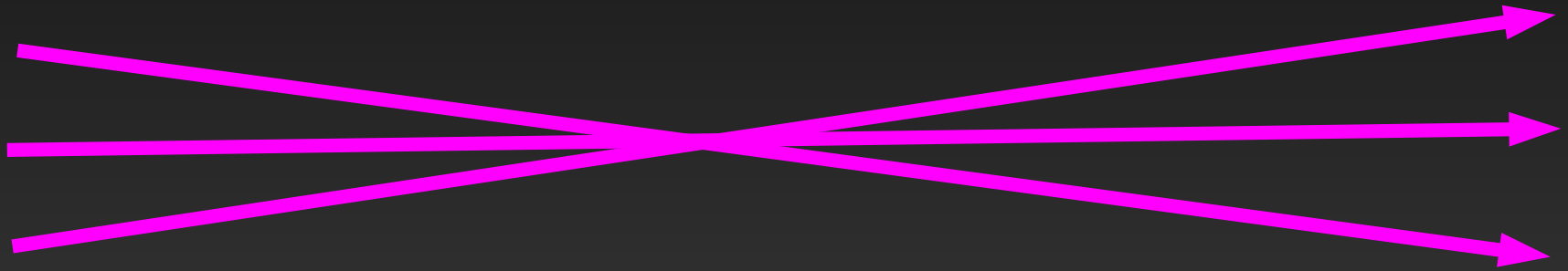


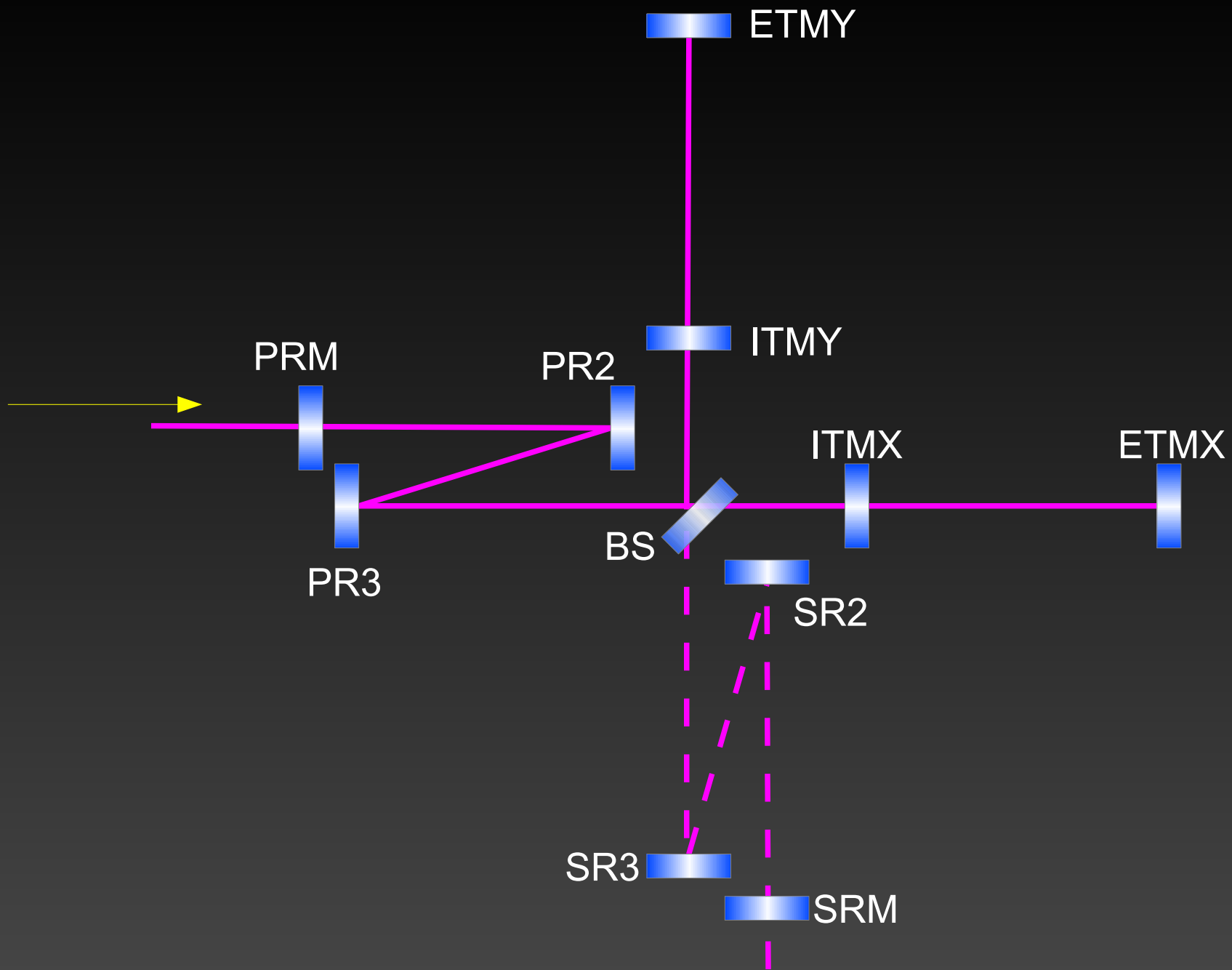
重力波検出器KAGRAの主干涉計開発

東大理 麻生洋一 他



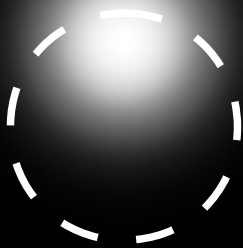
入射ビームは揺れている!!

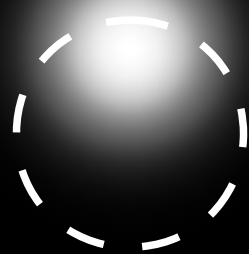




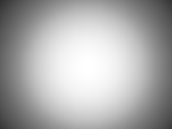
計算方法

Guido Mueller, *Optics Express*, **18**, 7118 (2005)





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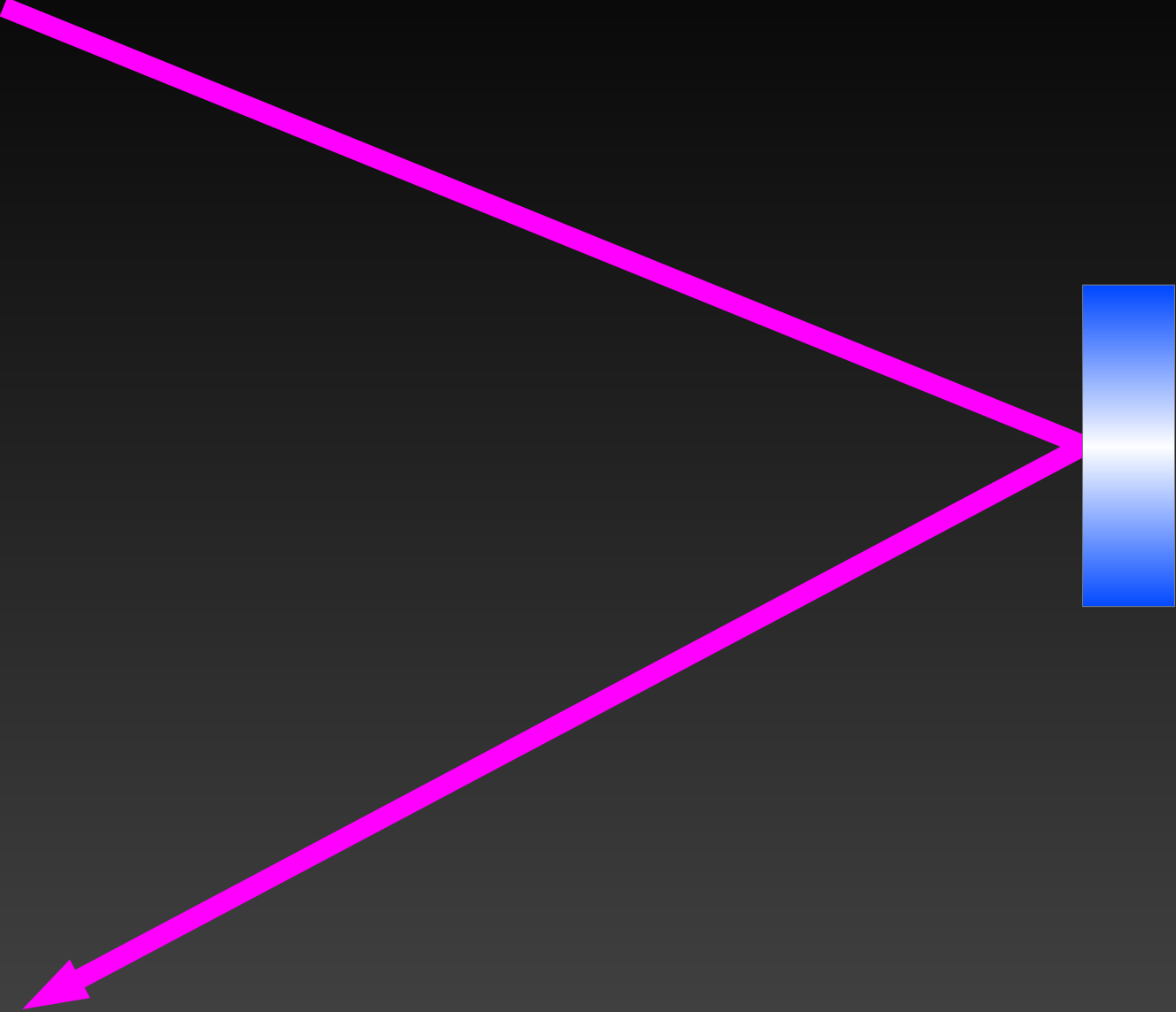


+

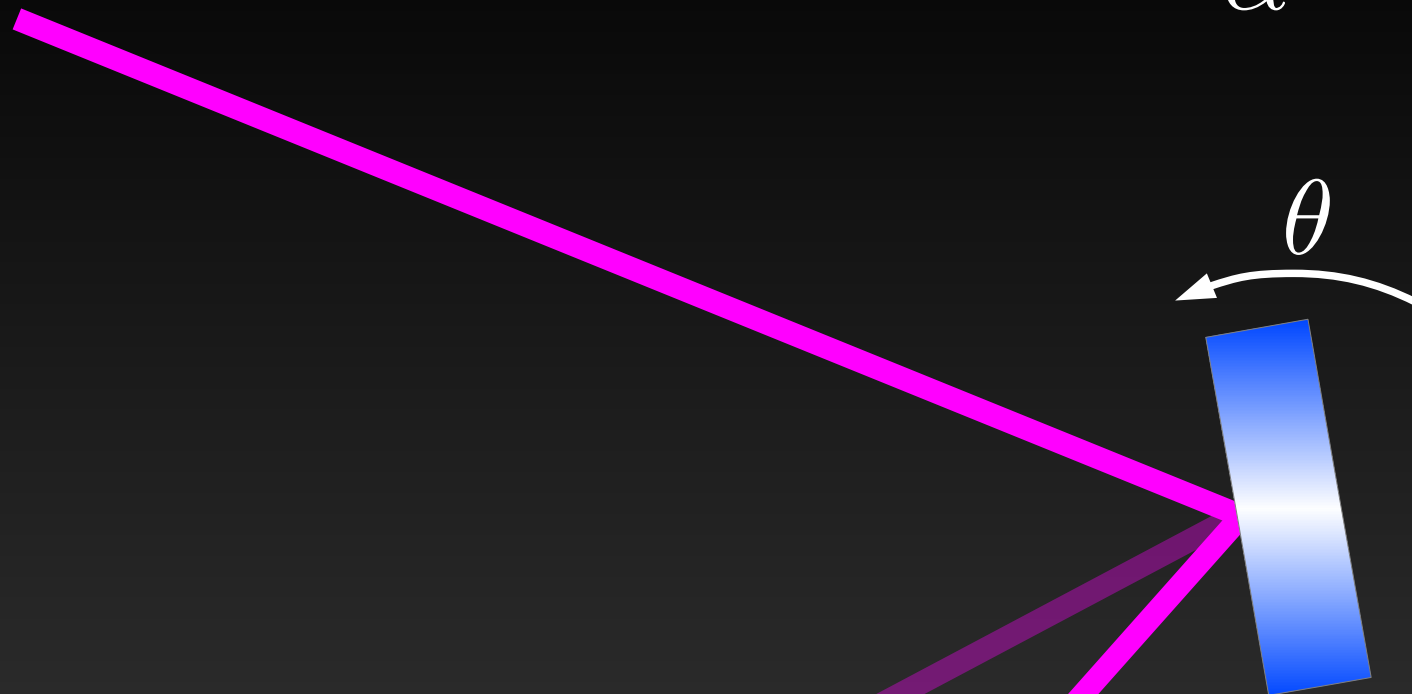


TEM00

TEM01



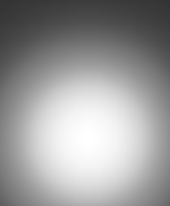
$$\alpha = \frac{\pi w}{\lambda} \theta$$



$$E_0^{00}$$

$$\sqrt{1 - 4\alpha^2} E_0^{00} + 2i\alpha E_0^{01}$$

$$E_0^{nm} = A_0 \cdot \gamma_{nm}(x, y) \cdot e^{i\Omega t + i\phi}$$

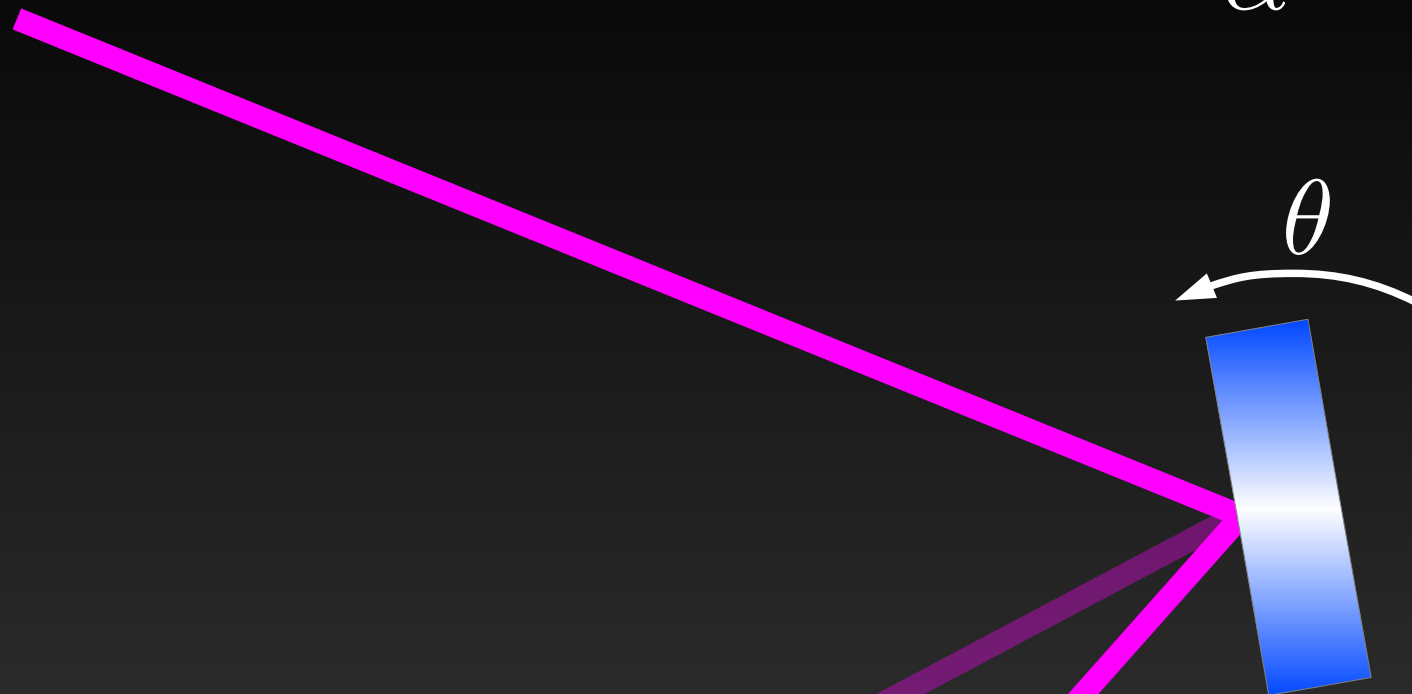


$\gamma_{00}(x, y)$



$\gamma_{01}(x, y)$

$$\alpha = \frac{\pi w}{\lambda} \theta$$



$$E_0^{00}$$

$$\sqrt{1 - 4\alpha^2} E_0^{00} + 2i\alpha E_0^{01}$$

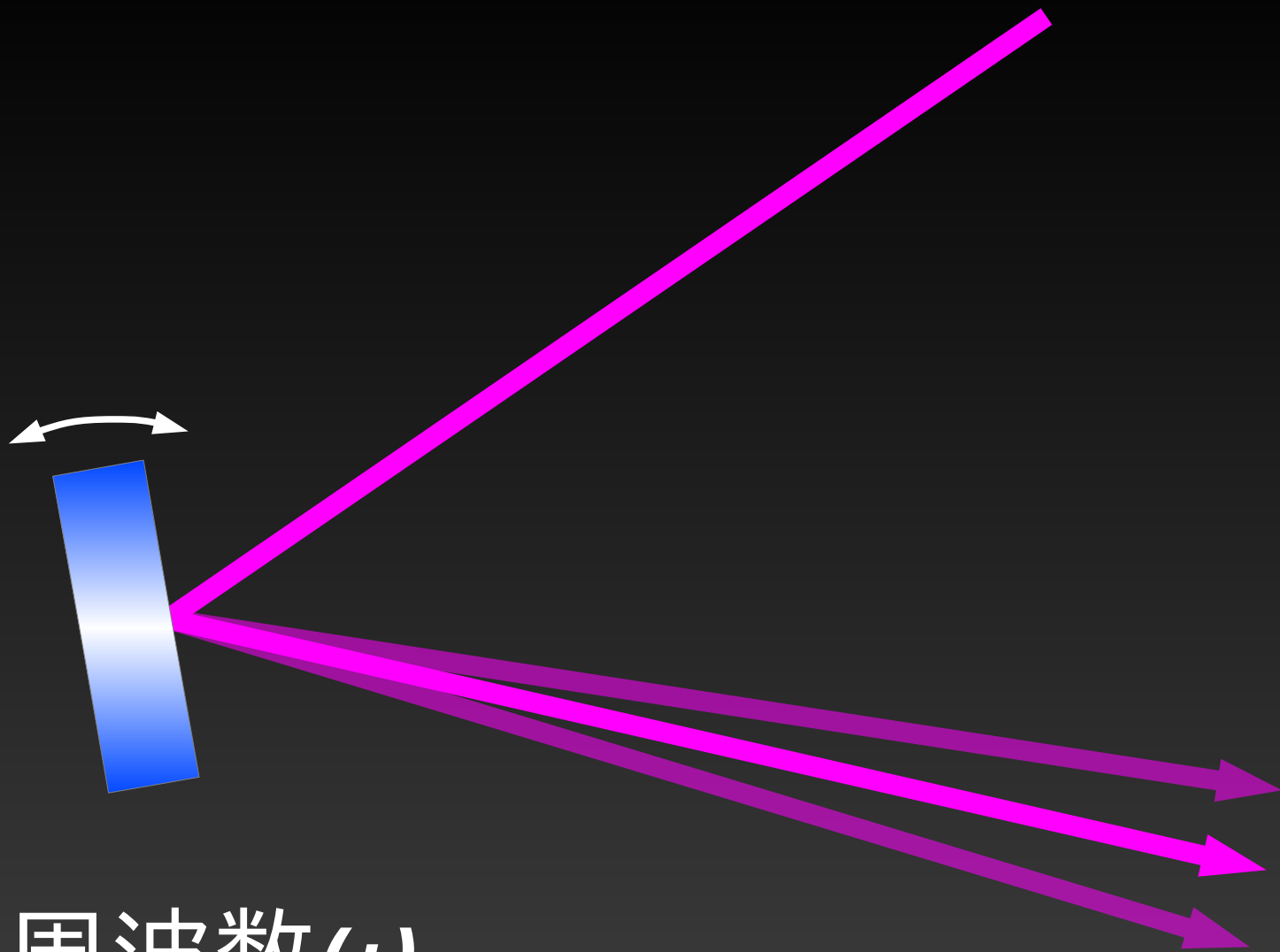
散乱行列

$$\begin{pmatrix} E_{0'}^{00} \\ E_{1'}^{01} \end{pmatrix} = \begin{pmatrix} \clubsuit & \diamondsuit \\ \heartsuit & \spadesuit \end{pmatrix} \begin{pmatrix} E_0^{00} \\ E_1^{01} \end{pmatrix}$$

傾き θ のミラー

$$\begin{pmatrix} E_{0'}^{00} \\ E_{1'}^{01} \end{pmatrix} = \begin{pmatrix} \sqrt{1 - 4\alpha^2} & 2i\alpha \\ 2i\alpha & \sqrt{1 - 4\alpha^2} \end{pmatrix} \begin{pmatrix} E_0^{00} \\ E_1^{01} \end{pmatrix}$$

$$\alpha = \frac{\pi w}{\lambda} \theta$$



角周波数 ω

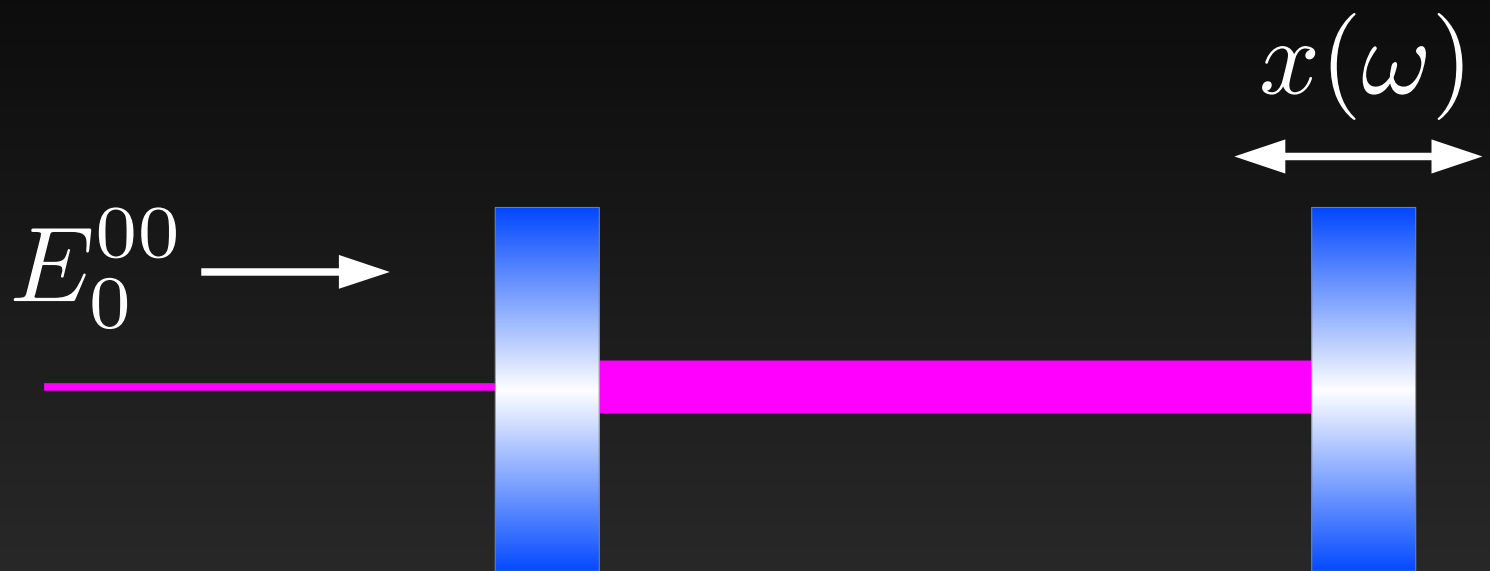
±ωのサイドバンド生成

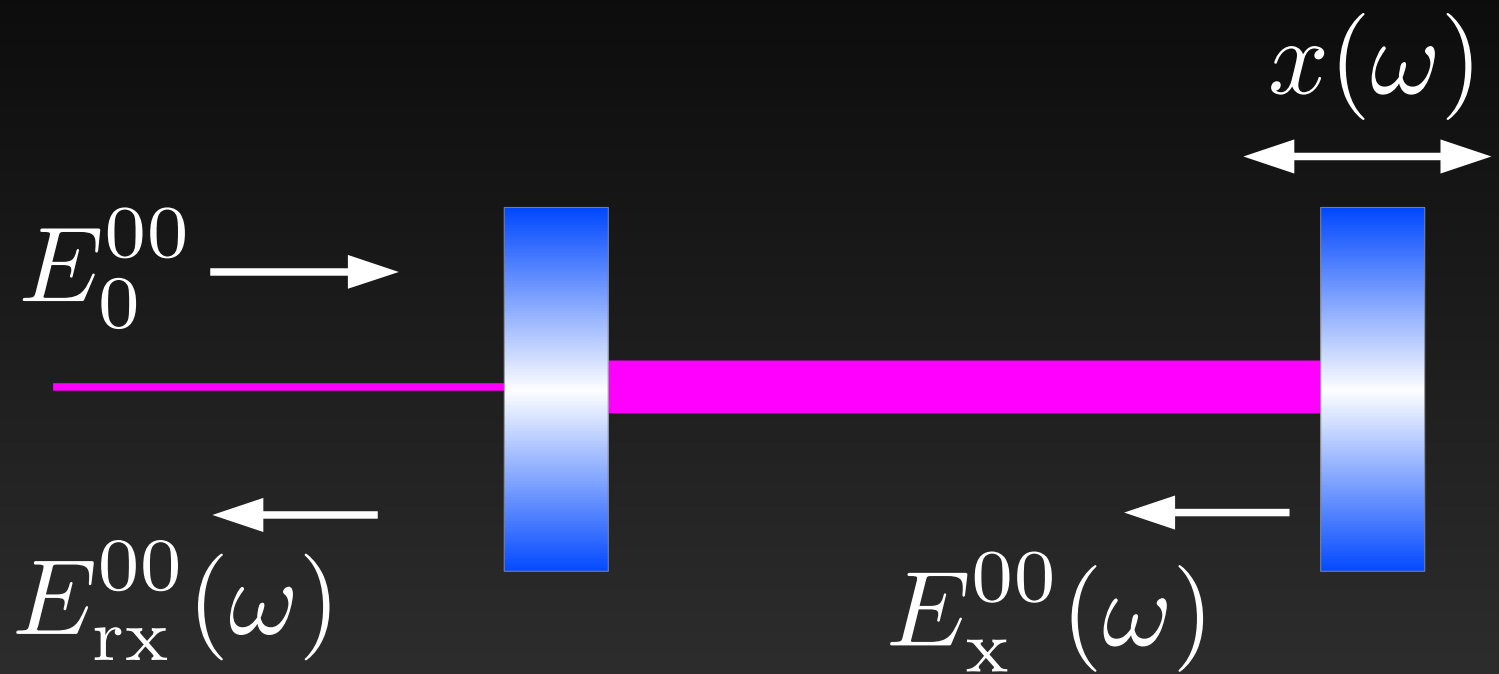
$$E_0^{00}$$



$$E_{0'}^{00} + E_1^{01} e^{i\omega t} + E_1^{01} e^{-i\omega t}$$

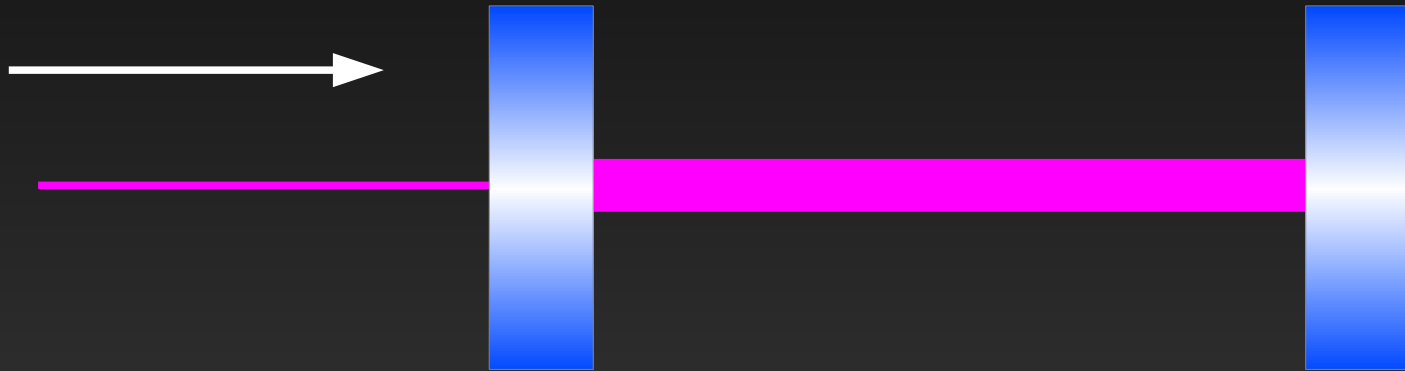


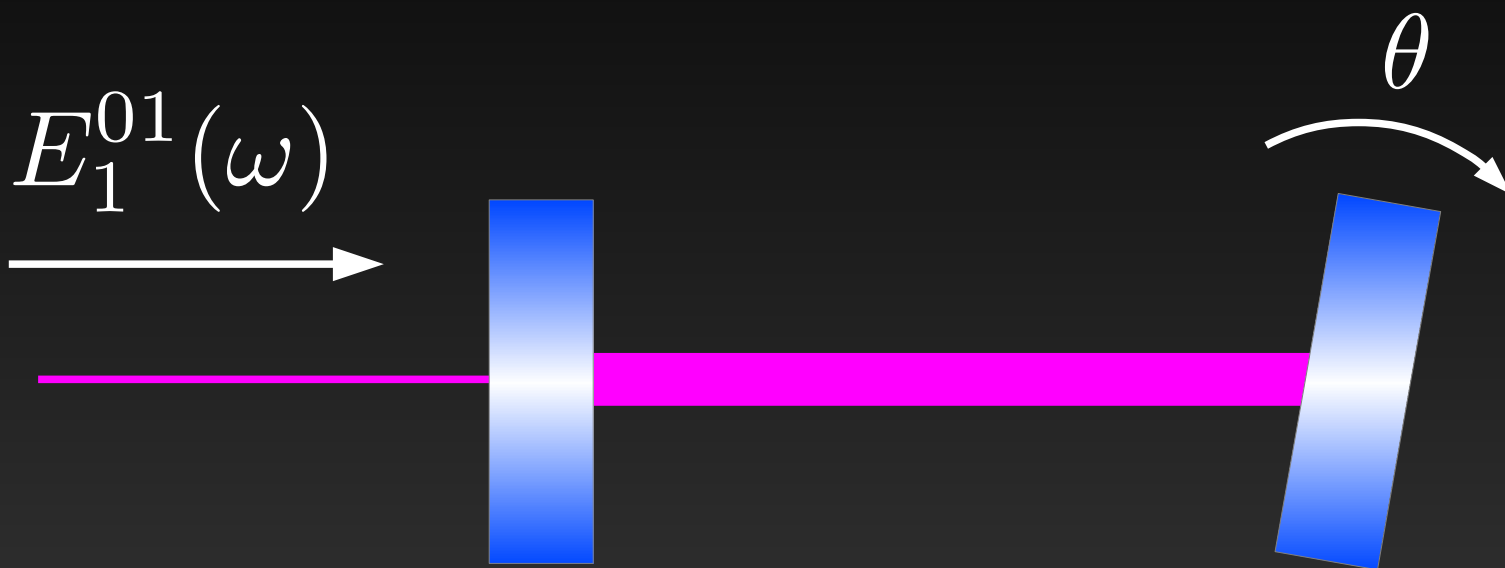


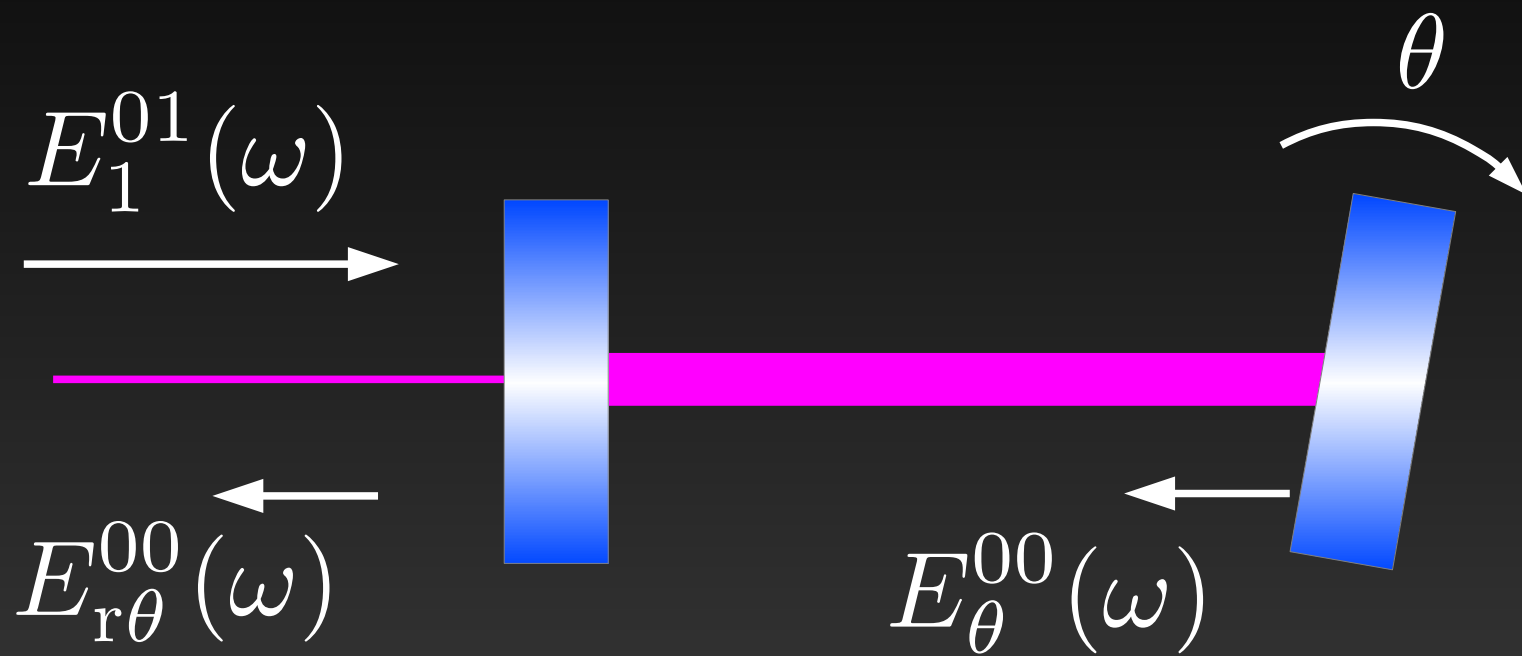


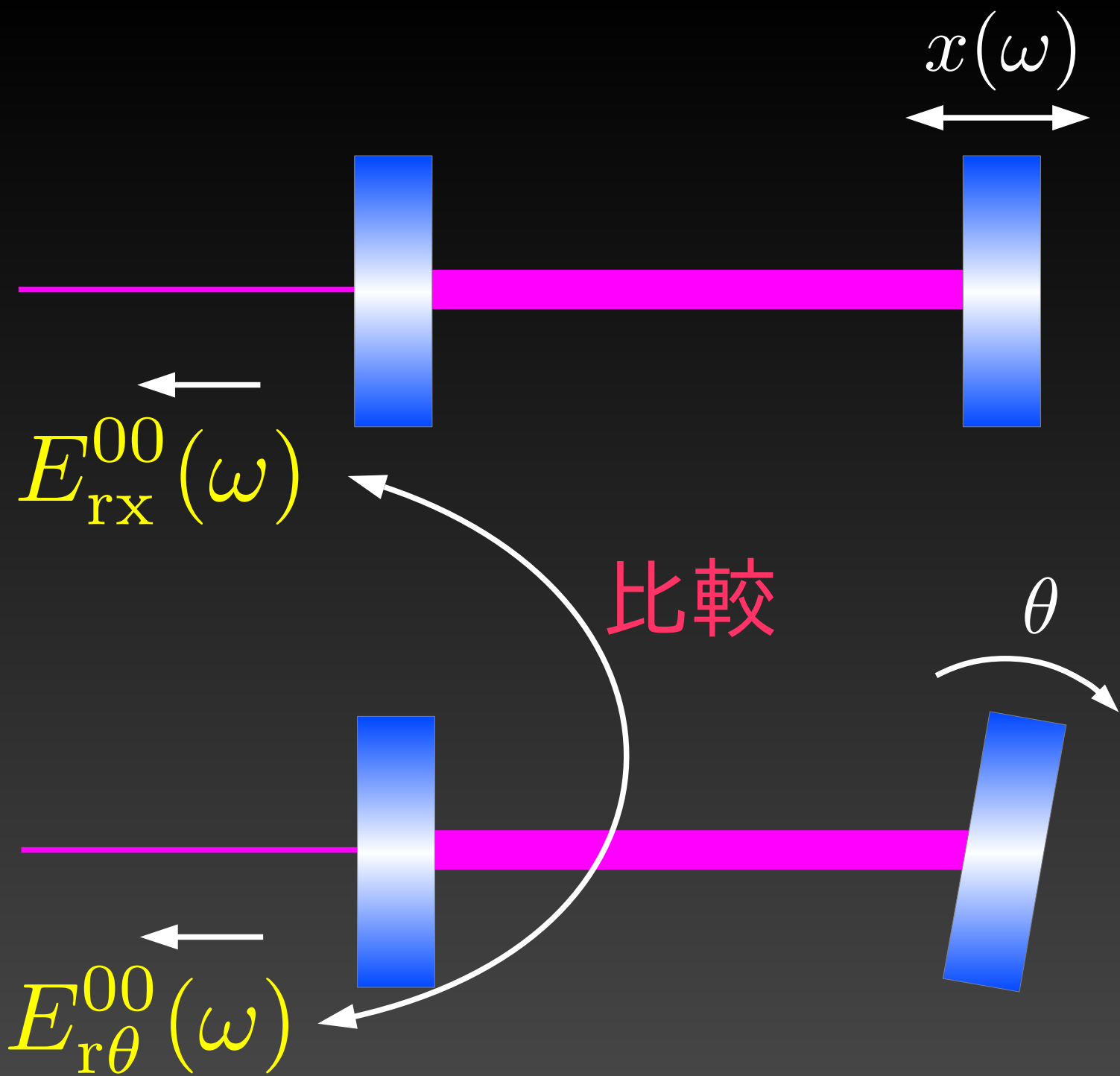
ビームジッタ サイドバンド

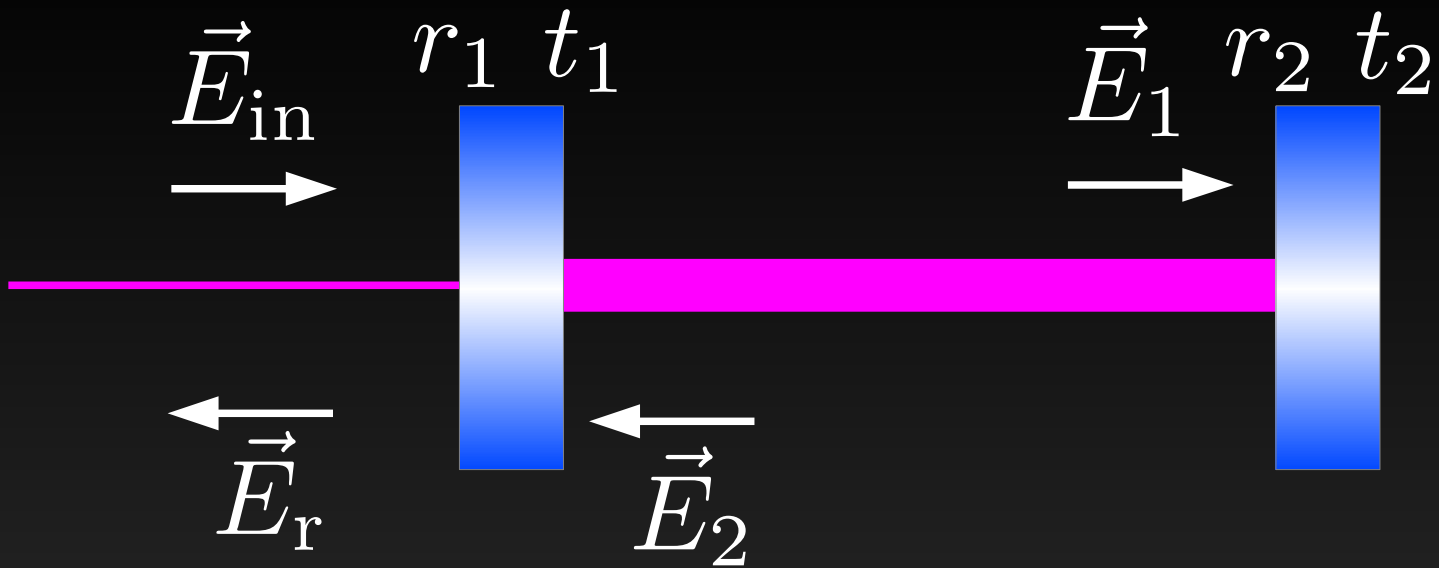
$$E_0^{00} + E_1^{01}(\omega) + E_1^{01}(-\omega)$$



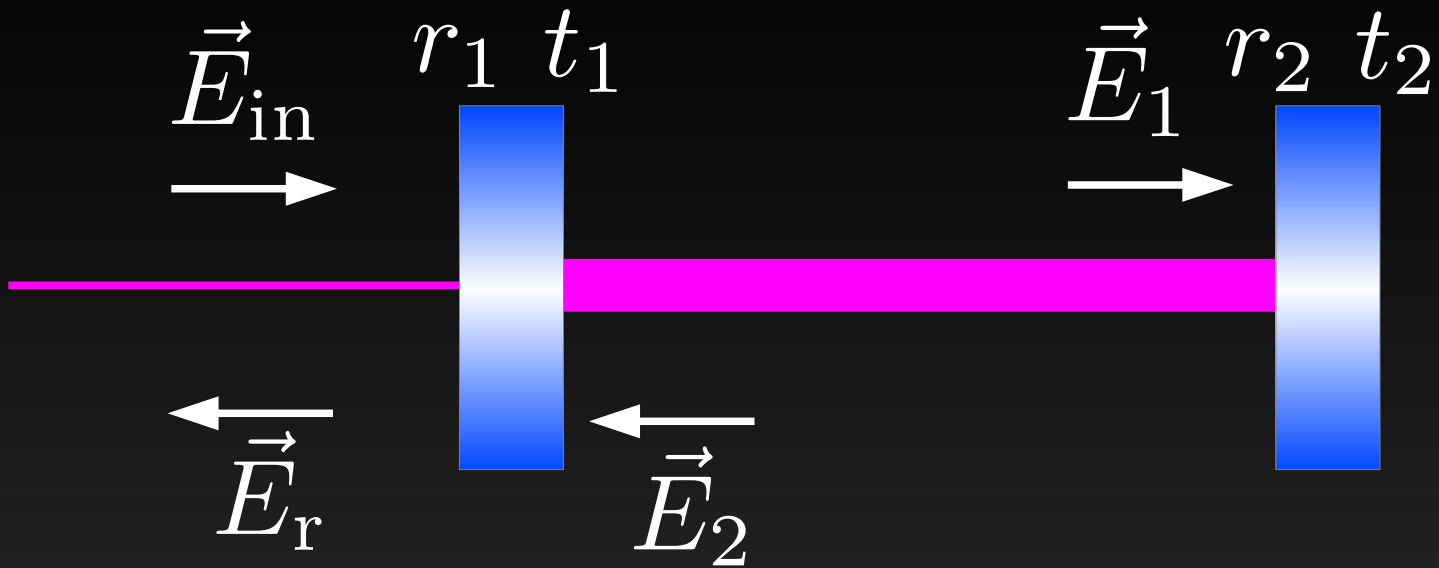




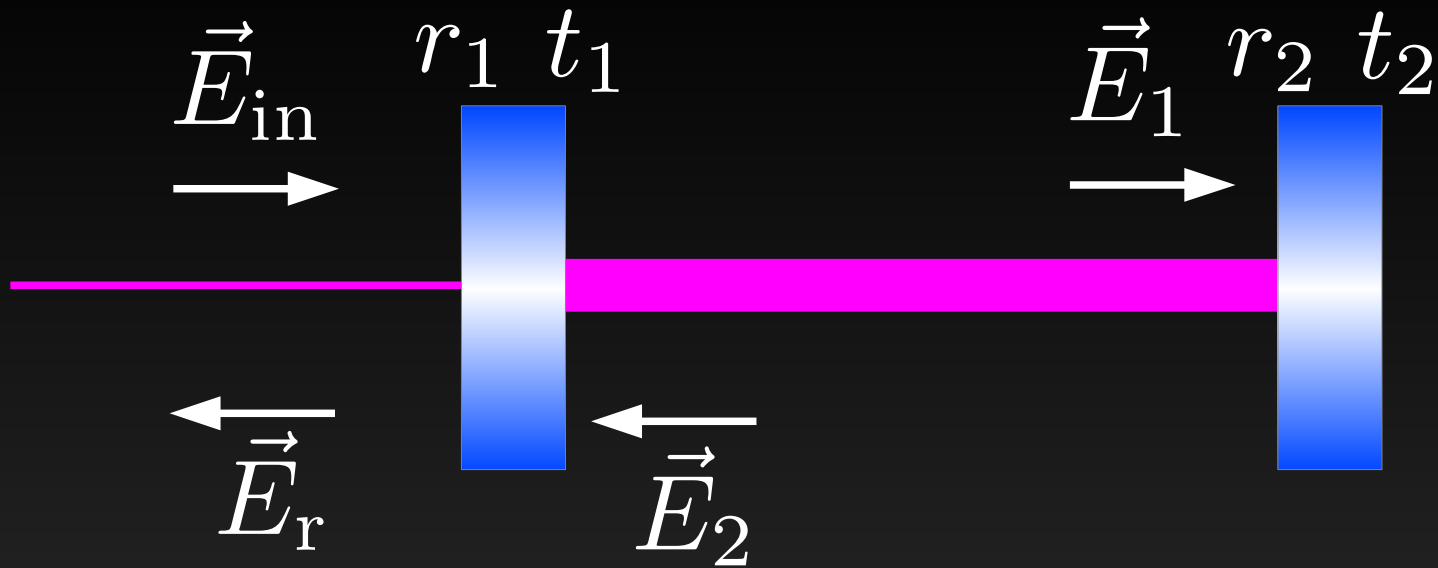




$$\vec{E}_{\text{in}} = \begin{pmatrix} E_{\text{in}}^{00} \\ E_{\text{in}}^{01} \end{pmatrix}$$

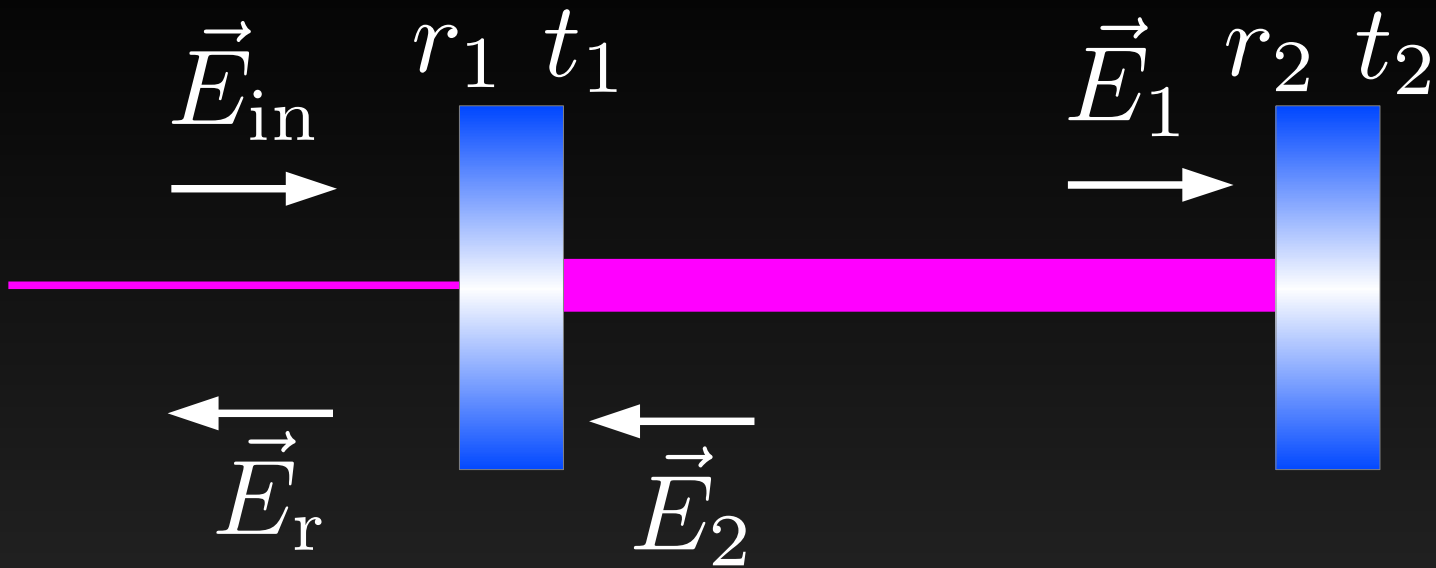


$$\vec{E}_1 = L \cdot R1 \cdot \vec{E}_2 + T1 \cdot \vec{E}_{\text{in}}$$



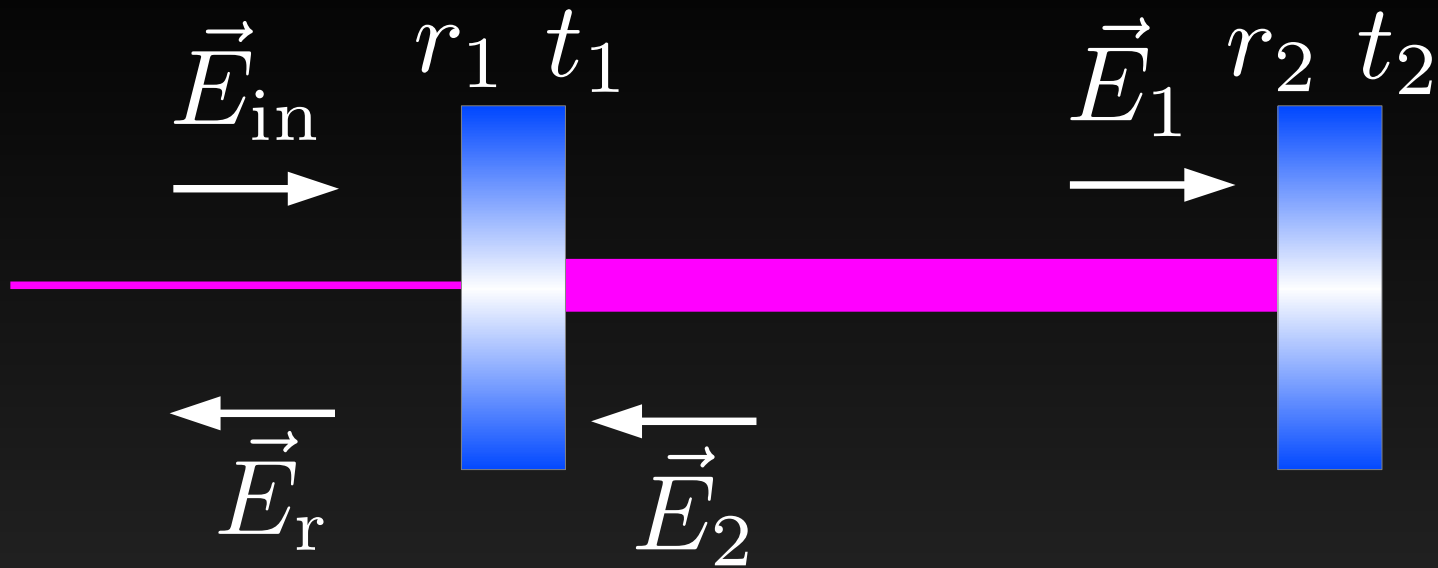
$$\vec{E}_1 = L \cdot \textcircled{R1} \cdot \vec{E}_2 + T1 \cdot \vec{E}_{\text{in}}$$

$$R1 = r_1 \begin{pmatrix} \sqrt{1 - 4\alpha^2} & 2i\alpha \\ 2i\alpha & \sqrt{1 - 4\alpha^2} \end{pmatrix}$$



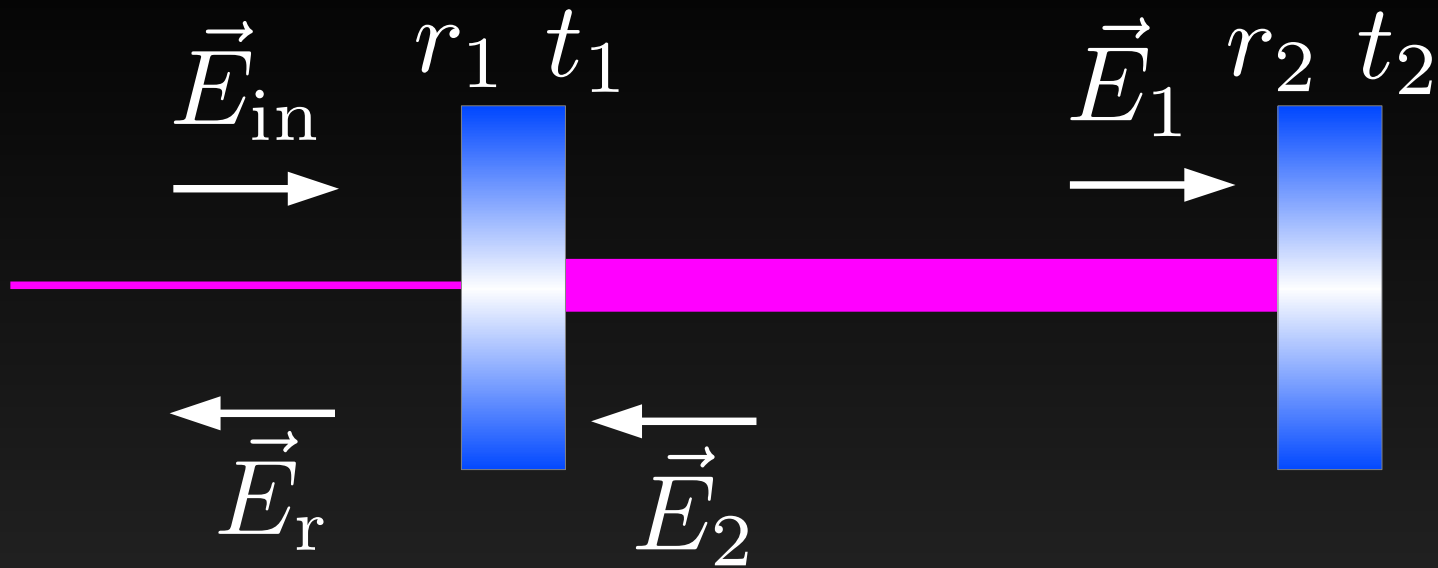
$$\vec{E}_1 = L \cdot R1 \cdot \vec{E}_2 + T1 \cdot \vec{E}_{\text{in}}$$

$$T1 = t_1 \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix}$$



$$\vec{E}_1 = L \cdot R1 \cdot \vec{E}_2 + T1 \cdot \vec{E}_{\text{in}}$$

$$L = \begin{pmatrix} e^{-i\omega L/c} & 0 \\ 0 & e^{-i\omega L/c + i\Phi_{\text{Gouy}}} \end{pmatrix}$$

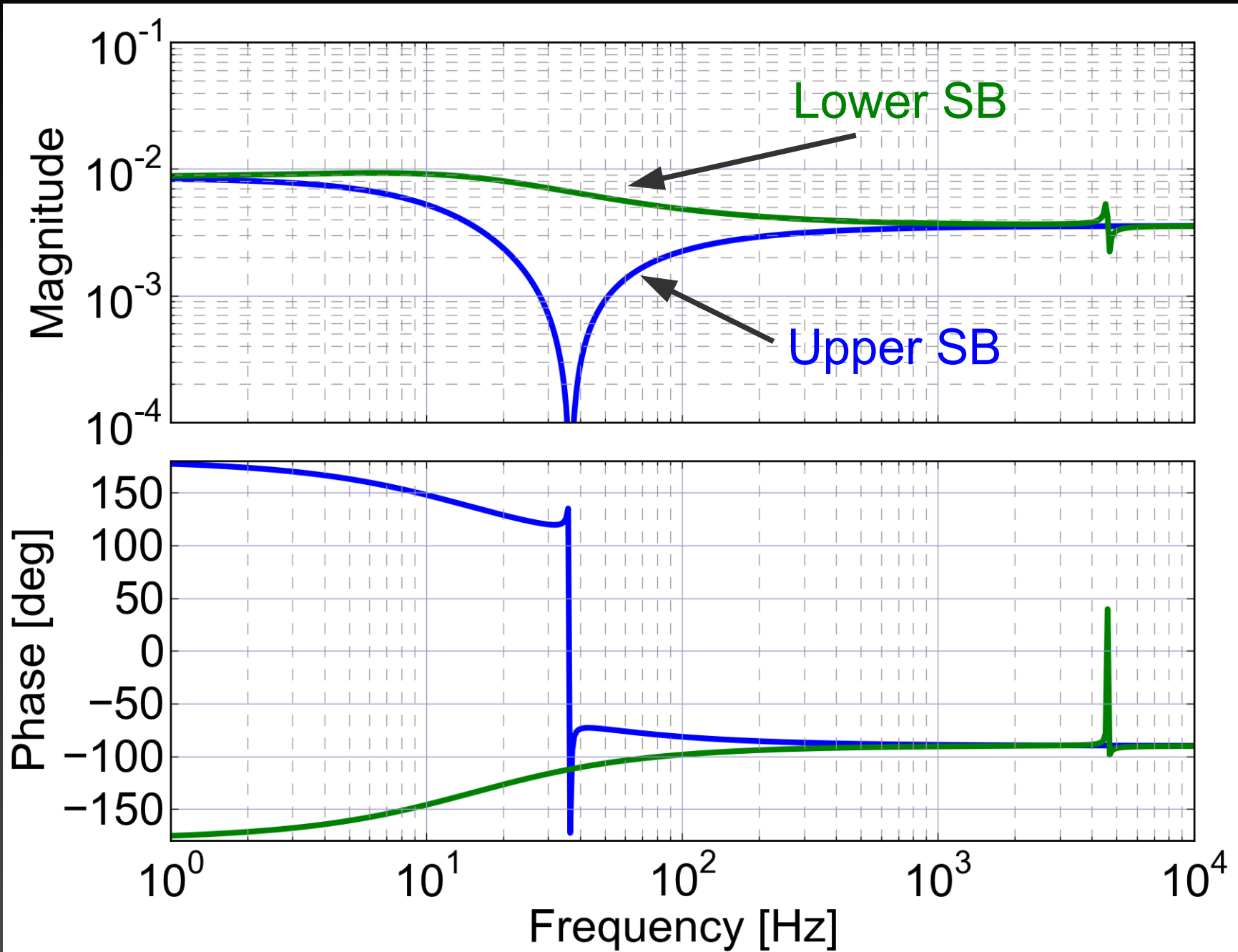


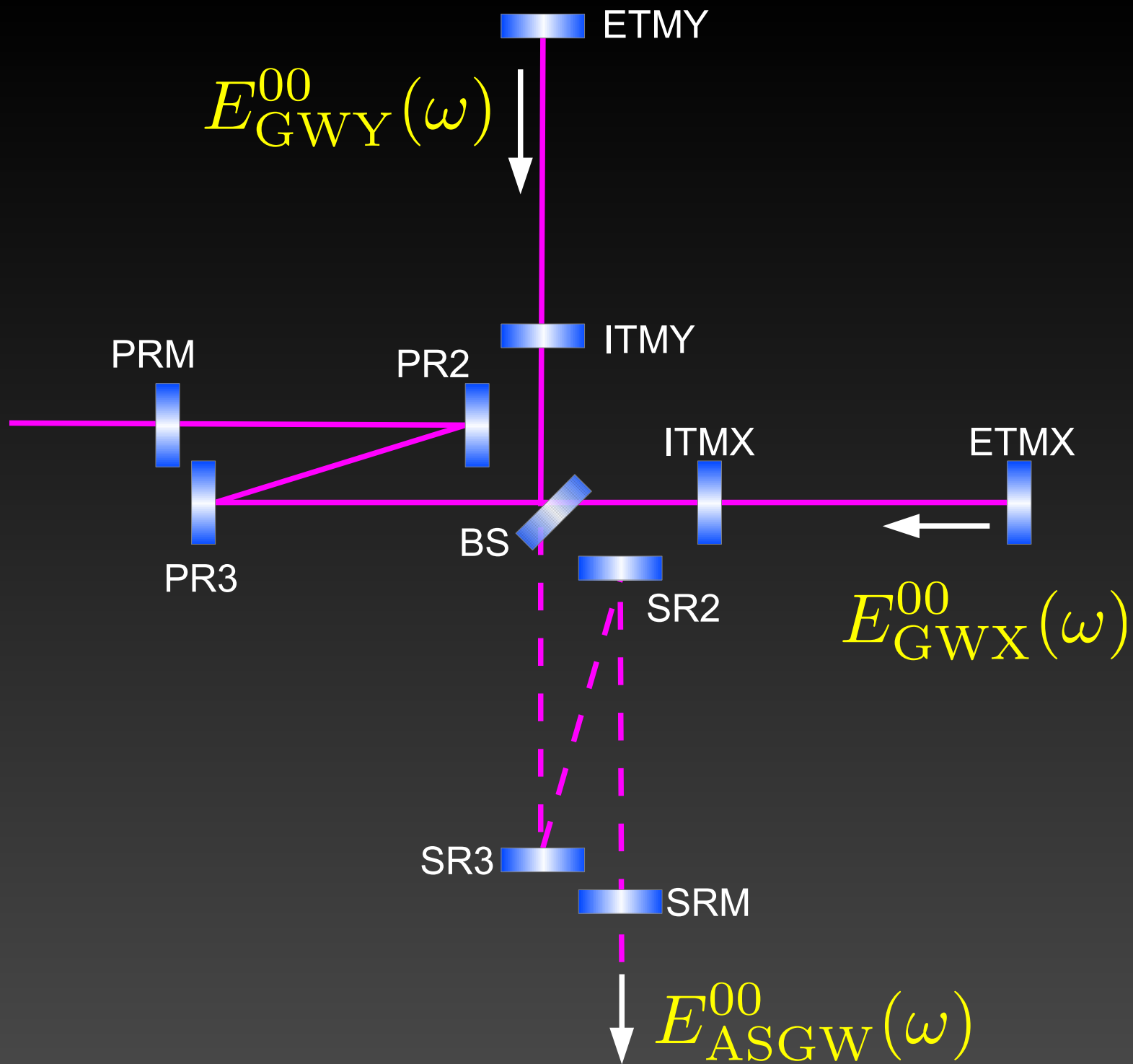
$$\vec{E}_1 = L \cdot R1 \cdot \vec{E}_2 + T1 \cdot \vec{E}_{\text{in}}$$

$$\vec{E}_2 = L \cdot R2 \cdot \vec{E}_1$$

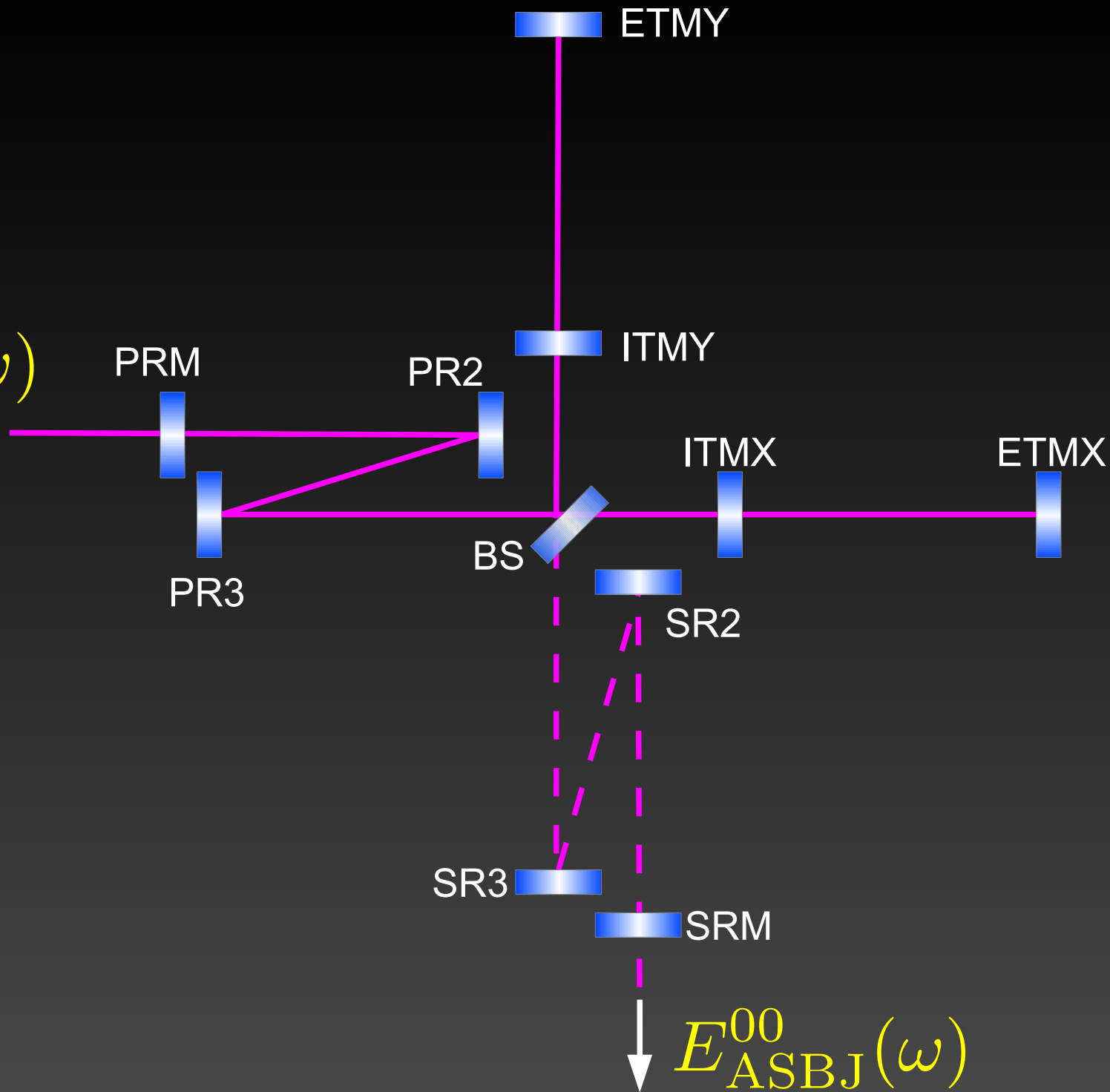
$$\vec{E}_r = T1 \cdot \vec{E}_2 - R1_{\text{back}} \cdot \vec{E}_{\text{in}}$$

TEM01 -> TEM00 伝達関数 (ITM 傾き 10^{-8} rad)



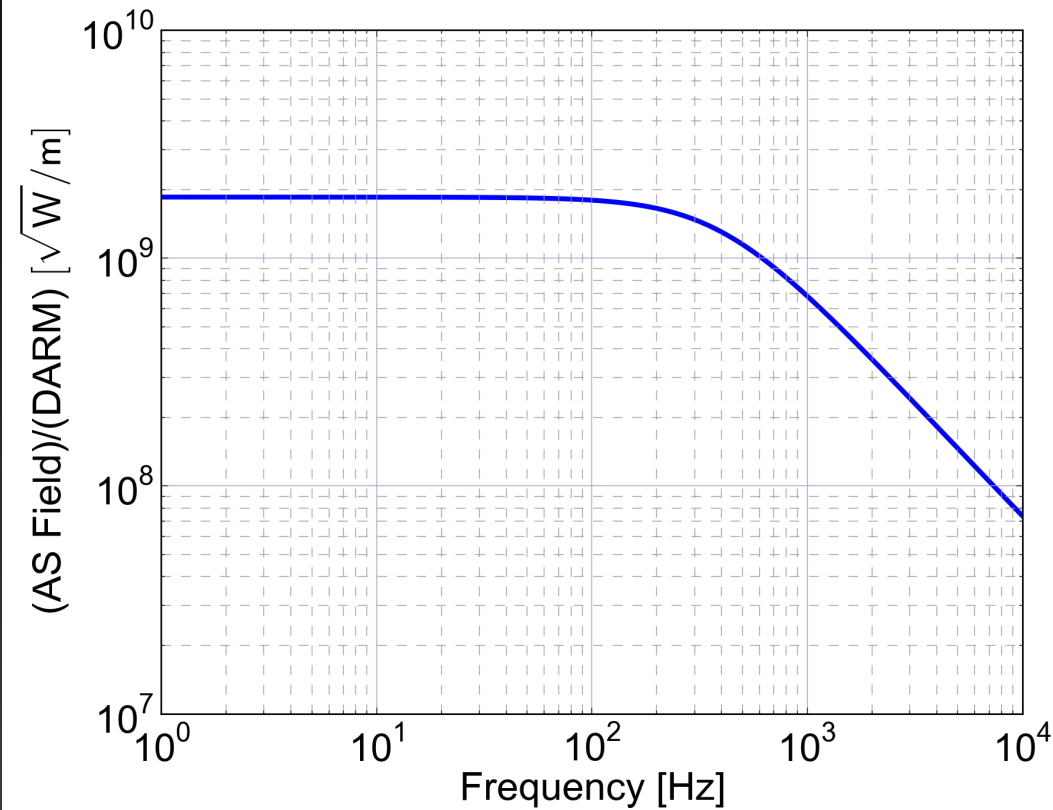


$$E_{BJ}^{01}(\omega)$$

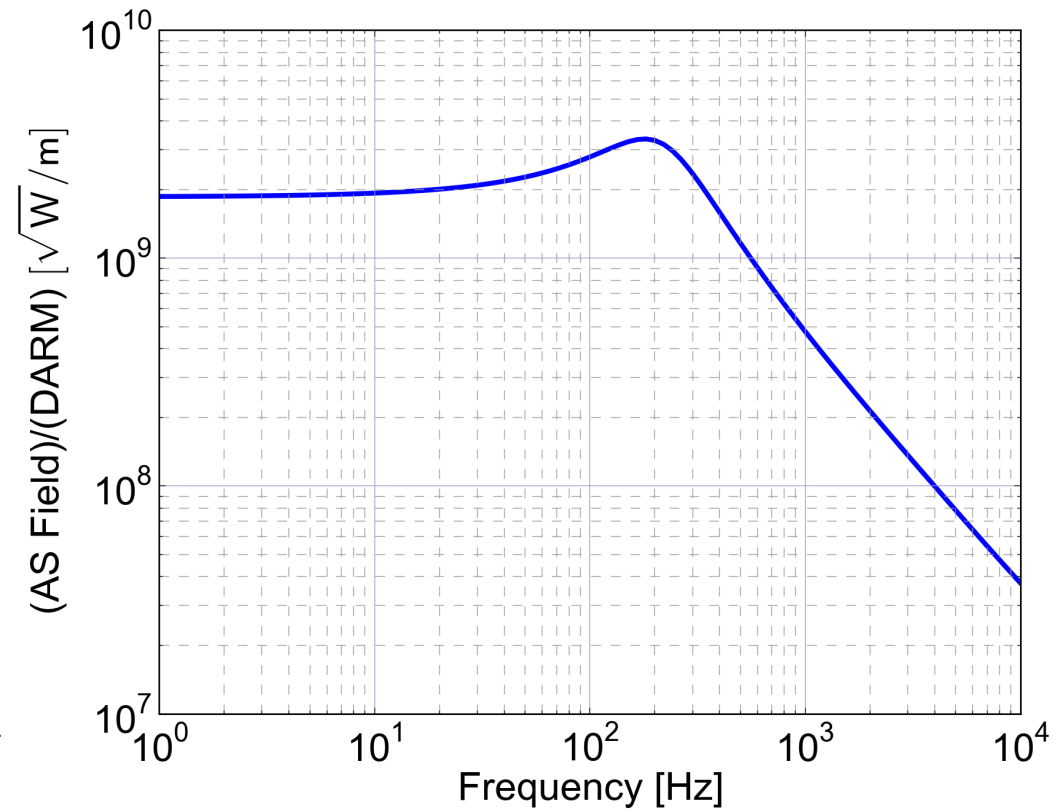


DARM -> GW Sideband @ AS Port

BRSE

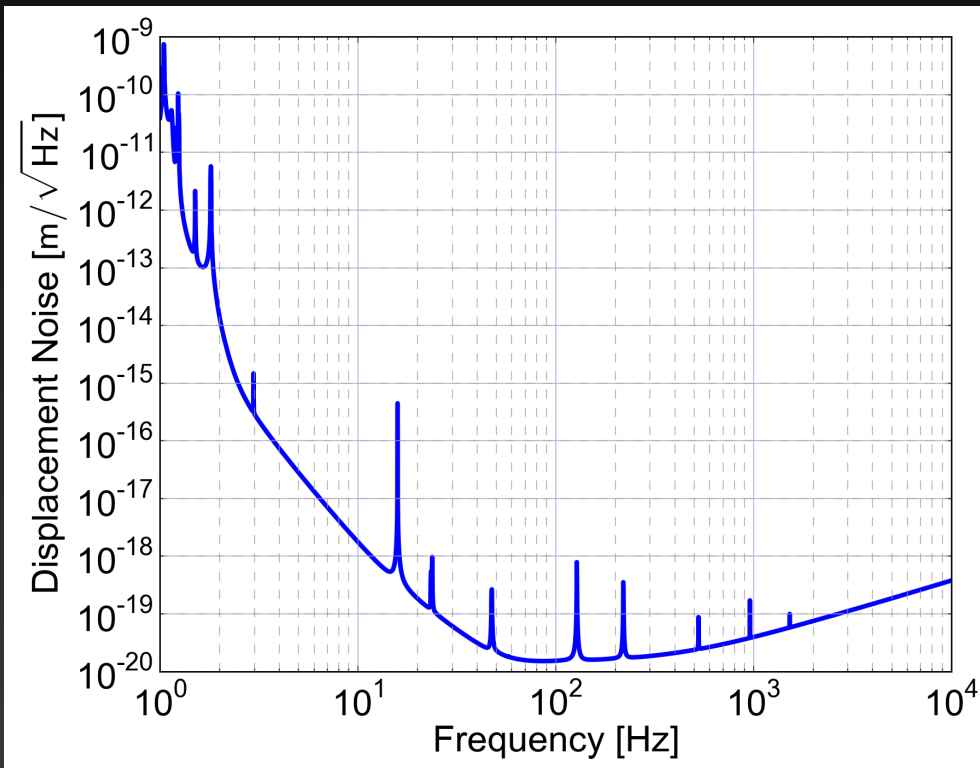


DRSE

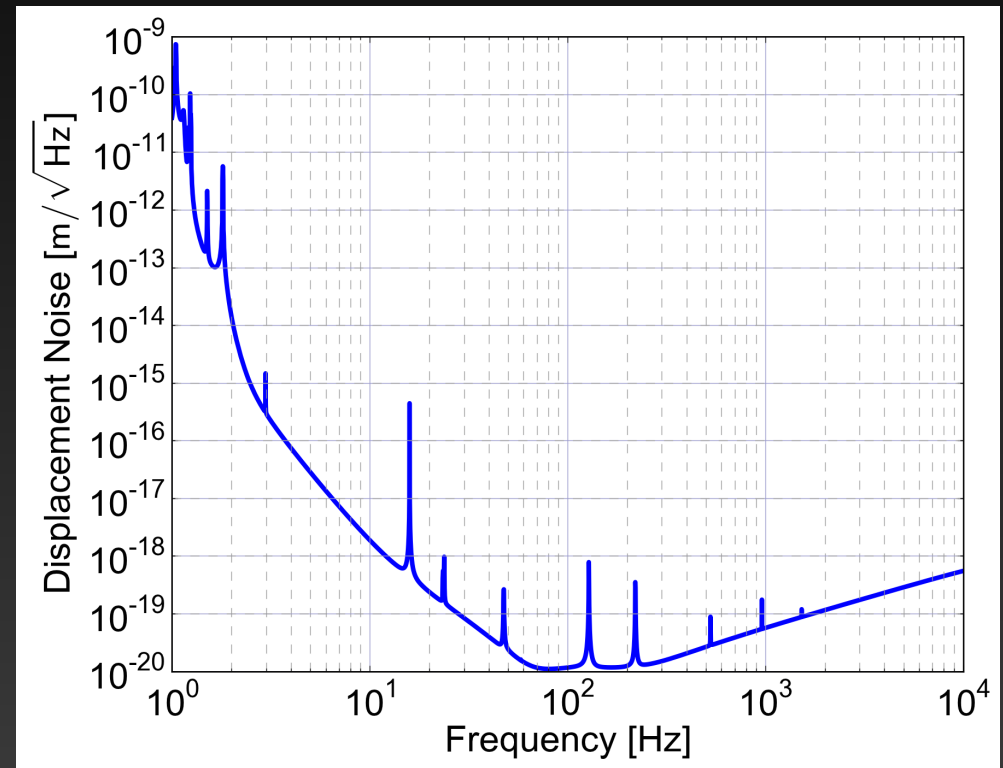


KAGRA変位換算雑音

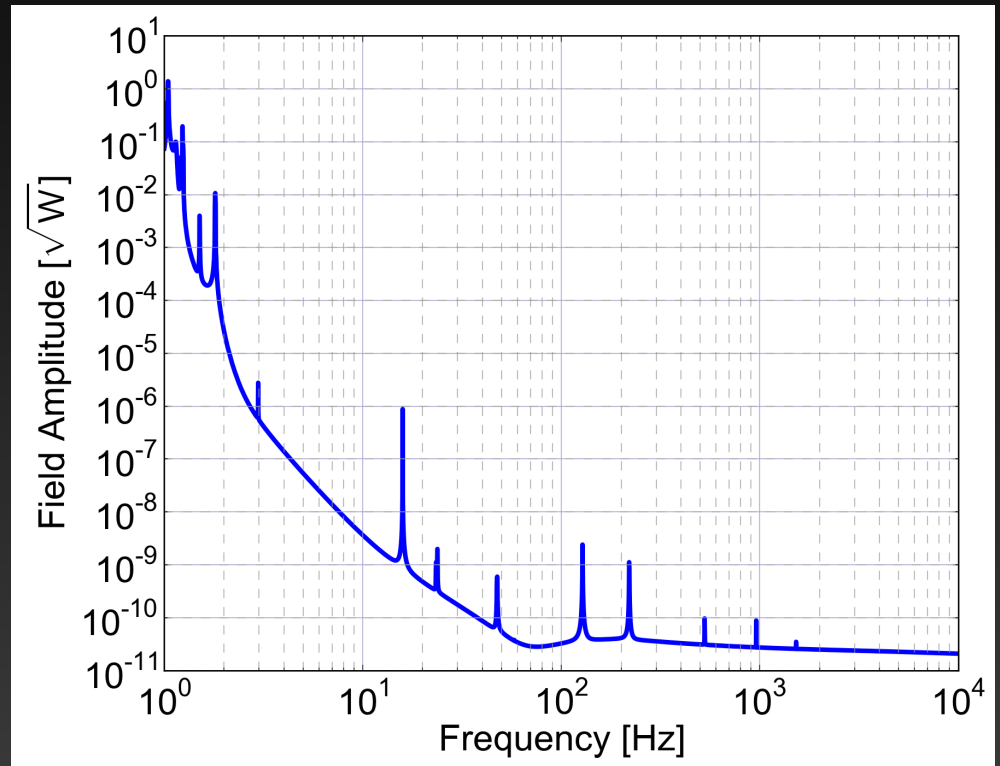
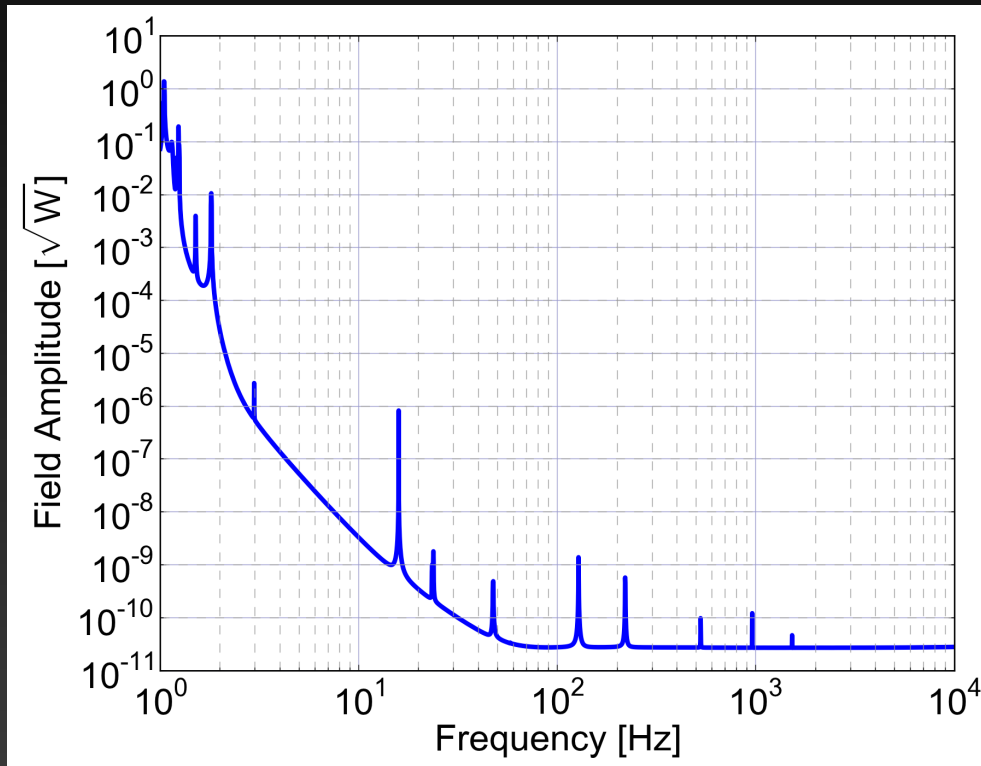
BRSE



DRSE

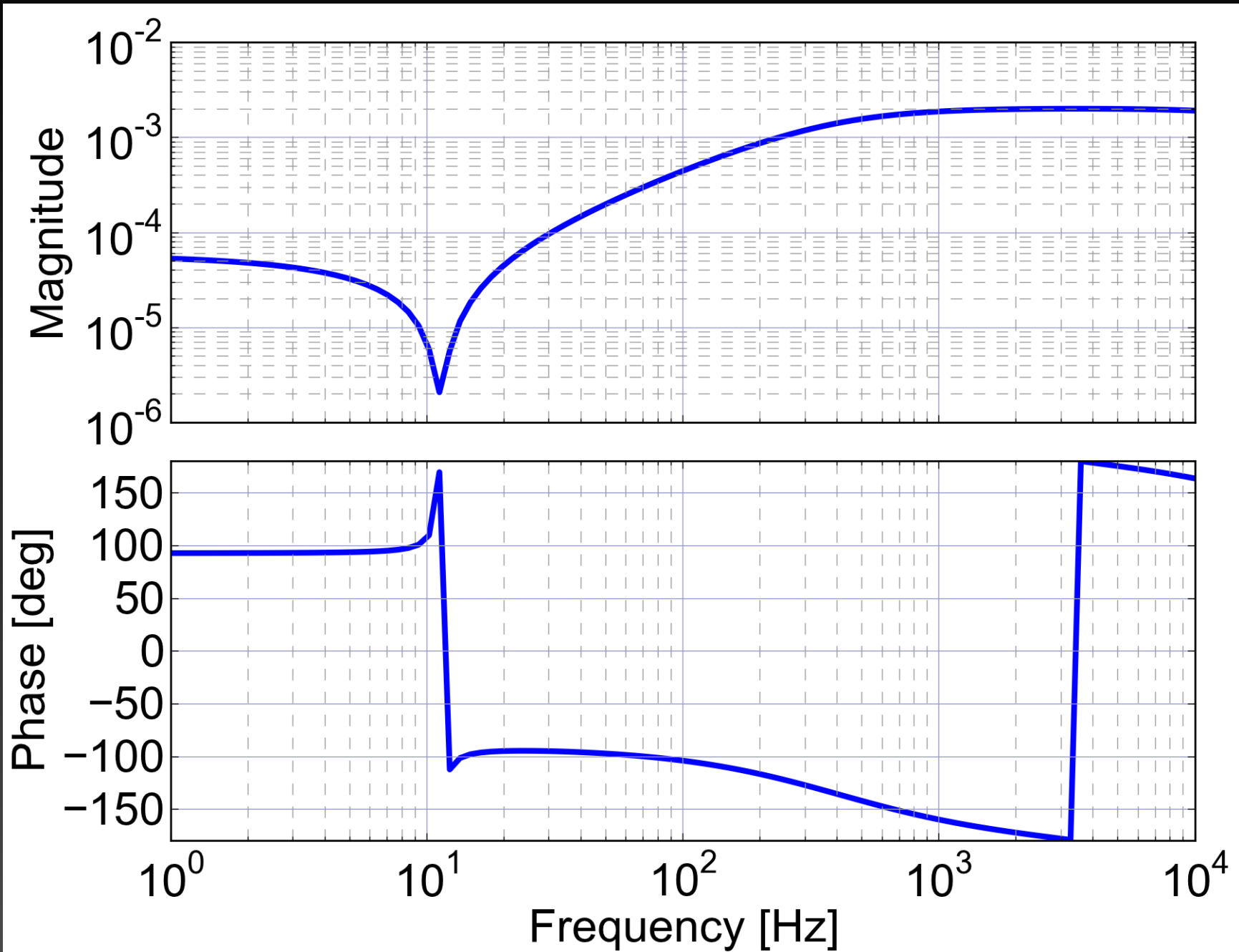


GW Sideband Amplitude @ AS Port

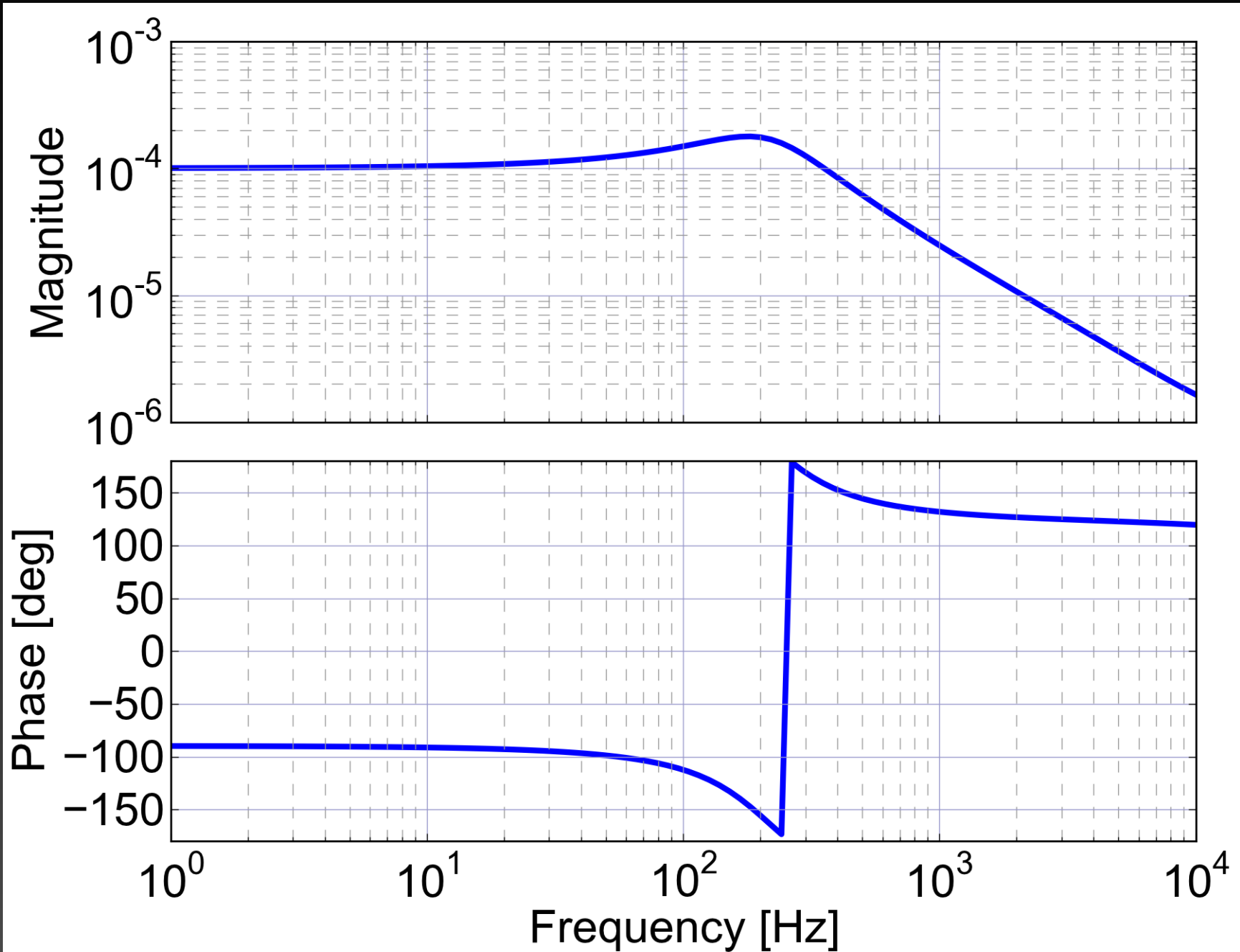


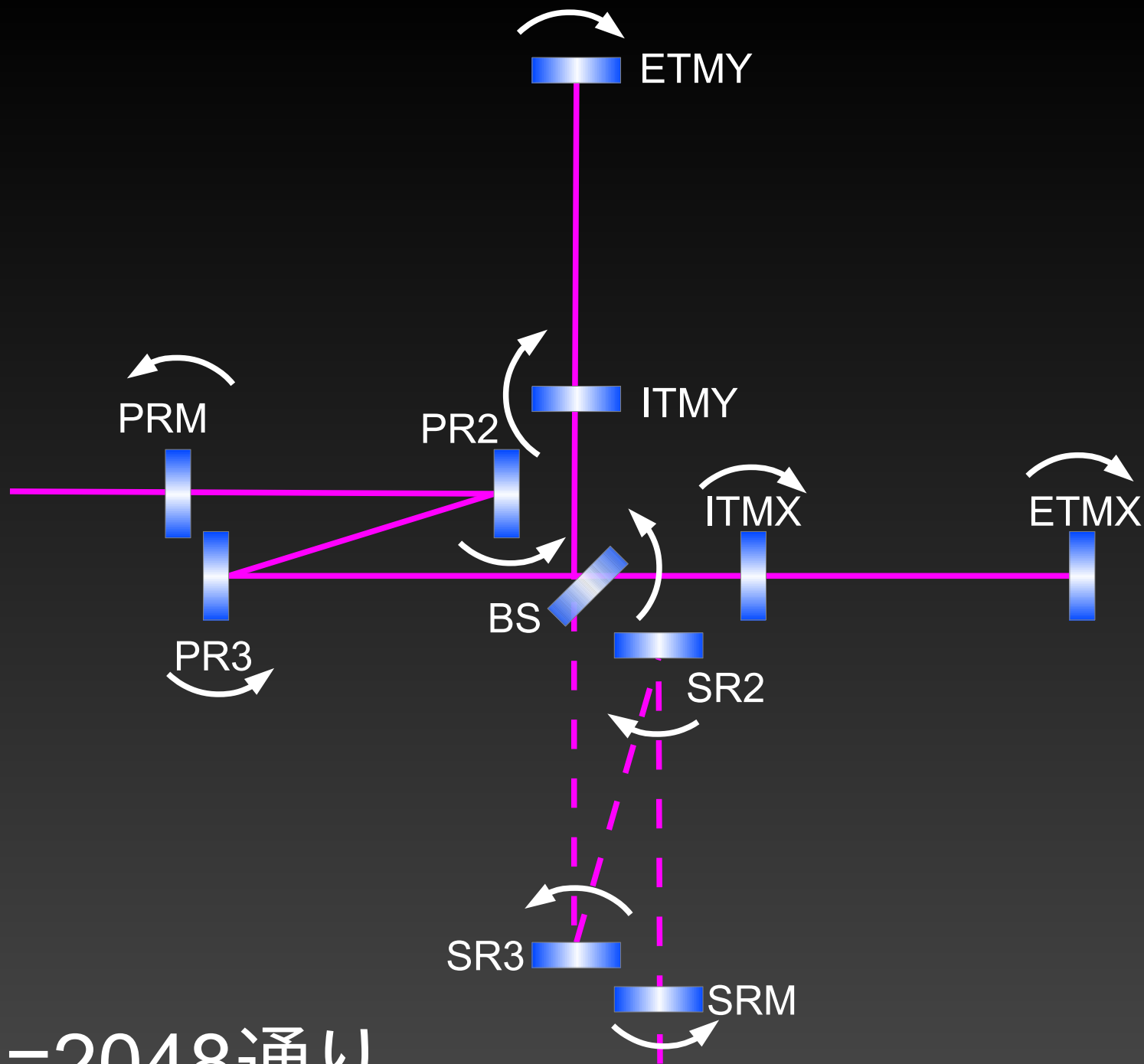
入射パワー1Wに換算

TEM01 @ Input -> TEM00 @ AS Port (BRSE, ITM差動傾き 10^{-8} rad)



TEM01 @ Input -> TEM00 @ AS Port
(DRSE, ETM差動傾き 10^{-8} rad)

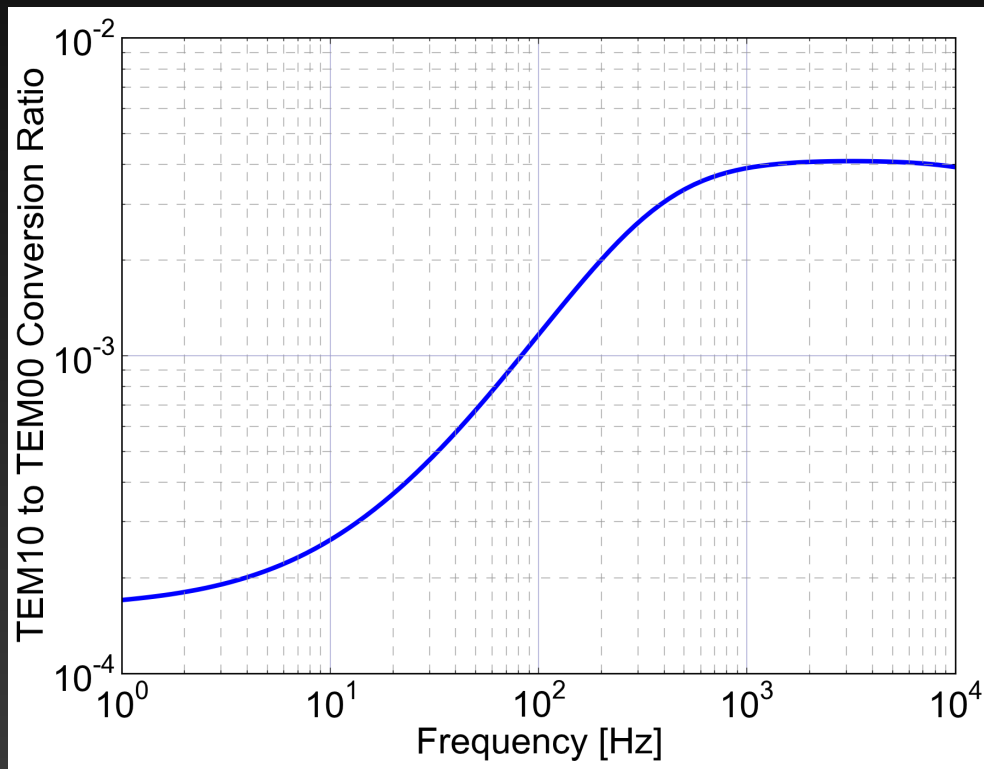




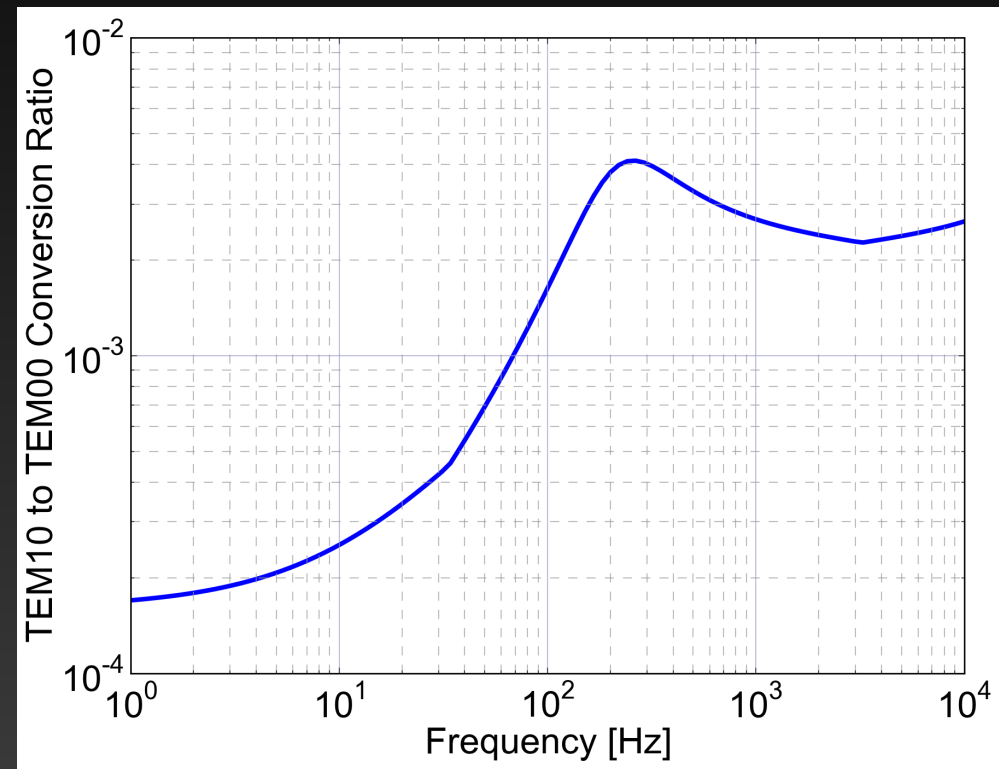
$2^{11}=2048$ 通り

TEM01 -> TEM00 伝達関数 最大値

BRSE

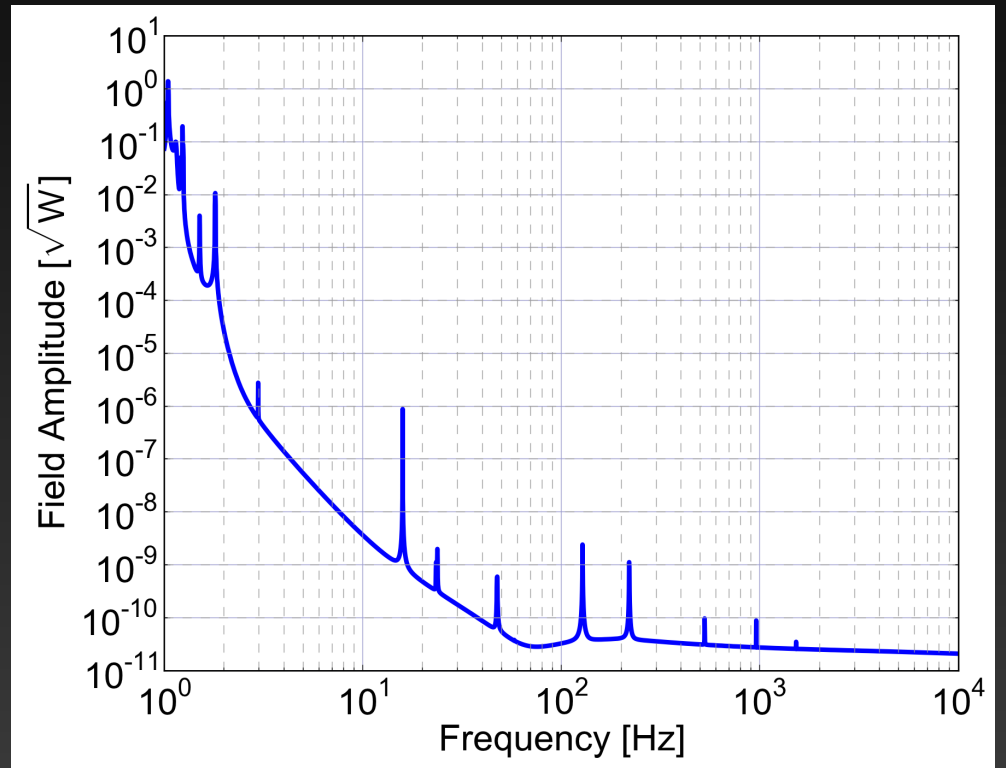
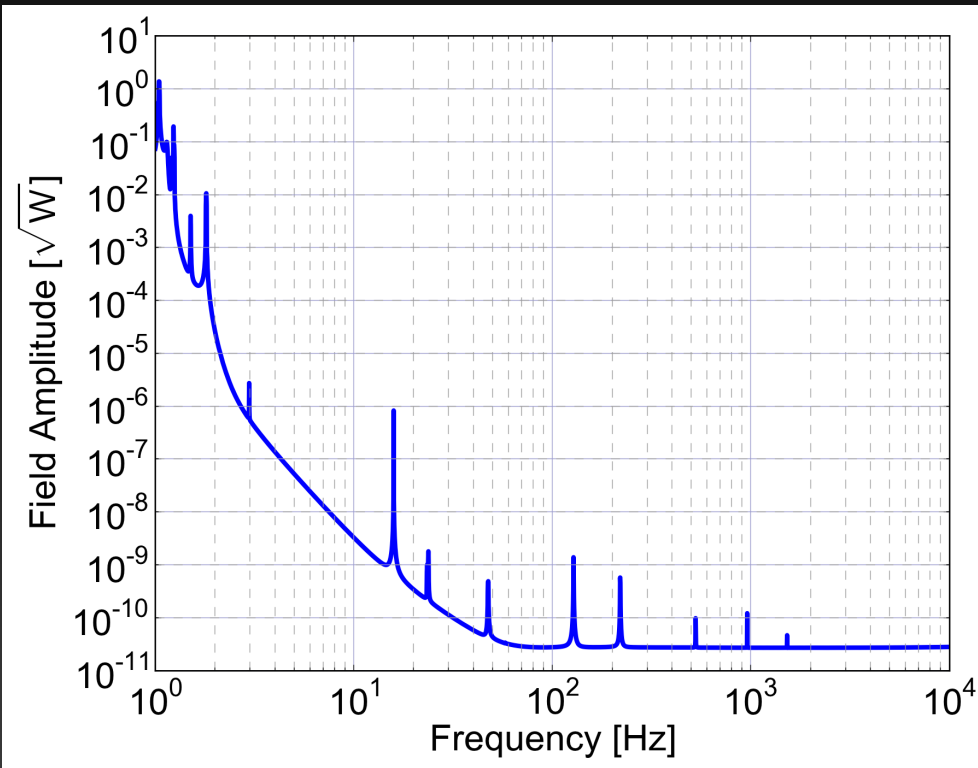


DRSE

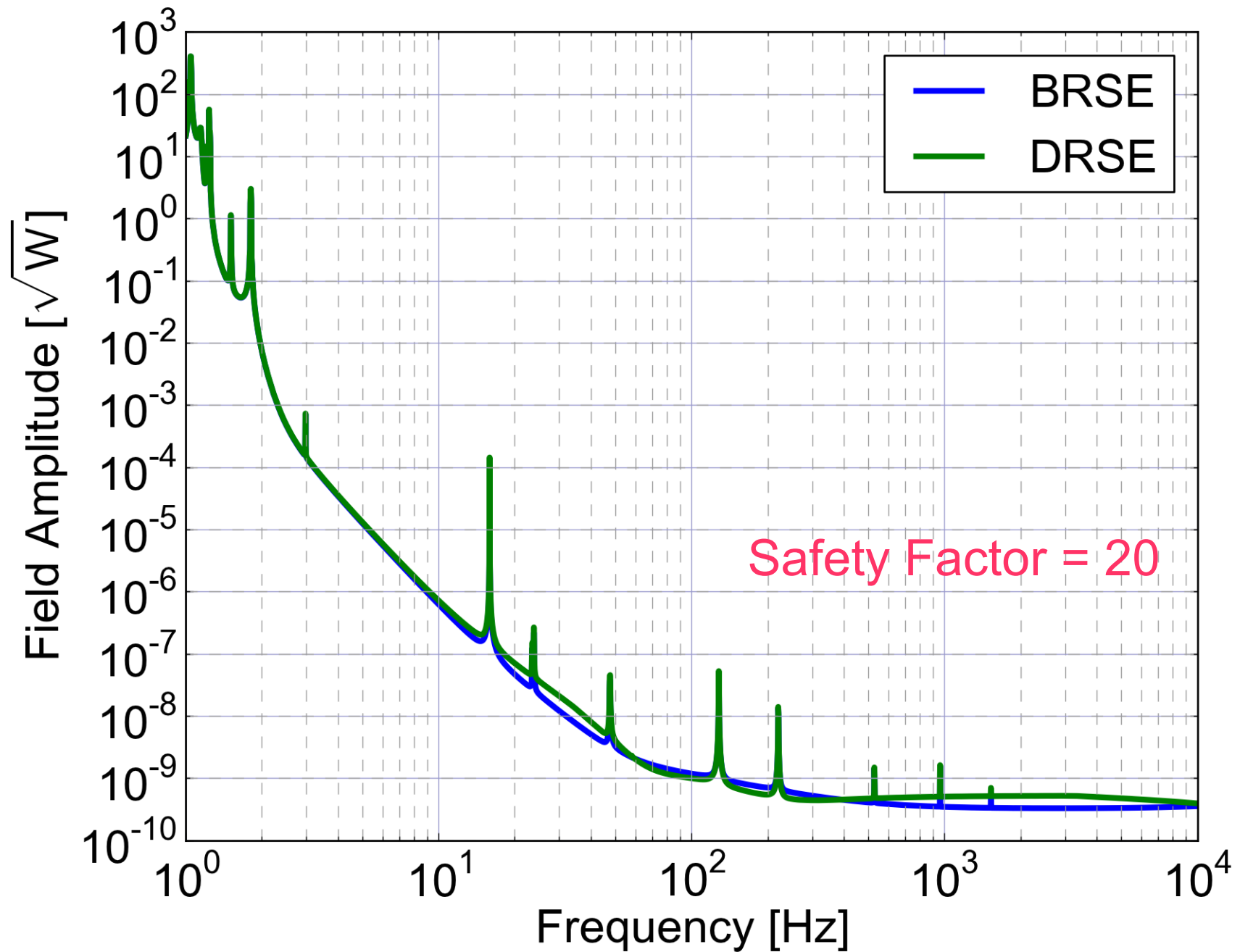


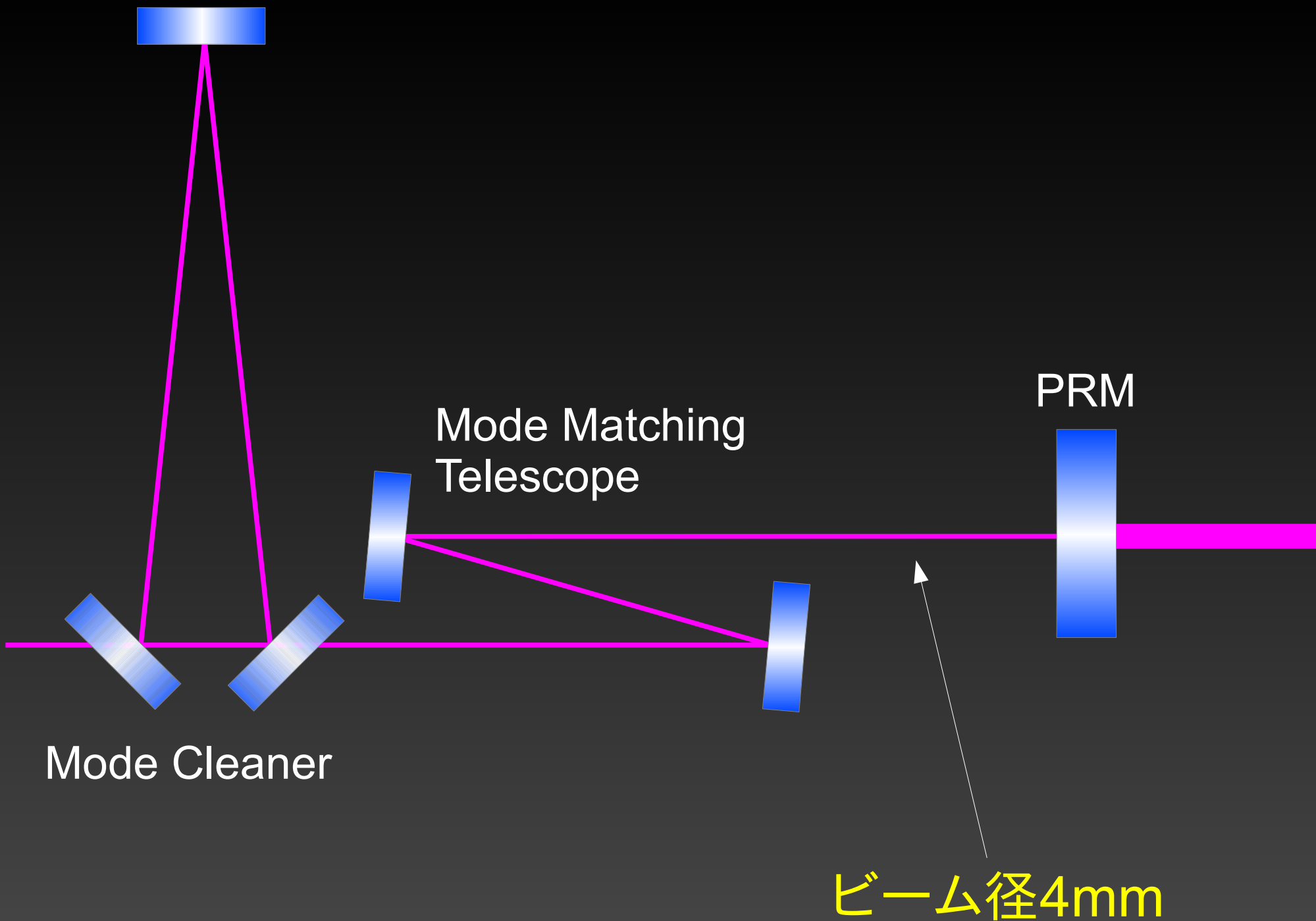
各鏡の傾きは 10^{-8} rad

GW Sideband Amplitude @ AS Port

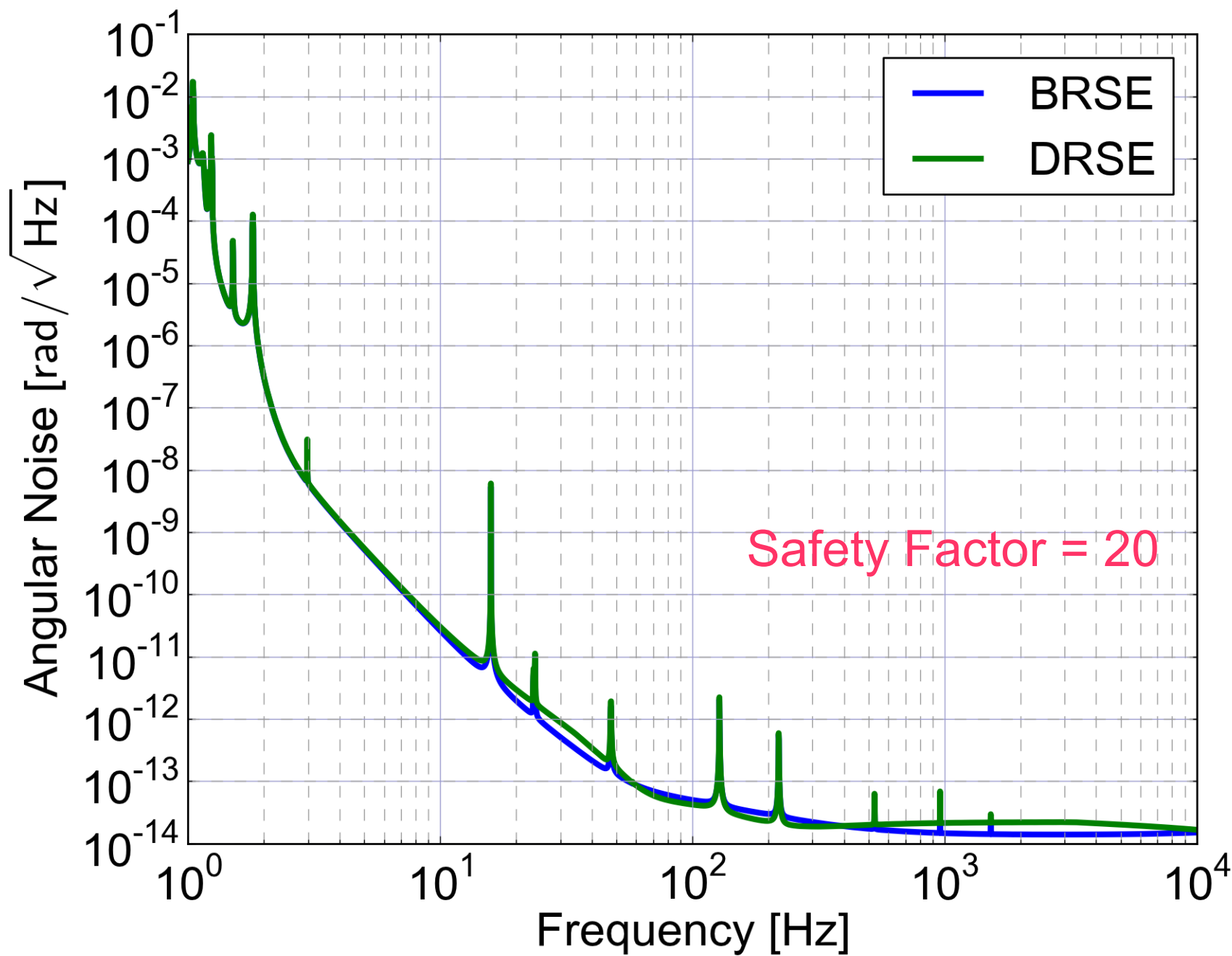


入射TEM01振幅への要求値(入射パワー1W)

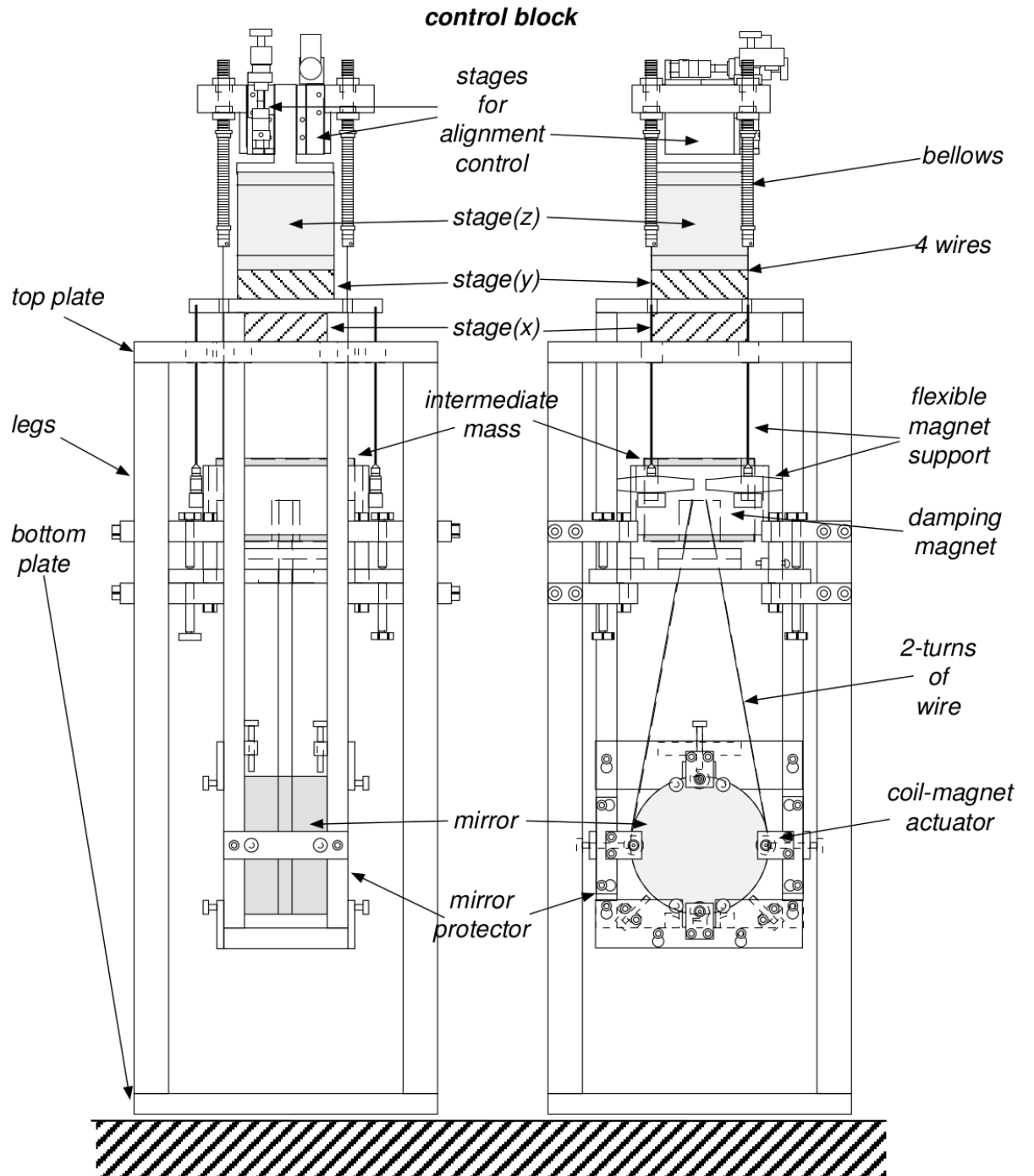




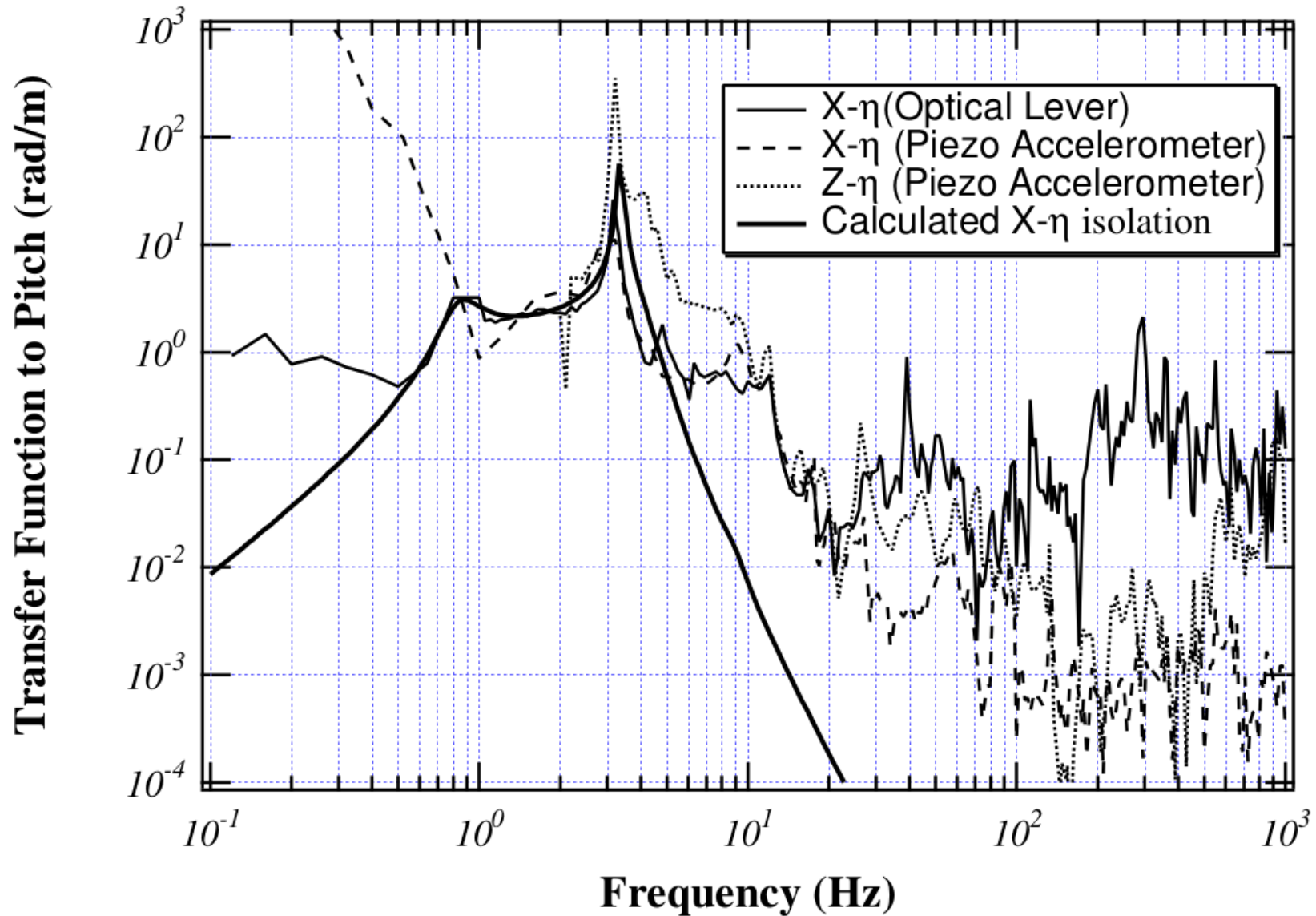
入射光学系回轉雜音要求值



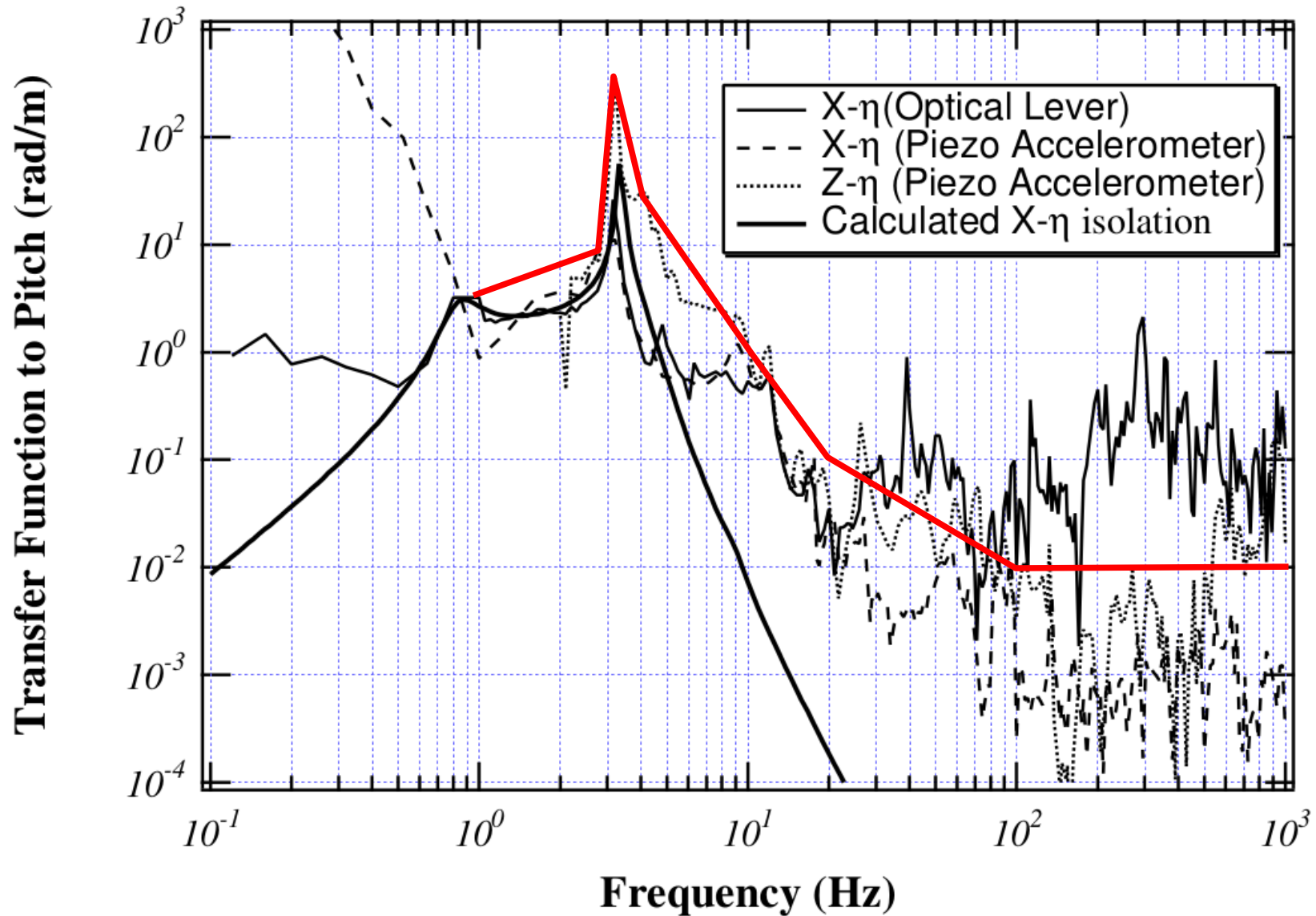
TAMA Suspension



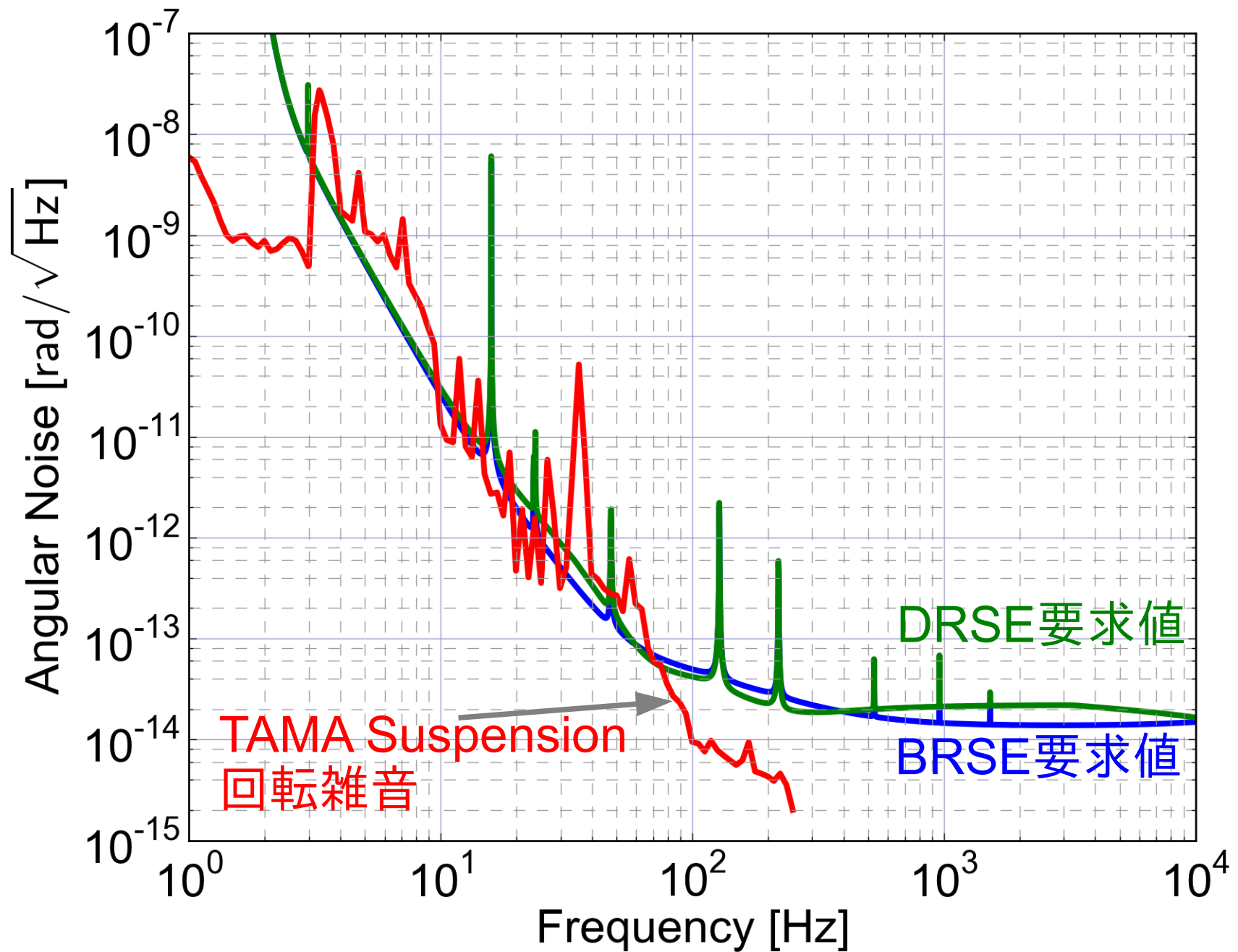
TAMA Suspension 並進→Pitch 伝達関数



TAMA Suspension 並進→Pitch 伝達関数



推定回轉雜音 vs 要求値

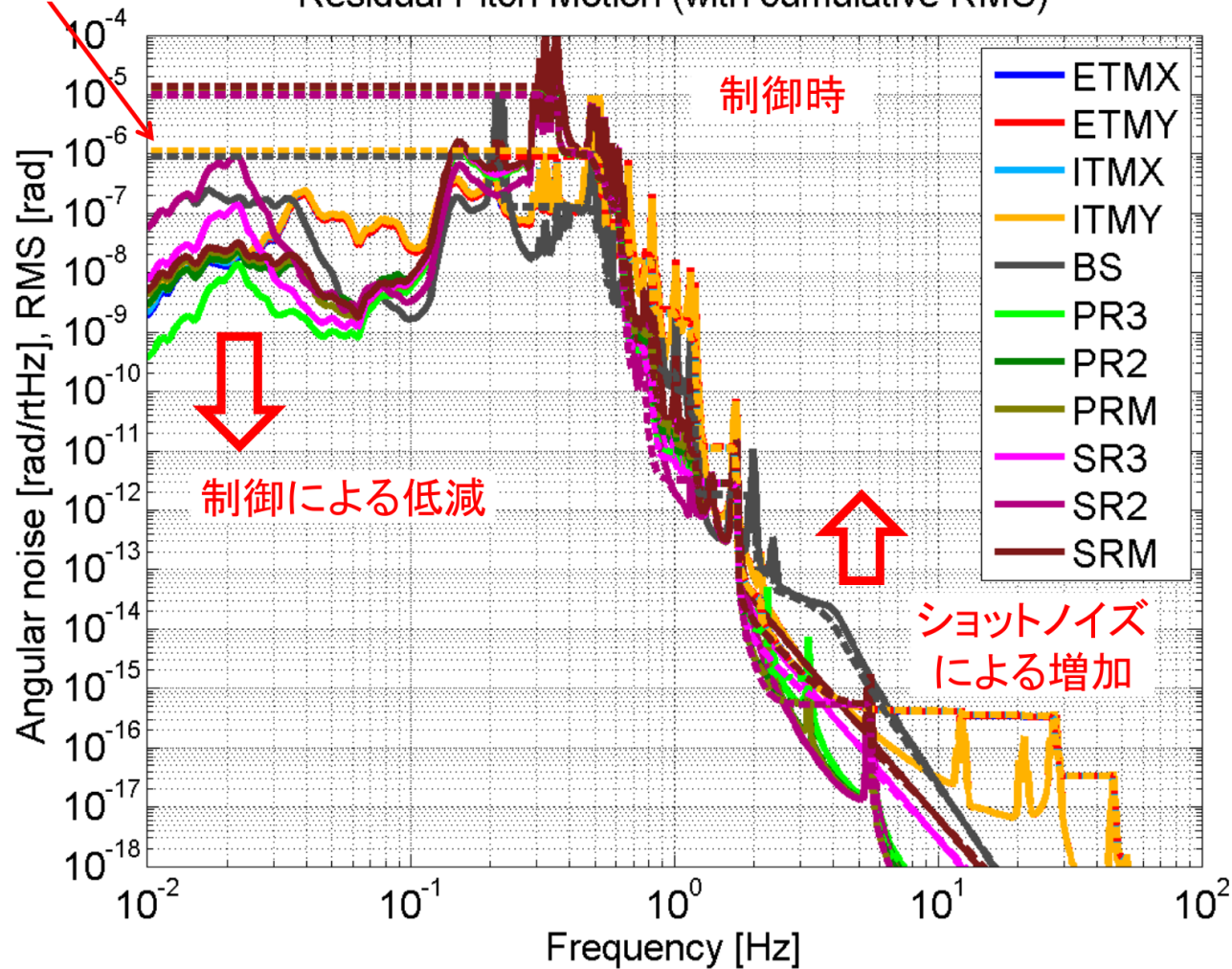


干渉計ミラーの傾きRMS 10^{-8} rad

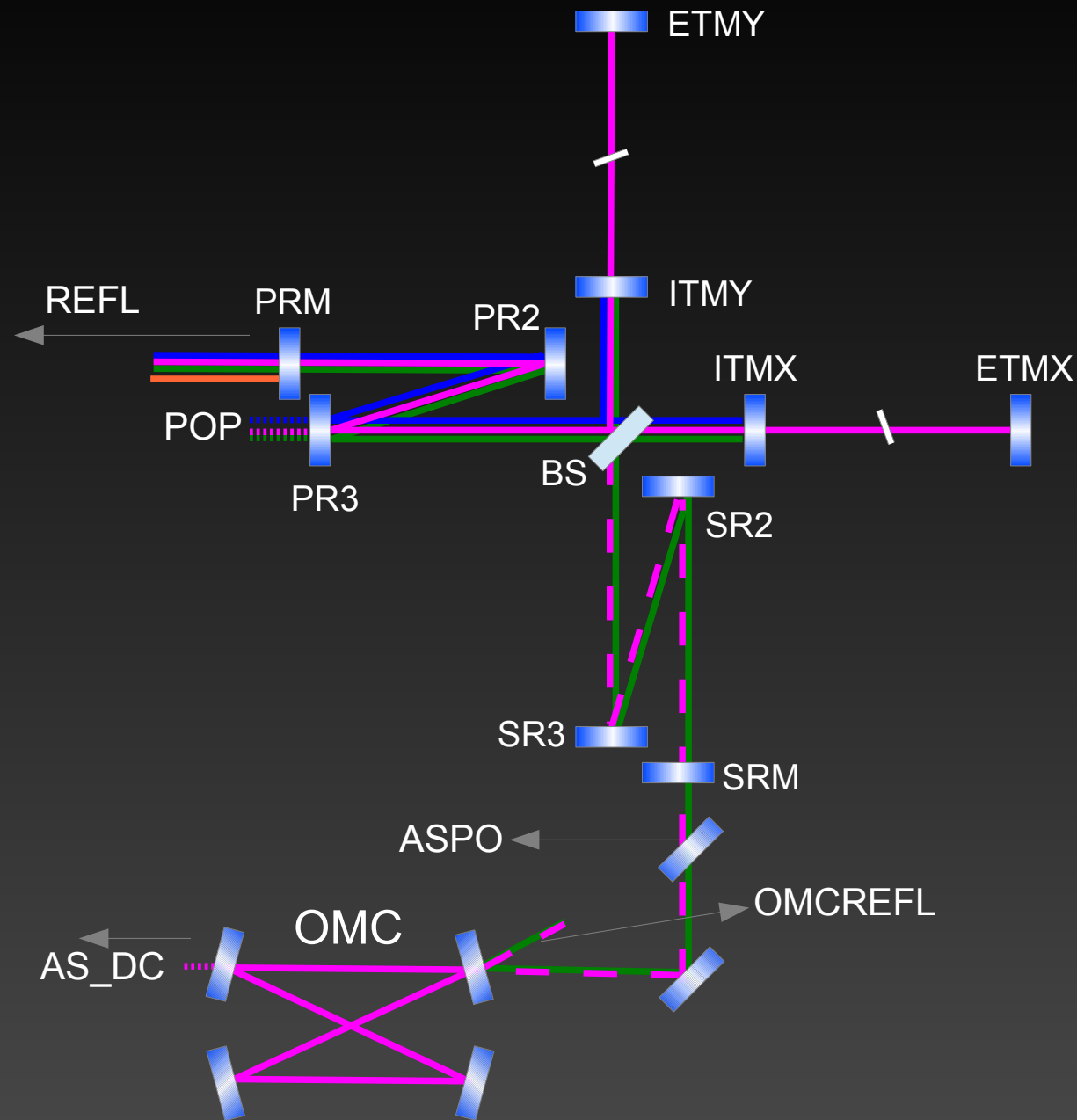
3. 残留角度揺れを計算

Residual Pitch Motion (with cumulative RMS)

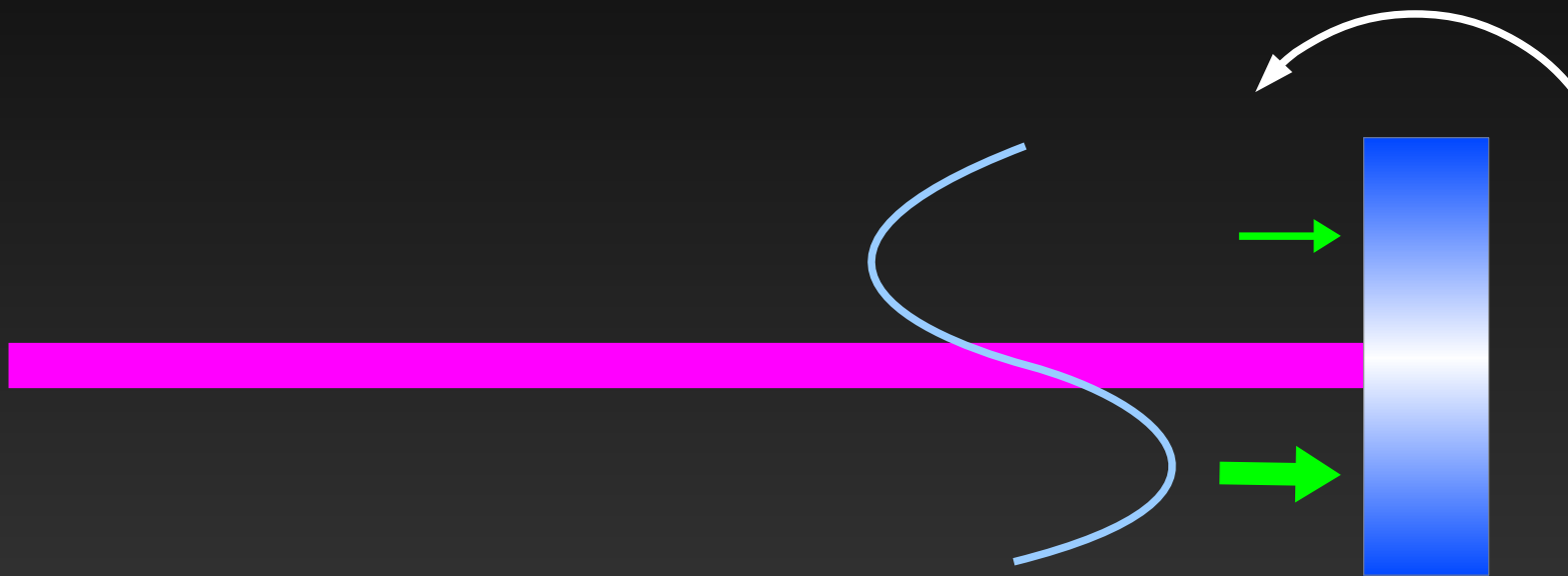
TMのRMS
~1 urad



RF SBはまだ考慮していない



輻射压效果



結論

主干涉計サスペンションの回転防振が重要

$$\text{RMS} < 10^{-8} \text{ rad}$$