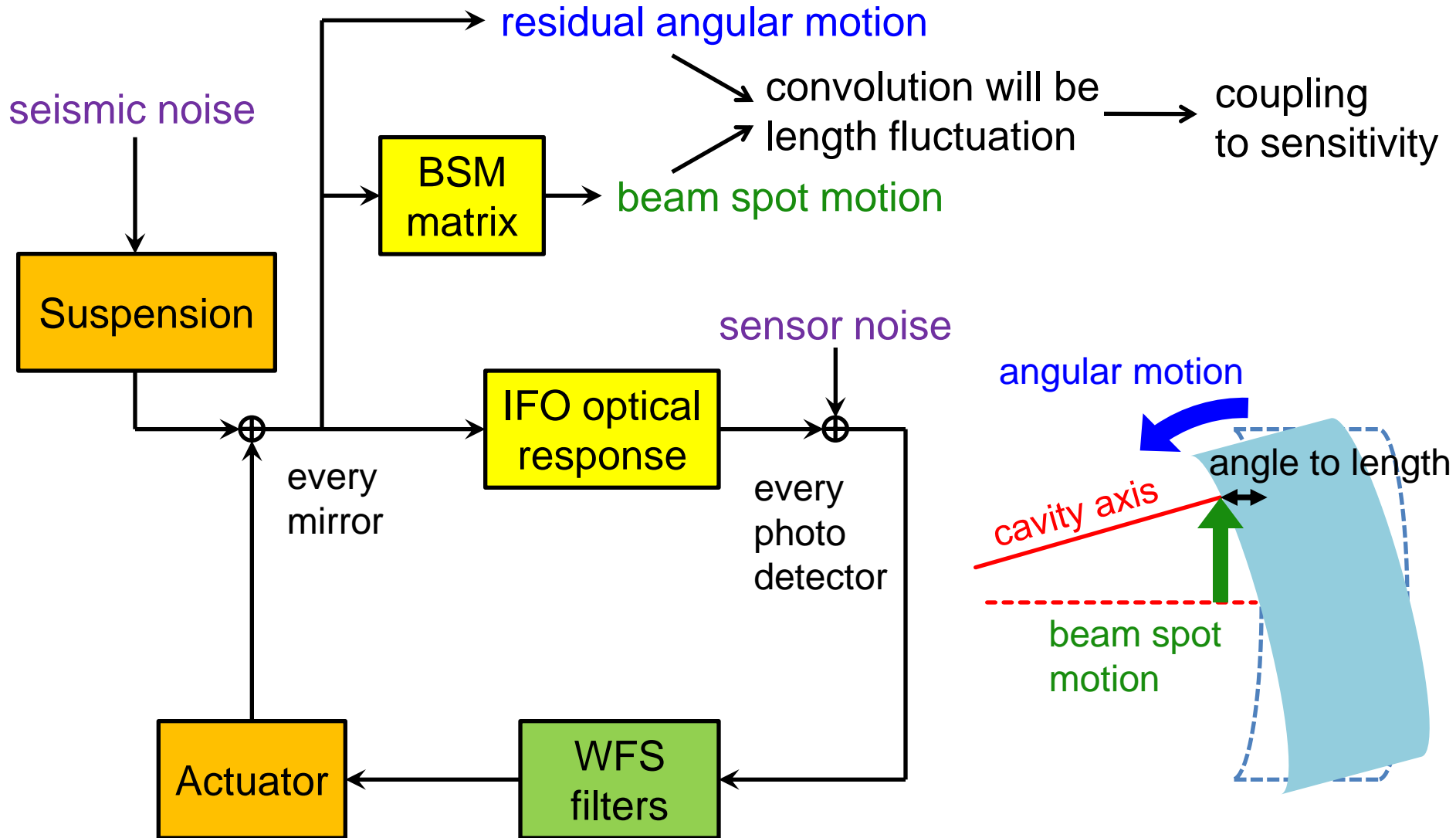


Alignment sensing and control

- mirror angular motion creates noise
- so we want to control them with high gain
- but sensor noise may worsen the motion



Modeling ASC



Angular sensing matrix

- angular mirror motions are sensed at different photo detectors

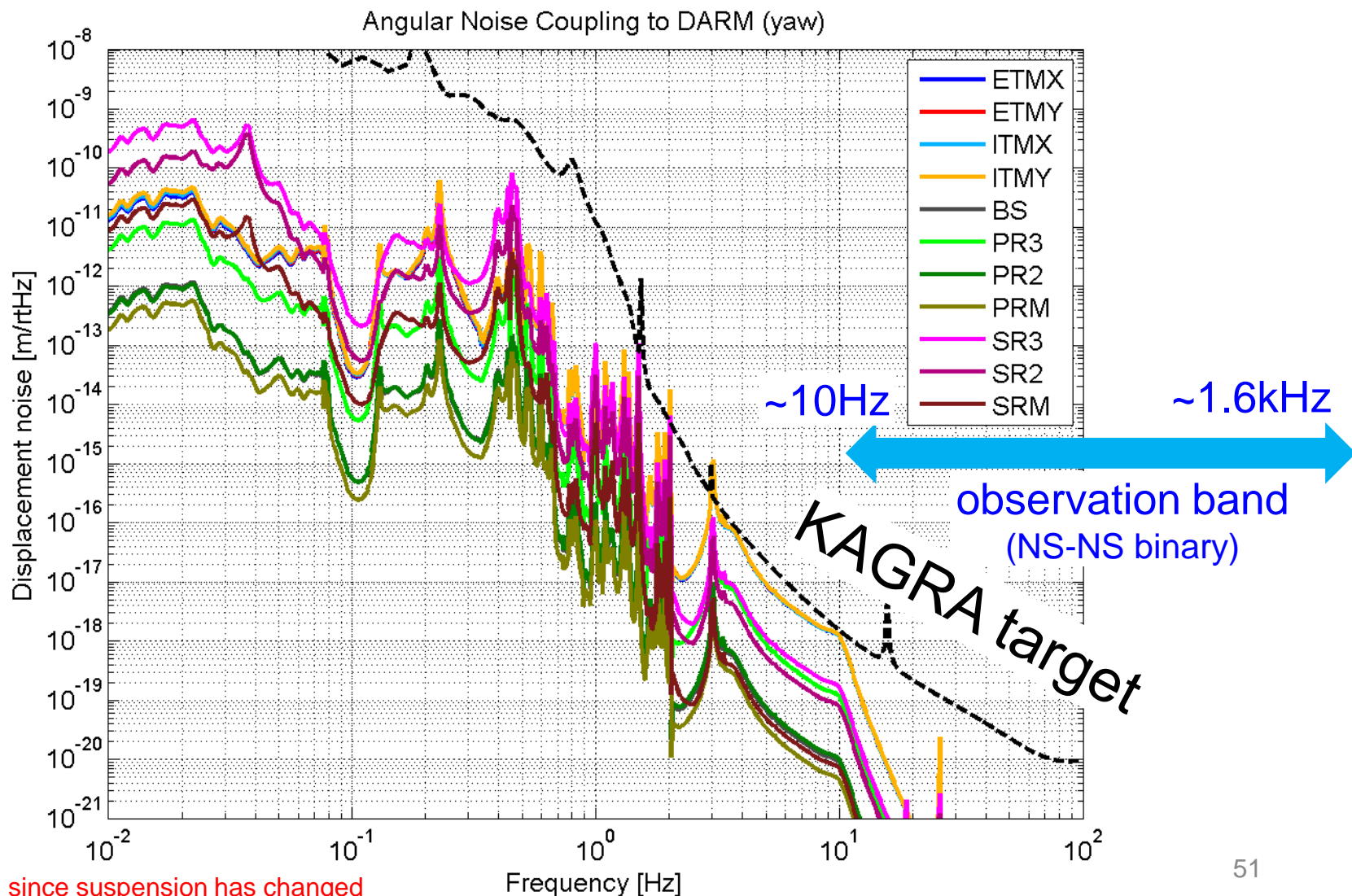
WFS Sensing Matrix [W/mrad]

(Gouy phases at POP A:-8.0, POP B:-76.4 REFL A:88.3, REFL B:-88.4, AS A:6.7, AS B:-83.7, TR A:-61.4 deg)

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
POP_ADC	-3.50	-16.76	-0.06	0.09	-0.49	-1.30	-0.40	-0.19	-0.11	-0.01	-0.01
POP_BDC	0.17	-0.02	0.00	0.00	-0.12	-0.30	-2.09	-1.02	0.01	0.00	0.00
POP_A1I	0.91	-0.44	0.00	-0.00	-0.23	-1.18	-0.14	-0.07	-0.51	-0.06	-0.03
POP_A1Q	0.02	-0.01	0.36	-0.36	0.26	-0.02	-0.00	-0.00	-0.01	-0.00	-0.00
POP_B1I	1.95	-0.69	0.00	-0.00	-0.46	-2.43	-0.30	-0.15	-1.09	-0.13	-0.07
POP_B1Q	-0.00	0.00	0.05	-0.05	0.04	0.00	0.00	0.00	0.00	0.00	0.00
POP_A2I	0.06	-0.02	0.00	-0.00	-0.03	-0.10	-0.01	-0.01	-0.00	-0.00	-0.00
POP_A2Q	-1.55	0.73	-0.00	0.00	1.00	2.86	0.35	0.17	-0.00	-0.00	-0.00
POP_B2I	-0.01	0.01	0.00	-0.00	0.01	0.02	0.00	0.00	0.00	0.00	0.00
POP_B2Q	-3.36	1.19	-0.01	0.01	2.10	6.06	0.74	0.37	-0.00	-0.00	-0.00
REFL_ADC	5.69	-7.59	-0.01	-0.00	-4.07	-12.20	-1.48	-4.96	-0.43	-0.05	-0.03
REFL_BDC	-3.42	0.31	-0.01	0.02	1.80	5.54	0.68	4.65	0.22	0.03	0.01
REFL_A1I	14.19	21.33	0.10	-0.14	-1.84	-9.94	-1.29	-1.05	-4.32	-0.51	-0.27
REFL_A1Q	-0.00	0.03	0.19	-0.19	0.14	0.01	0.00	0.00	0.01	0.00	0.00
REFL_B1I	-14.24	-21.26	-0.10	0.14	1.86	10.04	1.30	0.97	4.34	0.52	0.27
REFL_B1Q	-0.00	-0.03	-0.28	0.28	-0.20	-0.01	-0.00	0.00	-0.00	-0.00	-0.00
REFL_A2I	-52.89	-143.42	-0.56	0.83	8.28	25.80	3.60	4.37	-0.00	-0.00	-0.00
REFL_A2Q	-0.07	0.01	0.00	-0.00	-0.04	-0.10	-0.01	-0.01	0.00	0.00	0.00
REFL_B2I	53.05	143.18	0.56	-0.82	-8.41	-26.16	-3.65	-3.85	0.00	0.00	0.00
REFL_B2Q	-0.05	-0.01	-0.00	0.00	0.03	0.08	0.01	0.01	-0.00	-0.00	-0.00
AS_ADC	1.08	-1.08	1.35	5.04	-0.27	-1.53	-0.19	-0.09	-0.72	-0.08	-0.03
AS_BDC	-0.00	0.00	-0.09	-0.03	-0.06	-0.01	-0.00	-0.00	0.01	0.00	-0.04
AS_A1I	-0.00	0.00	-0.00	-0.02	0.00	-0.00	-0.00	-0.00	0.00	0.00	0.00
AS_A1Q	0.21	-0.20	6.78	25.40	0.11	-0.16	-0.02	-0.01	-0.28	-0.03	-0.01
AS_B1I	0.00	-0.00	-0.05	0.05	-0.03	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00
AS_B1Q	-0.00	-0.01	-0.46	-0.15	-0.25	-0.00	-0.00	-0.00	0.01	0.00	-0.01
TRX_ADC	-9.23	0.40	-9.23	0.38	0.00	-0.01	-0.00	-0.00	0.00	0.00	0.00
TRX_BDC	0.22	17.87	0.20	17.81	-0.00	-0.02	-0.00	-0.00	0.00	0.00	0.00
TRY_ADC	-9.23	0.40	9.23	-0.38	-0.01	-0.01	-0.00	-0.00	-0.00	-0.00	-0.00
TRY_BDC	0.22	17.87	-0.20	-17.81	-0.01	-0.02	-0.00	-0.00	-0.00	-0.00	-0.00

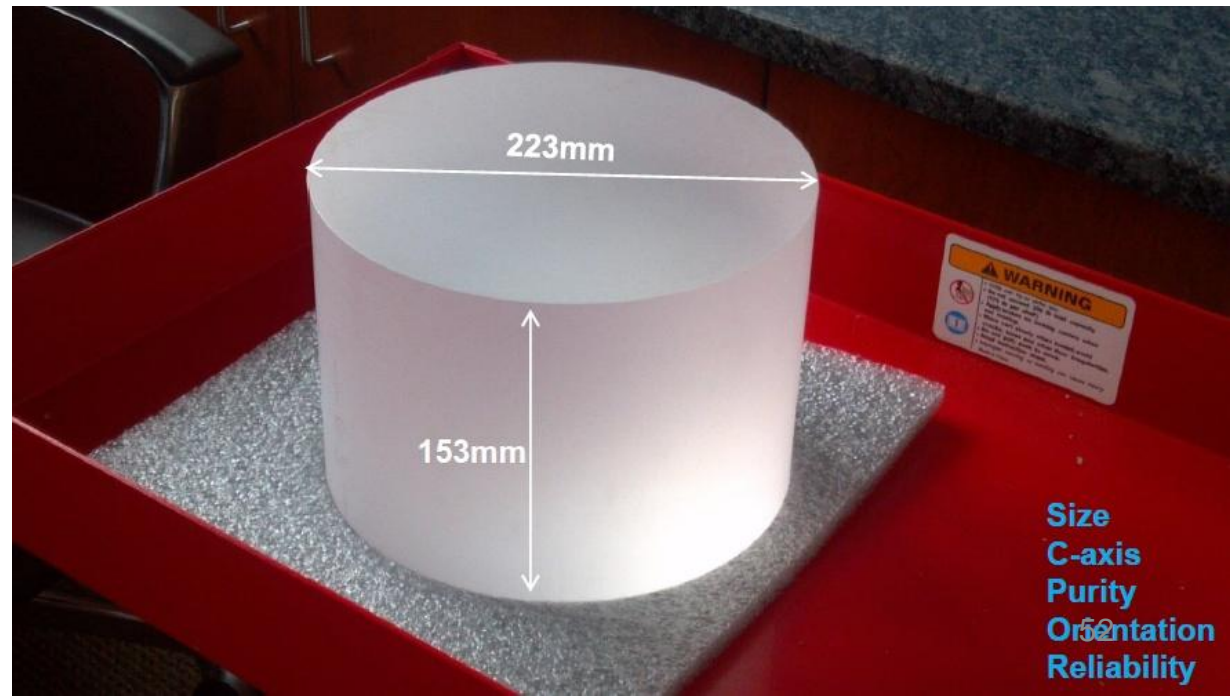
ASC noise coupling to sensitivity

- close, but meets requirement



Current status

- finalized KAGRA interferometer design
- confirmed they are reasonable from ASC and many other considerations
- mirrors being fabricated
- ASC barely meets requirement, detailed simulation on-going



Summary 3/3

- There are many degrees of freedom to control KAGRA interferometer
- Modeling interferometer control scheme is essential for designing interferometer
- I developed a model for simulating alignment sensing and control scheme for KAGRA
- We finalized KAGRA interferometer design
- More detailed, practical designing on going

Thank you
감사합니다
ありがとう

