

2012/02/04 KAGRA F2F MEETING

JGW-G1200859



# **Suspension Thermal Noise of a Non-Uniform Fiber**

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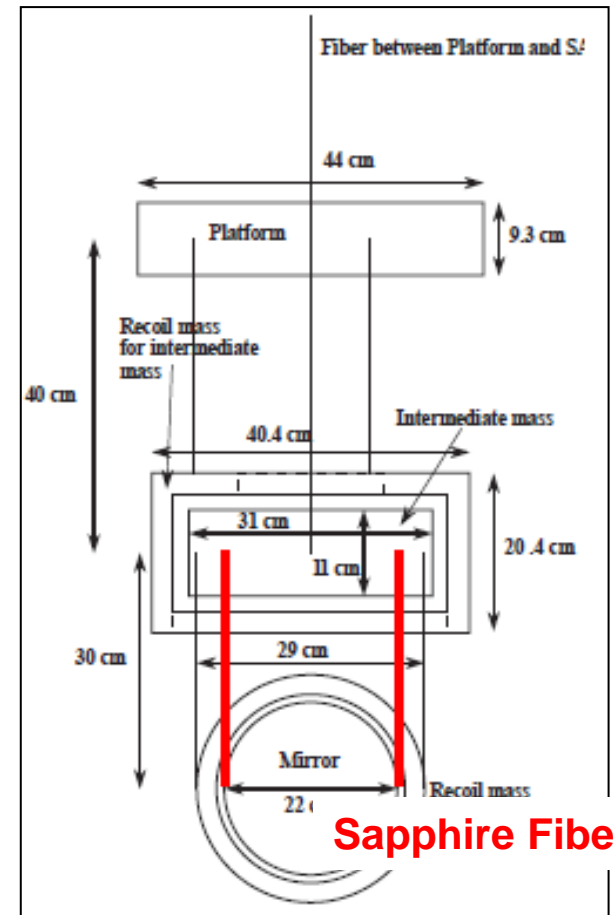


# Sapphire Fibers for **KAGRA**

- **Short** and **thick** sapphire fibers to transfer enough amount of heat ( $\sim 1$  W)
- Current Parameters:  
 **$\Phi 1.6$  mm, L30 cm**
- Problems of thick & short fibers:
  - ◆ Low dilution factor and large thermal noise
  - ◆ High resonant frequency of vertical mode
  - ◆ Heavy violin modes

Degrade the sensitivity @  $\sim 100$  Hz

## Cryogenic Payload for KAGRA

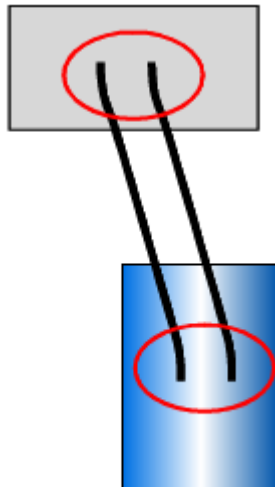


**Sapphire Fibers**

# Non-Uniform Fiber



- **Thin** fiber at both ends to lower the suspension thermal noise.
- **Thick** fiber in the middle to obtain large thermal transmissivity.

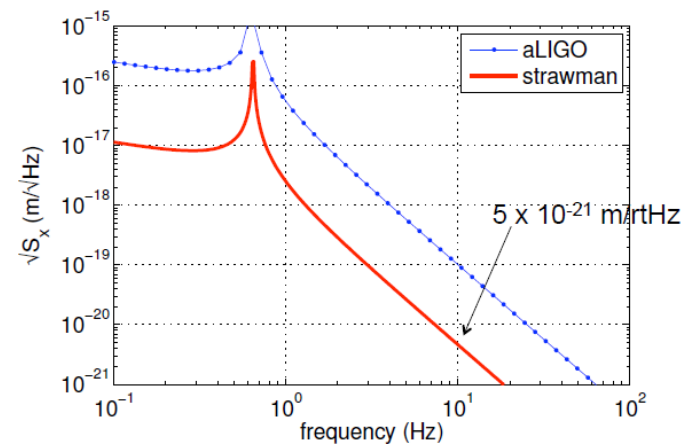
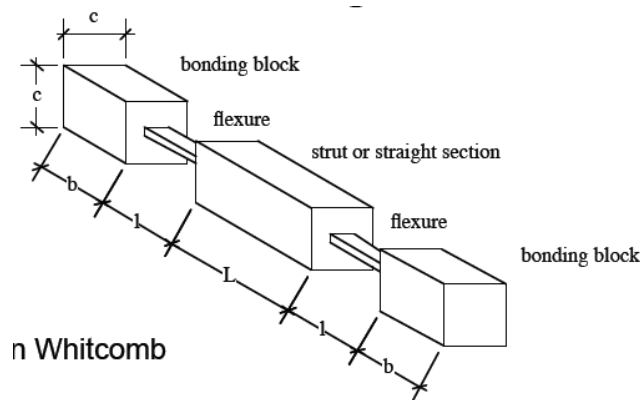


$U_e$ : Potential energy stored in the bending of fibers  
 $U_g$ : Gravitational potential energy (lossless)

$$\phi_{\text{pendulum}} = \phi_{\text{fiber}} \times \frac{U_e}{U_g + U_e}$$

# About This Work

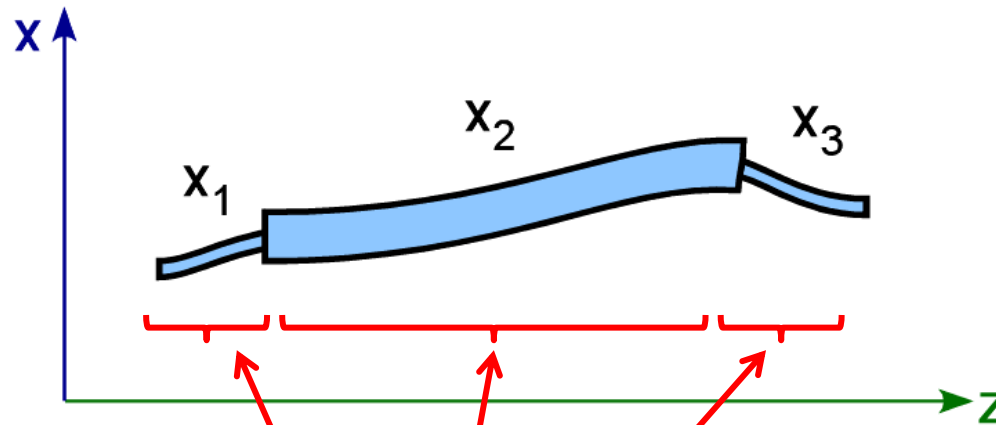
- “Flexure + Strut” fiber was suggested by Warren Johnson.  
**[W. Johnson, KAGRA Collaboration Meeting, Nov. 8th, 2011]**



- We have not known its suspension thermal noise **at high frequencies** (>100 Hz), including the **violin modes** and the **vertical modes**.

# Model & Calculation Method

- Analytical model in the frequency domain.
- 12 coefficients (A1~D3) must be calculated from boundary conditions.



## Beam Profile

$$x_n(z) = A_n \cos(k_n z) + B_n \sin(k_n z) + C_n \exp(k_{e,n} z) + D_n \exp(-k_{e,n} z) \quad (n = 1, 2, 3)$$

# Boundary Conditions

Phil Willems, Physics Letters A 300 (2002) 162–168

- The displacement and gradient are 0 at the top of the fiber.

$$\begin{aligned} x_1 &= 0, \\ x_1' &= 0 \end{aligned} \quad (\text{at } z = 0)$$

- Two beam profiles are smoothly connected at the boundary.

Continuous displacement  $x_1 = x_2,$

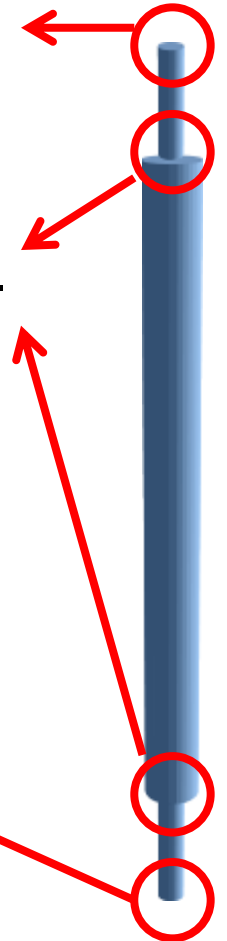
Continuous gradient  $x_1' = x_2',$  (at  $z = L_e$ )

Equilibrium of moment  $I_1 x_1'' = I_2 x_2''$

Equilibrium of force  $EI_1 x_1''' - Tx_1' = EI_2 x_2''' - Tx_2'$

- Equation of motion about the suspended mirror.

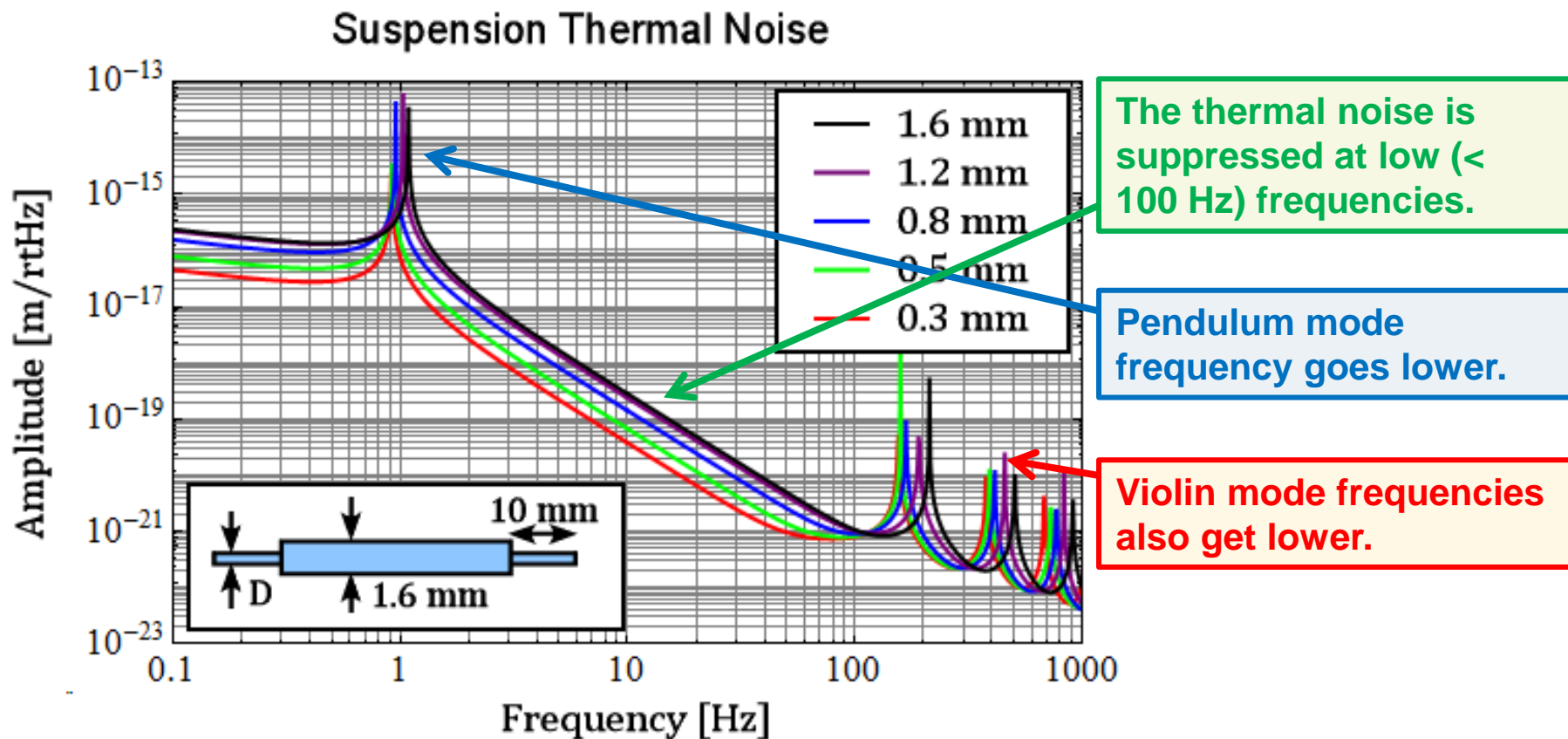
$$\begin{aligned} x_3' &= 0, \\ EI_1 x_3''' - Tx_3' + M_{\text{TM}} \omega^2 x_3 &= -\tilde{F} \end{aligned} \quad (\text{at } z = L)$$



# Calculation Result (1)

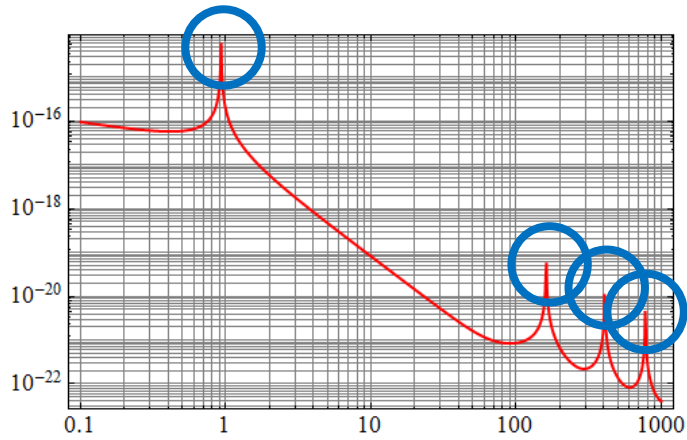


- Decreasing the fiber thickness in the first 1 cm.

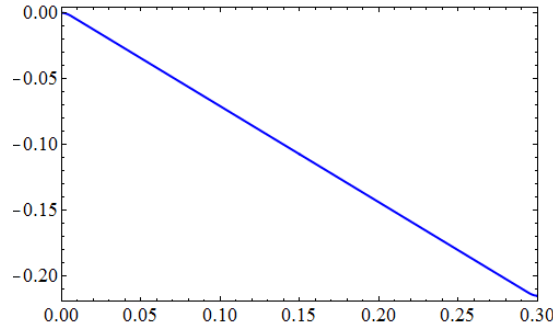




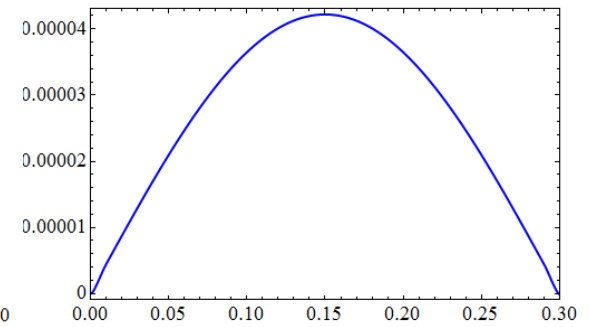
# Mode Shape (Beam Profile)



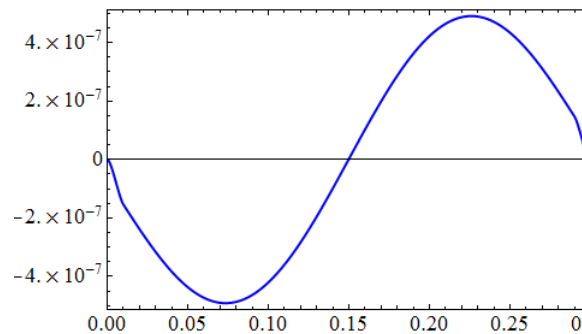
Pendulum Mode



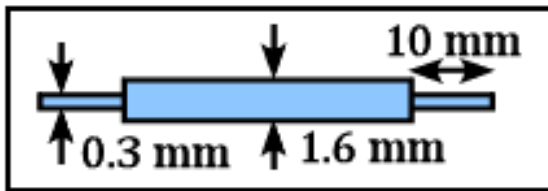
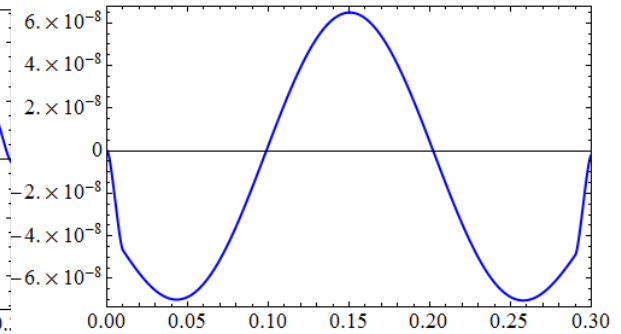
1st Violin Mode



2nd Violin Mode



3rd Violin Mode



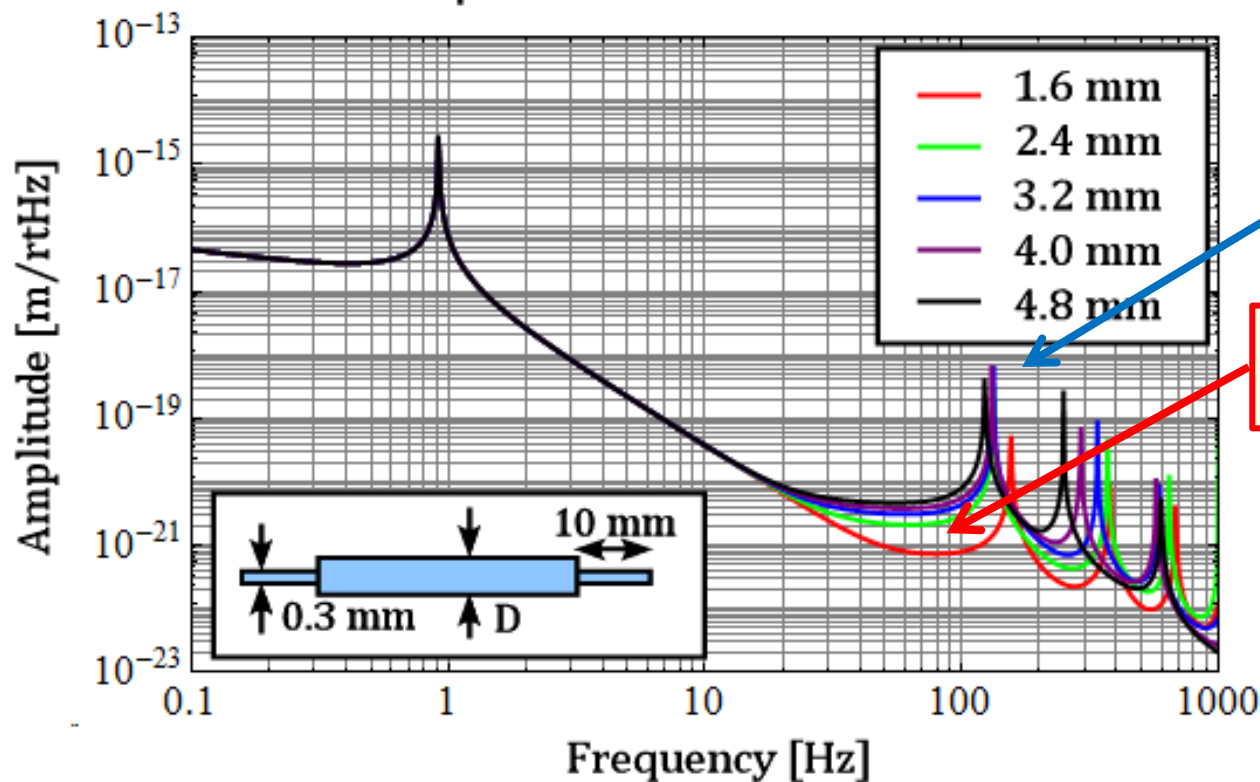


# Calculation Result (2)



- Increasing the thickness in the middle

### Suspension Thermal Noise



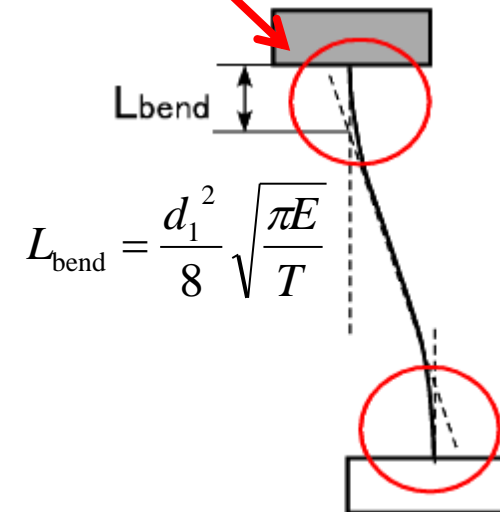
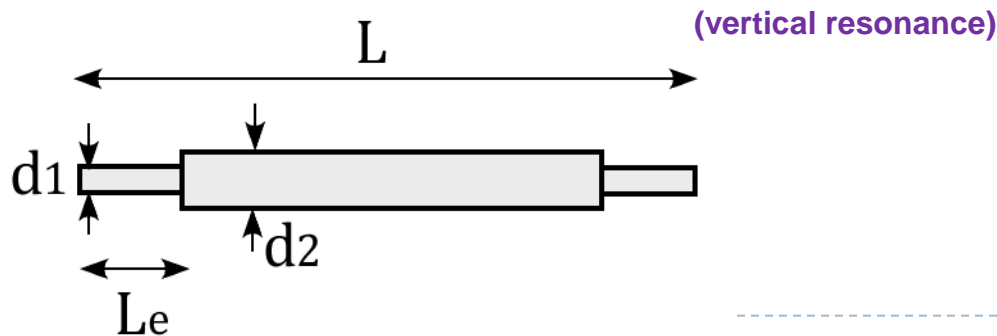
Violin mode frequencies get even lower.

Floor level around 100 Hz increases!!

# Parameters for KAGRA

1. Decrease the wire thickness in the ends.
2. Make the thin part long enough to cover **the bending part** of the fiber.
3. Increase the wire thickness in the middle to keep the heat transmissivity.  
(taking into account the size effect of the thermal conductivity)

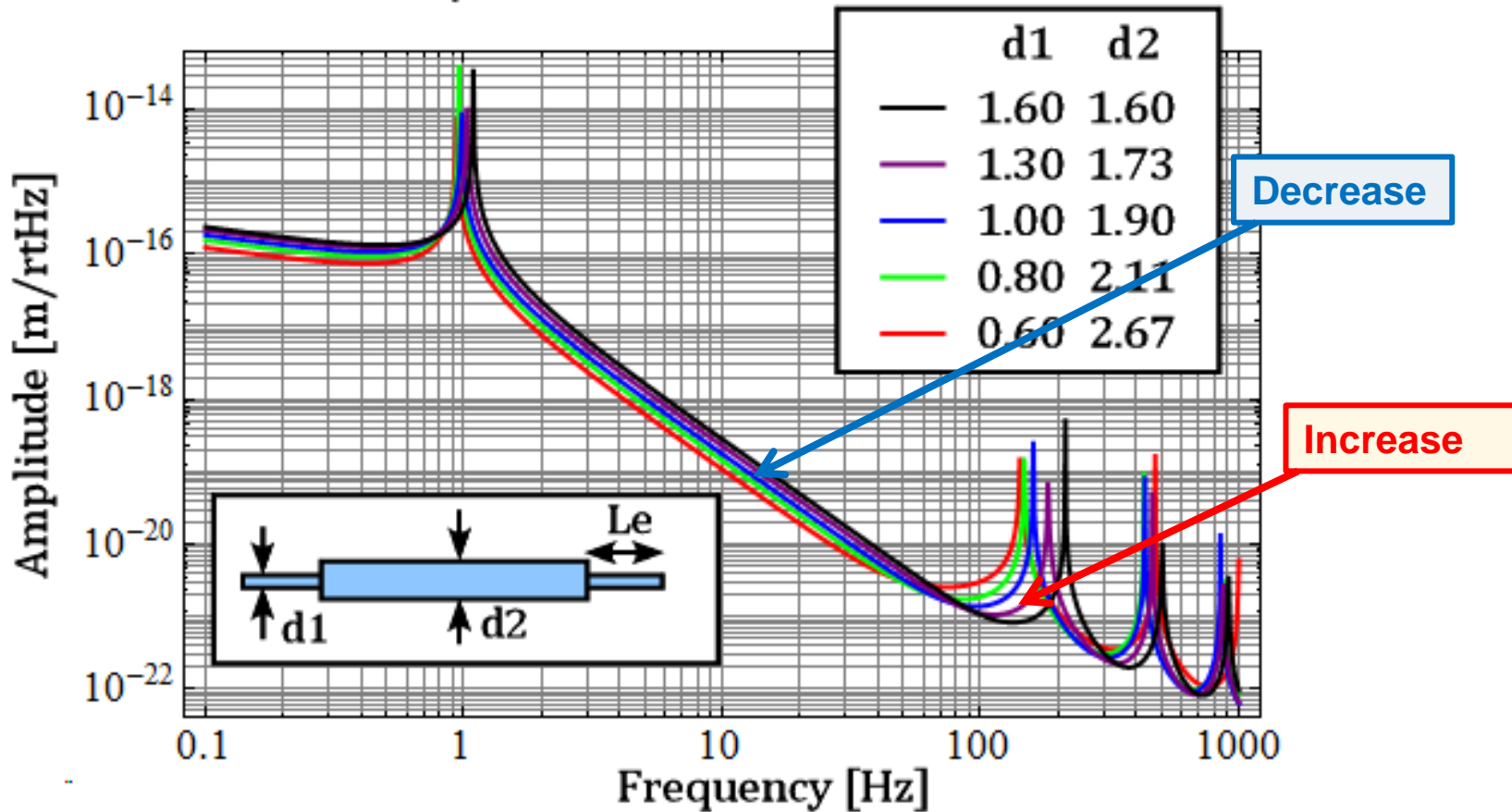
d1 [mm]	d2 [mm]	Le [mm]	f [Hz]
0.60	2.67	6.3	127
0.80	2.11	11.2	111
1.00	1.90	17.4	106
1.30	1.73	29.5	102
1.60	1.60	44.7	102



# Calculation Result (3)



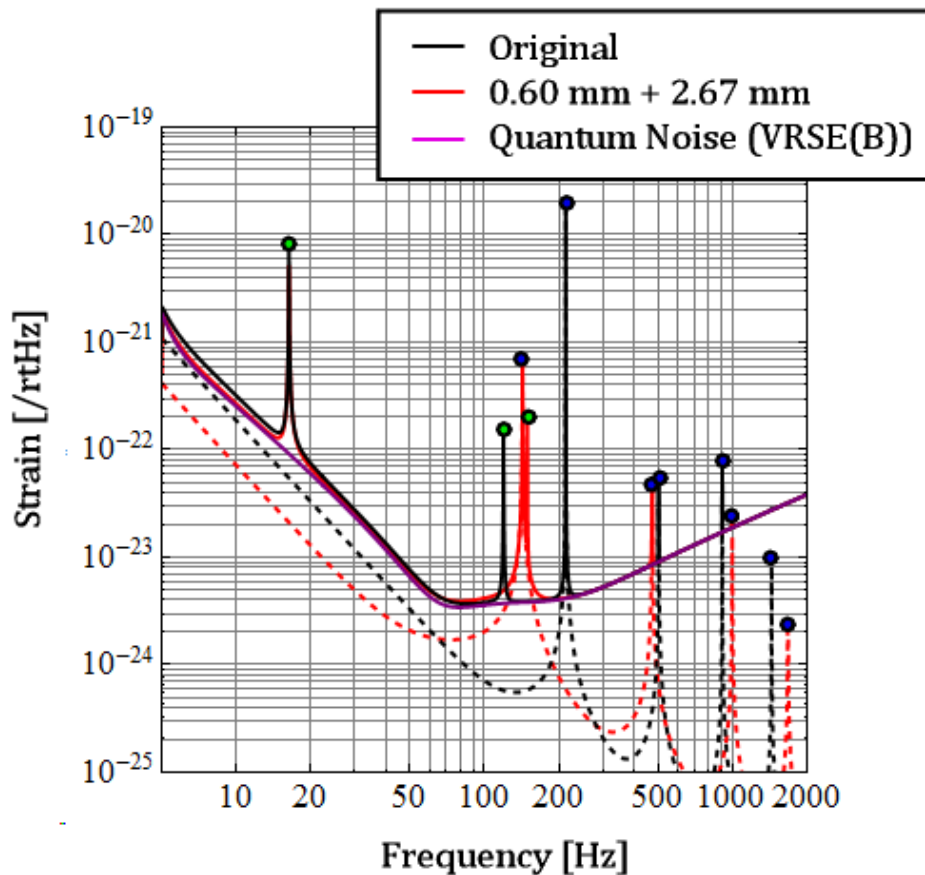
### Suspension Thermal Noise



# Total Sensitivity



- Including **vertical thermal noise** and **quantum noise**



- **Vertical Mode**
- **Violin Mode**

<50 Hz:

Thermal noise decreases, but the sensitivity is not improved.  
(due to the existence of the quantum noise)

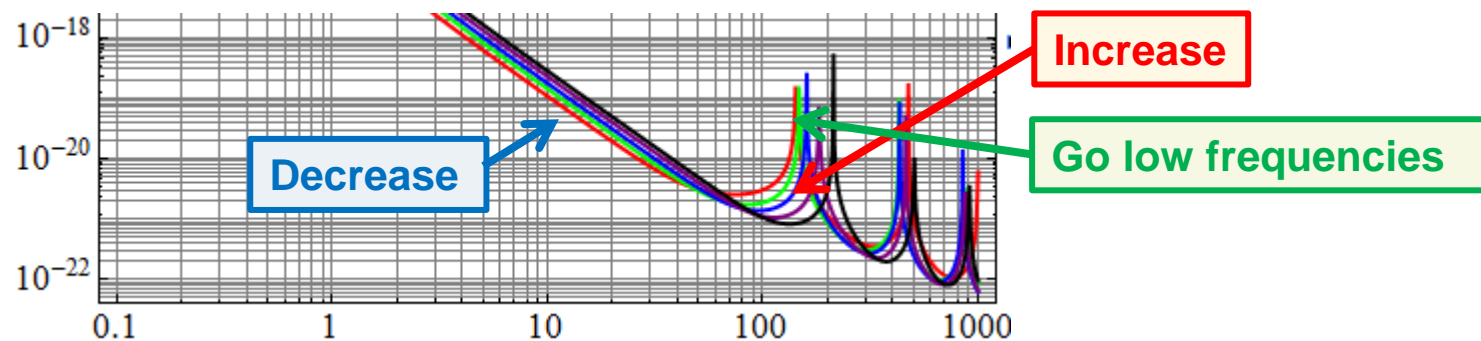
>50 Hz:

In both cases, the sensitivity around 100 Hz is degraded by the violin and the vertical mode resonances.

# Conclusion



- There is a **trade-off** of using non-uniform fibers :
  - ◆ The suspension thermal noise at low frequencies (<50 Hz) decreases, by the “dissipation dilution” effect.
  - ◆ However, the suspension thermal noise at high frequencies (~100 Hz) increases and the resonant frequencies of the violin modes get lower.



- Resonances of the violin modes and vertical mode still remain at ~100 Hz.



END





# Appendix

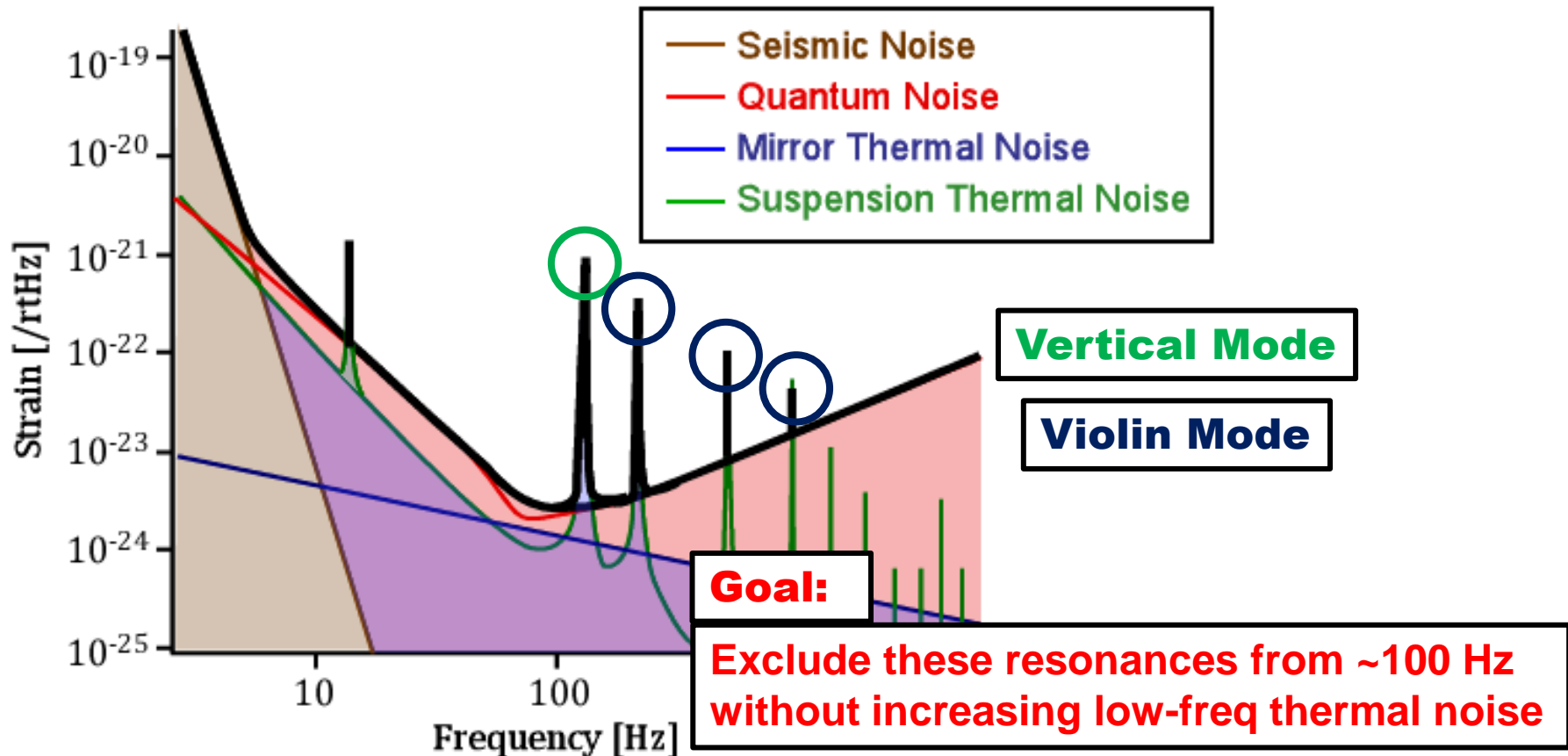


# KAGRA Sensitivity

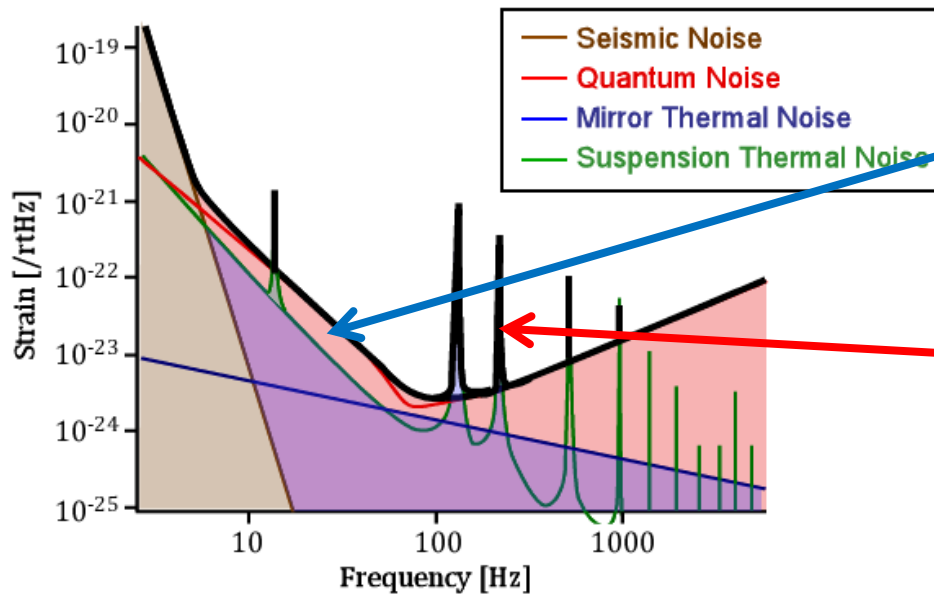


- \* 1/300 Coupling from vertical noise
- \* Loss angle of the sapphire fiber:  $2 \times 10^{-7}$
- \* Quantum Noise: VRSE (Detuned)

Sapphire Fibers ( $\Phi 1.6$  mm, L30 cm)



# Dumbbell Fiber



The sensitivity is not dominated by the thermal noise at  $< 50$  Hz

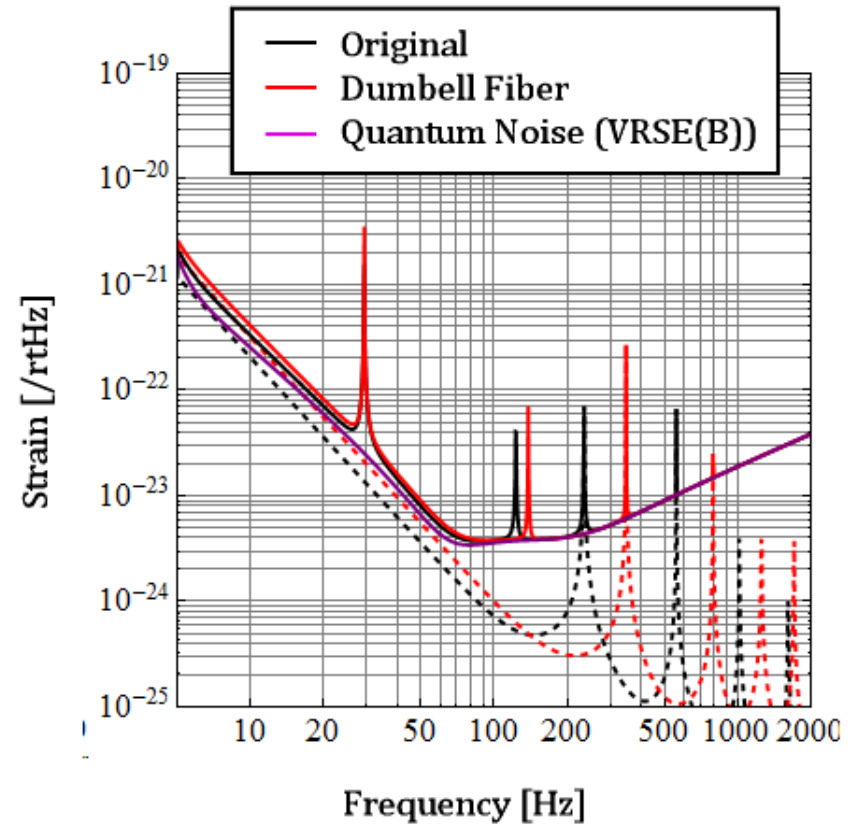
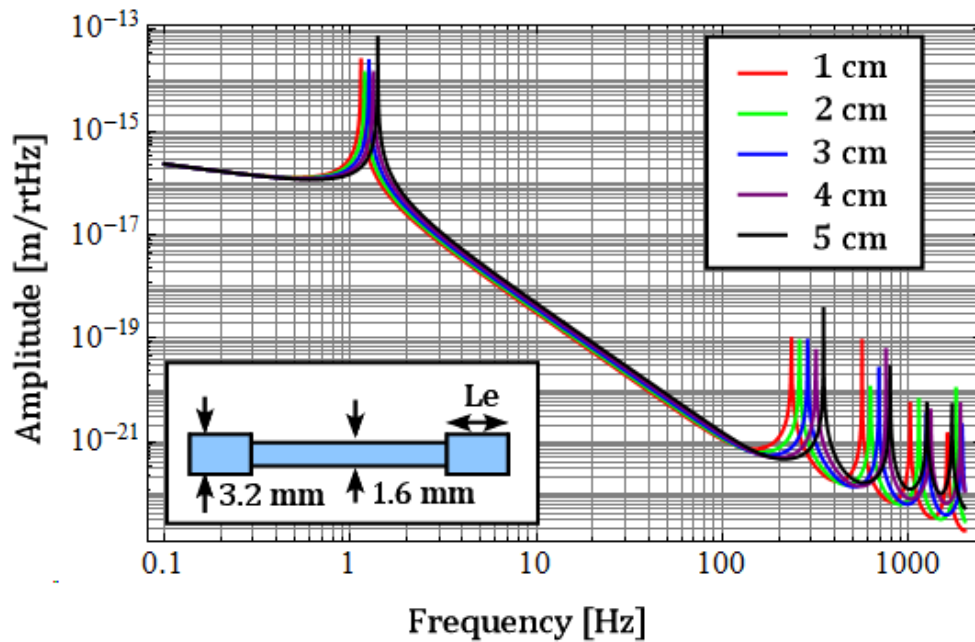
We want to exclude these resonances away from  $\sim 100$  Hz

- Reverse idea: **dumbbell fibers**

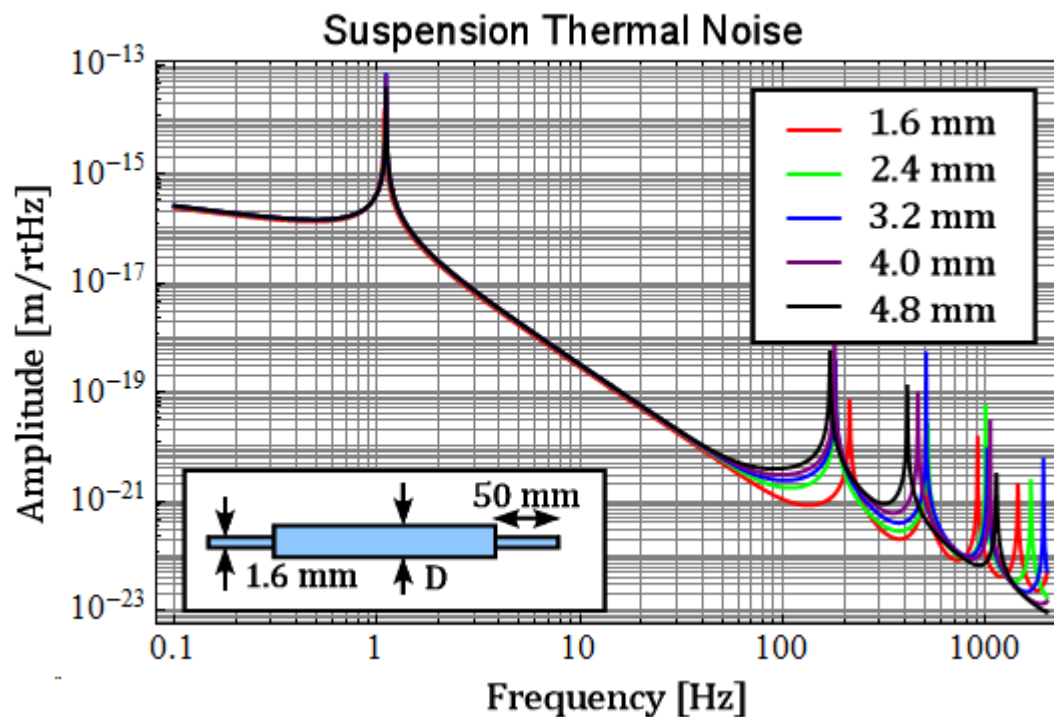


(Just making the effective length of the wire short ...)

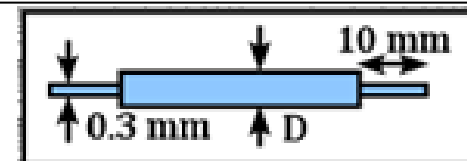
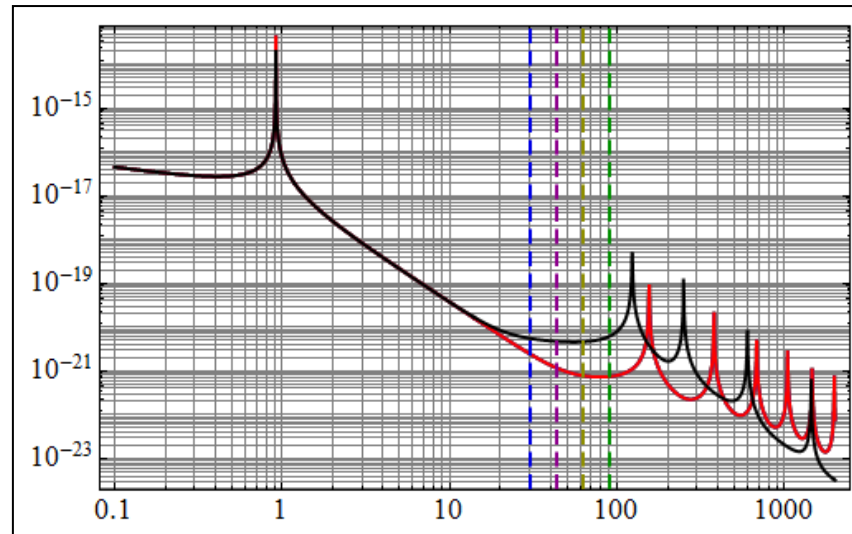
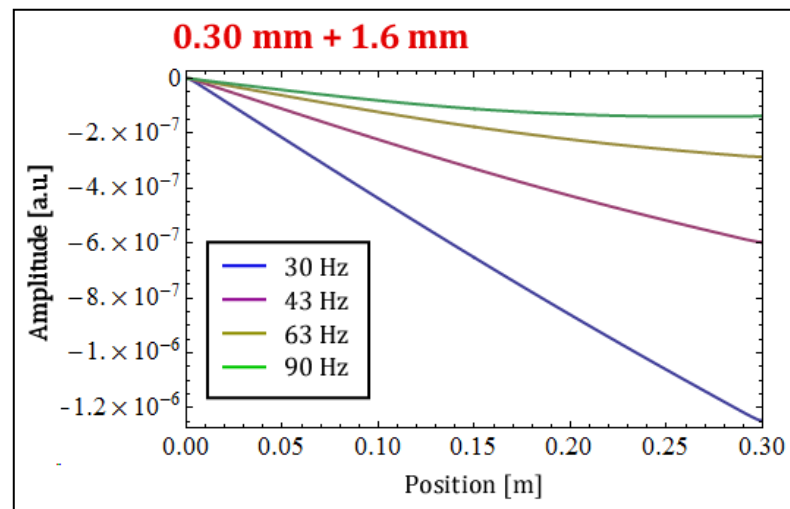
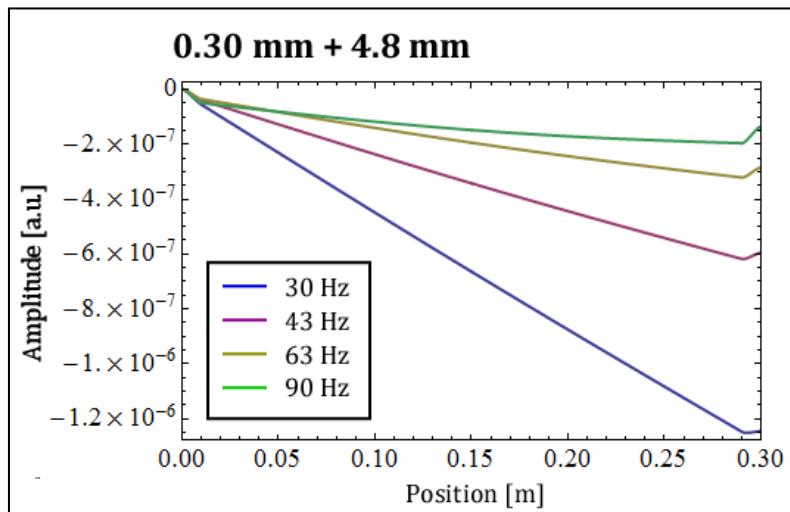
# Dumbbell Fiber Results



# Increasing Middle Thickness



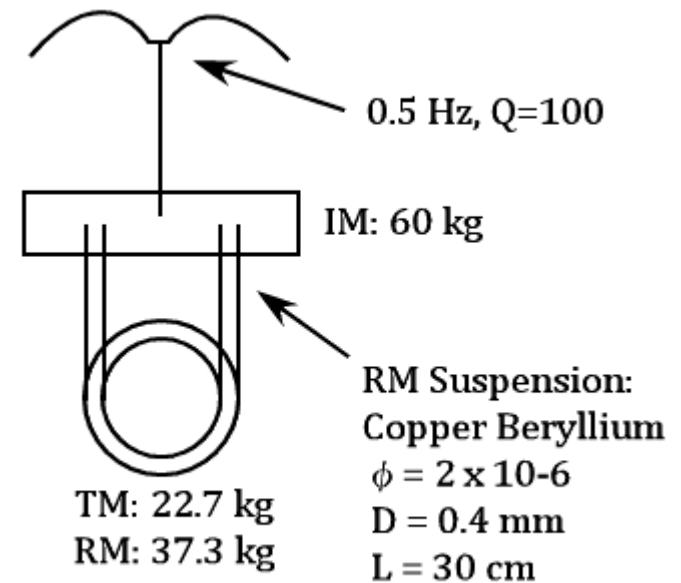
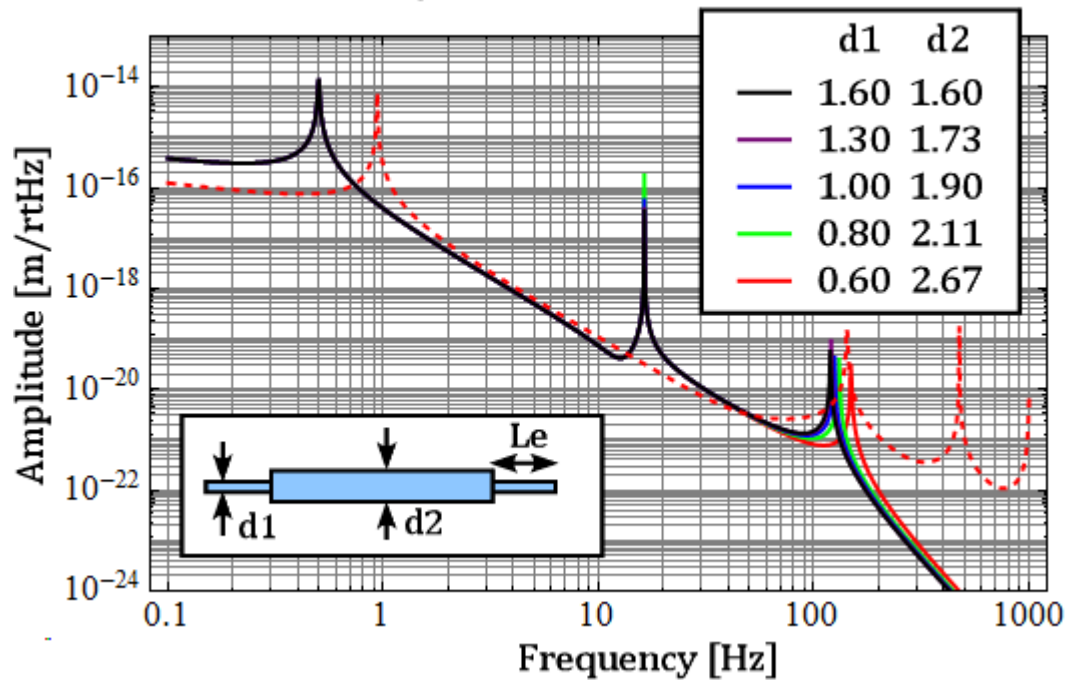
# Beam Profile



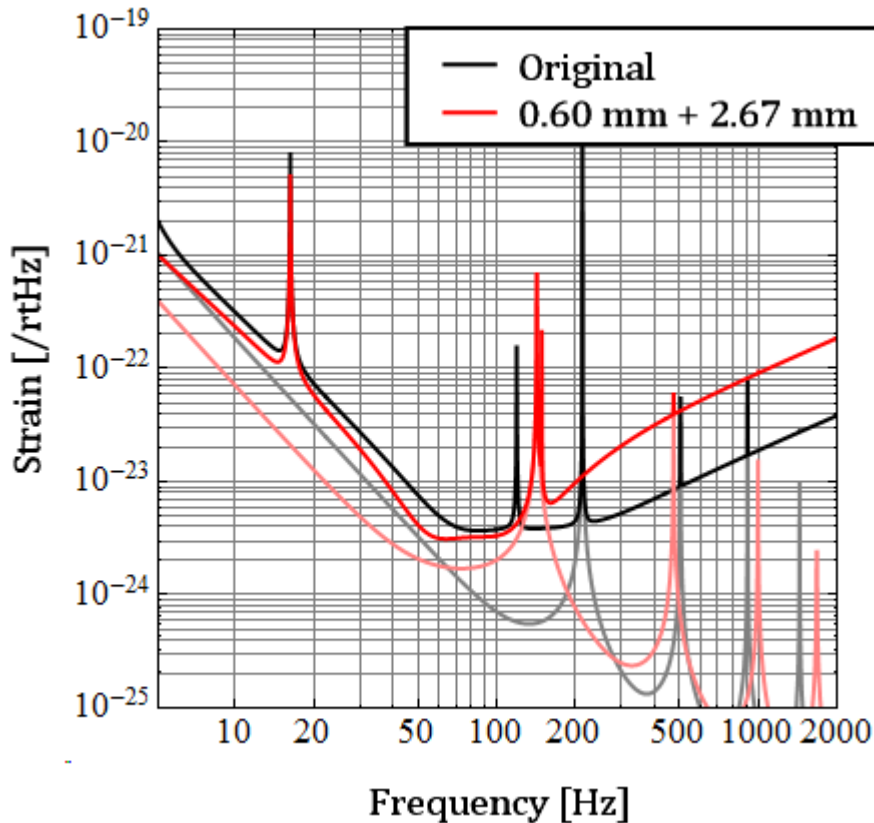
# Vertical Thermal Noise



Suspension Thermal Noise



# Optimize Quantum Noise



Laser Power  $\rightarrow$  1/2  
Finesse  $\rightarrow$  2/3

IR: 248 Mpc  $\rightarrow$  257 Mpc