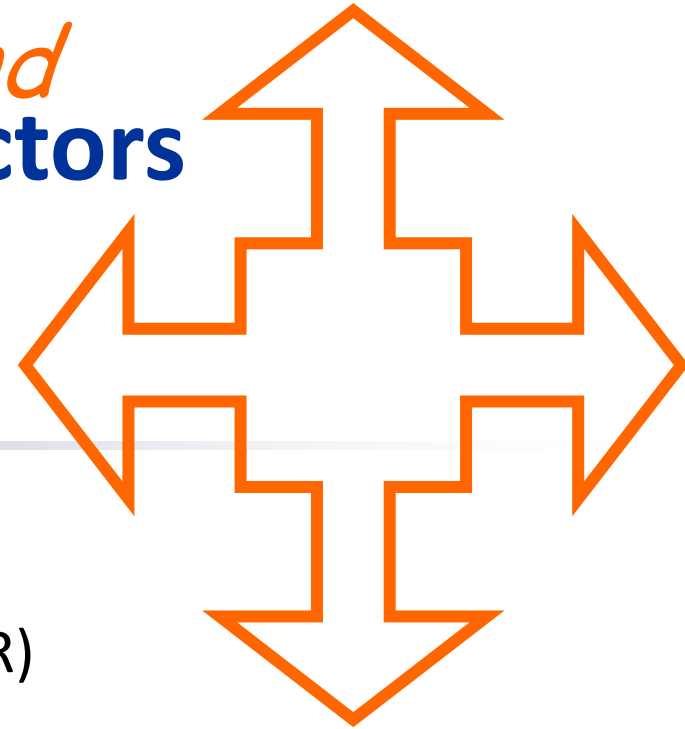
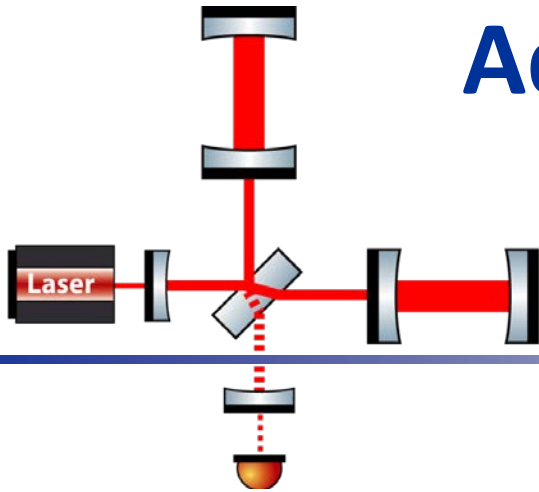


# Diffractive Optics for *Beyond* Advanced Detectors



Daniel Friedrich (ICRR)

f2f meeting  
4th of Feb. 2012

# Hannover, Germany → 東京, 日本



- Since Nov. 2011:  
JSPS research fellow  
with Prof. Kawamura



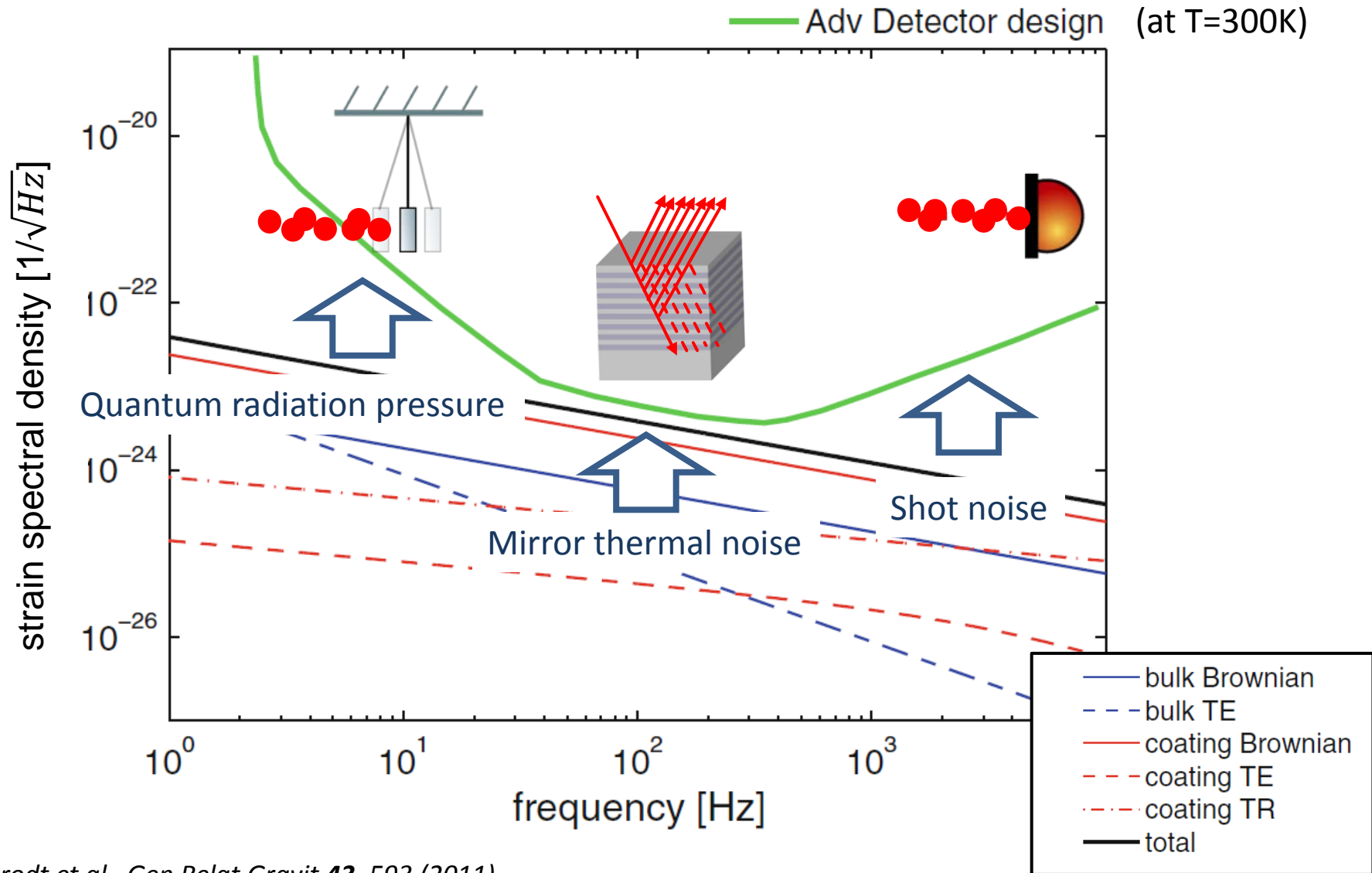
- Nov. 2011:  
PhD thesis



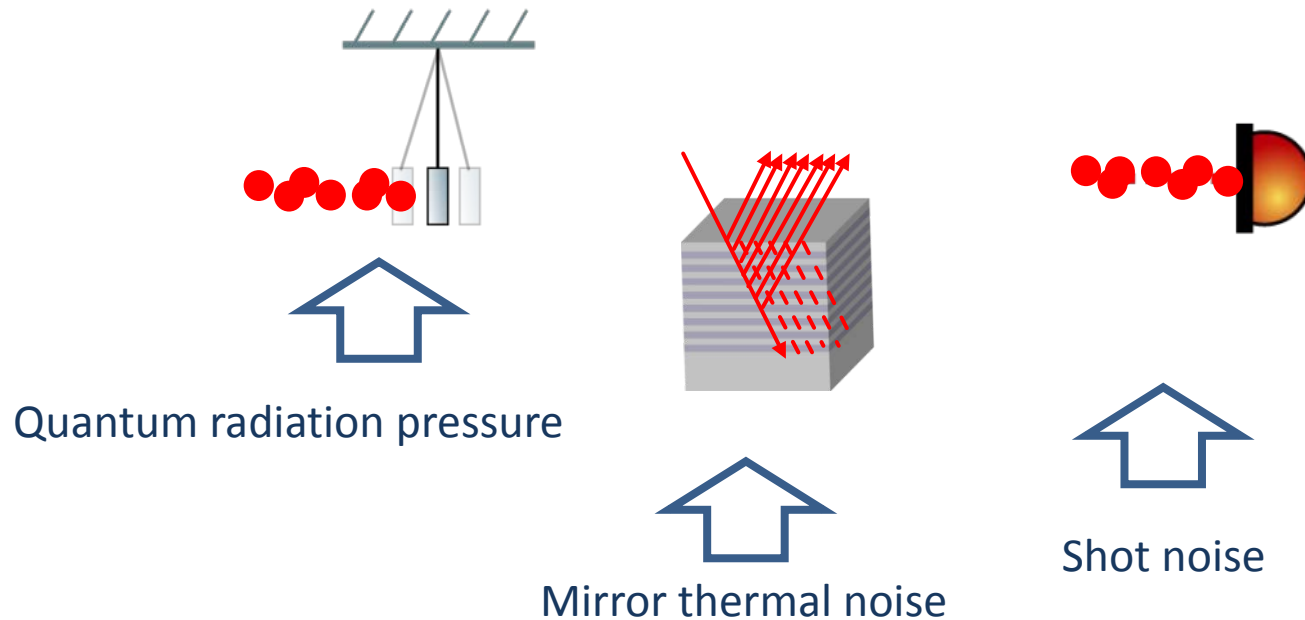
Albert-Einstein-Institut  
Hannover

*“Laser interferometry with coating-free mirrors”*

# 3 Main Noise Sources



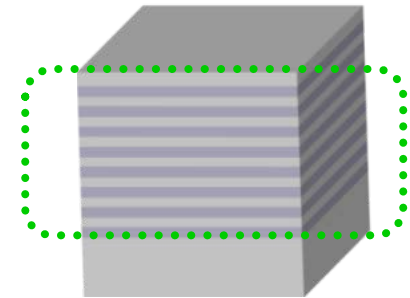
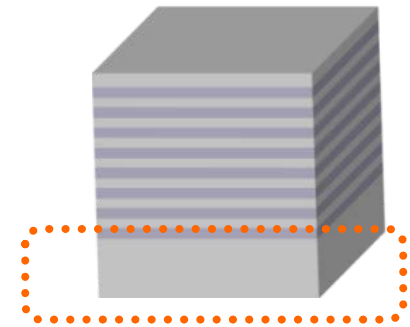
# High Quality Optics



- Core optics must
  - ... be highly transparent
  - ... have low mechanical loss
  - ... be available in large sizes

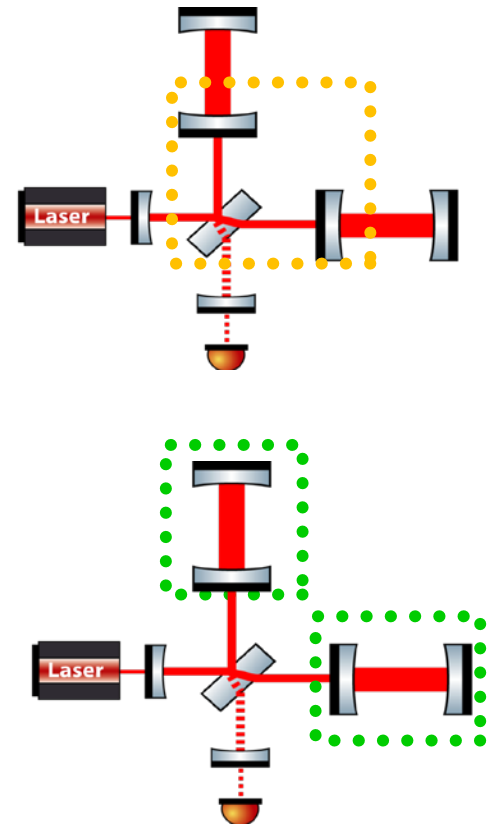
## Outline of this talk

- All-reflective interferometry
  - Avoid transmission through substrates
  - Reflection gratings
- Coating free mirrors
  - Avoid mechanical lossy multilayer coatings
  - Waveguide gratings
- Outlook/Summary



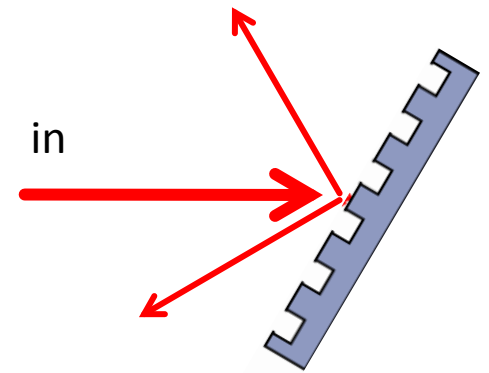
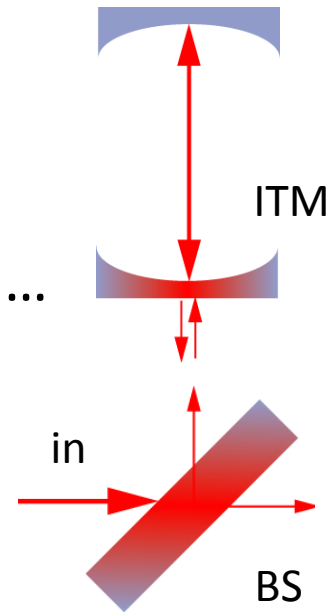
## Outline of this talk

- All-reflective interferometry
  - Avoid transmission through substrates
  - Reflection gratings as BS or ITMs
- Coating free mirrors
  - Avoid mechanical lossy multilayer coatings
  - Waveguide gratings as ITMs and ETMs
- Outlook/Summary



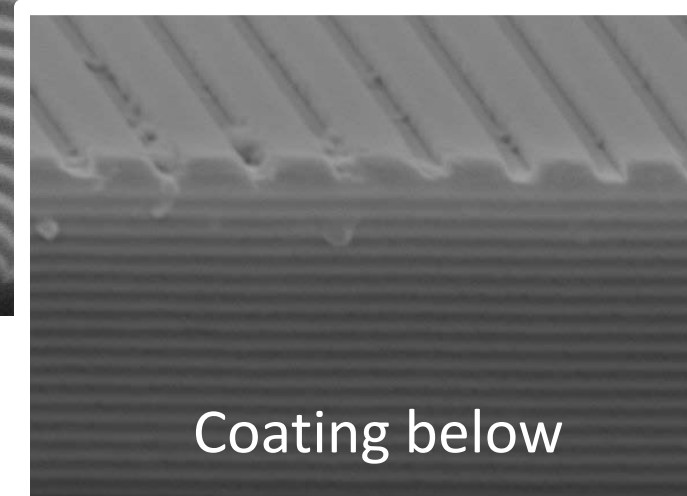
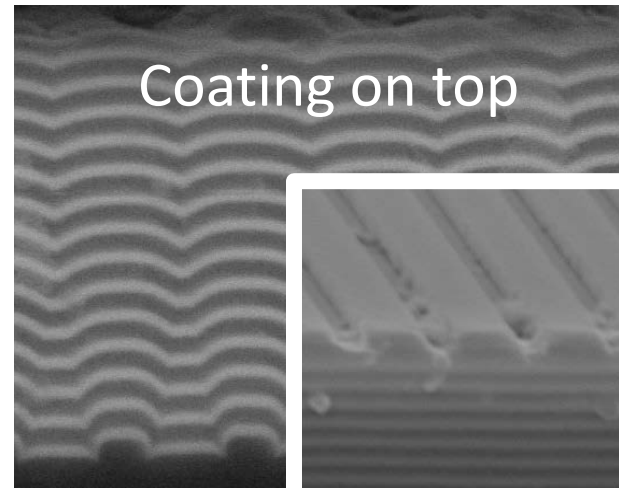
# All-reflective interferometry

- Transmission through substrates
  - Optical absorption / heating / thermorefractive noise, ...
  - Substrates must be highly transparent
  - Substrates must have low mechanical loss
- Reflection gratings
  - Allow for opaque substrate materials (e.g. Si @ 1064nm)



# Dielectric Reflection Gratings

- Multilayer coating
  - High reflectivity
- Grating structure
  - Diffraction → beam splitting

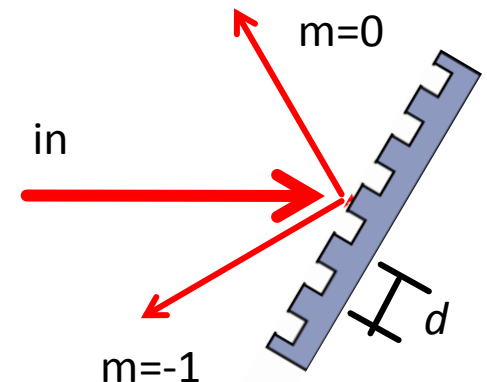


- Existence and direction of diffraction orders  $m$

$$n_b \sin(\beta_m) = n_a \sin(\alpha) + \frac{m\lambda}{d}$$

- Design via rigorous methods (RCWA)

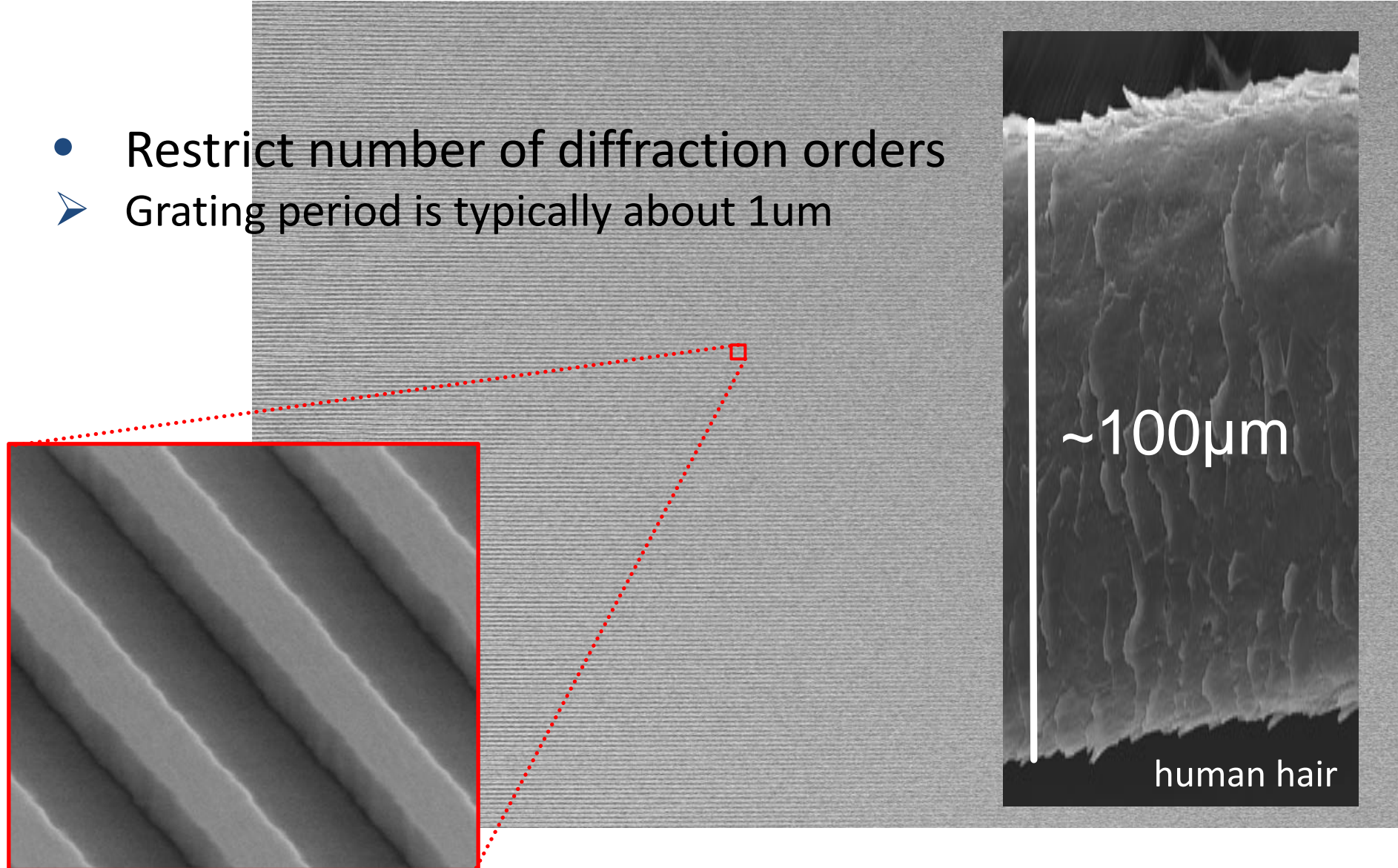
*M.G. Moharam et al. J. Opt. Soc. Am. 71 (1981)*





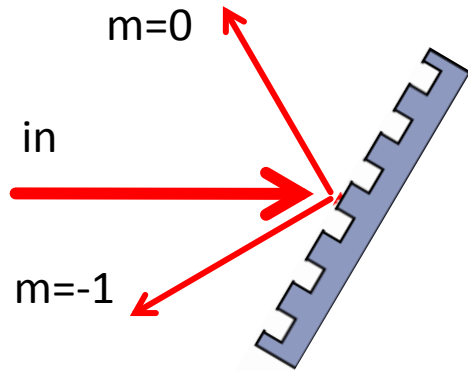
# Grating Dimension

- Restrict number of diffraction orders
- Grating period is typically about 1 $\mu$ m



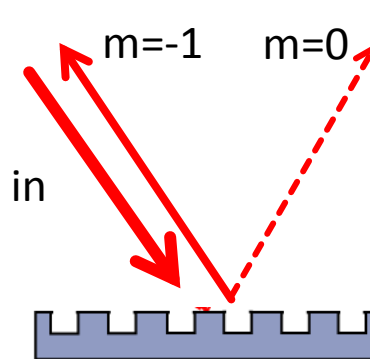
# Various concepts

- 50/50 beam splitter

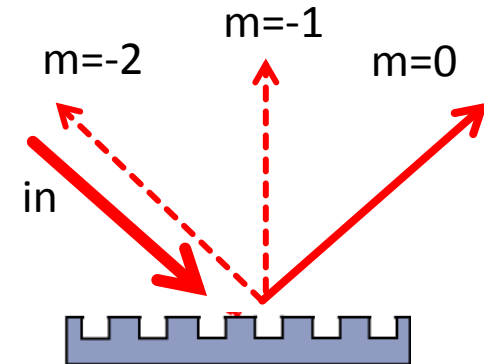


S.Fahr *et al.*, *Appl.Opt.* **46**, 6092 (2007)

- 1st/2nd order Littrow gratings



L.Li *et al.*, *Opt.Lett.* **20**, 1349 (1995)



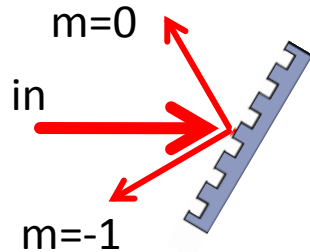
A.Bunkowski *et al.*,  
*Opt.Lett.* **30**, 1183 (2005)

➤ Michelson ifo.

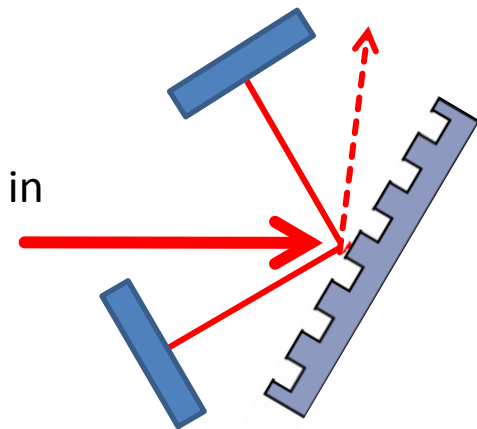
➤ Cavity coupler

# Various applications

- 50/50 beam splitter



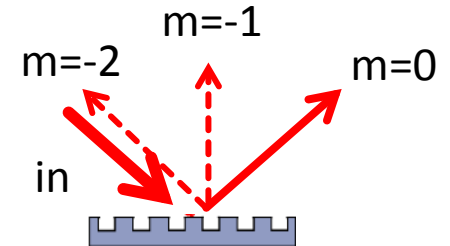
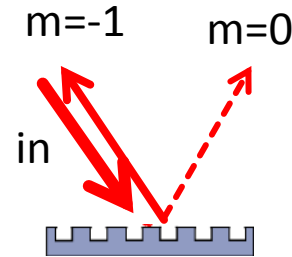
- Michelson ifo.



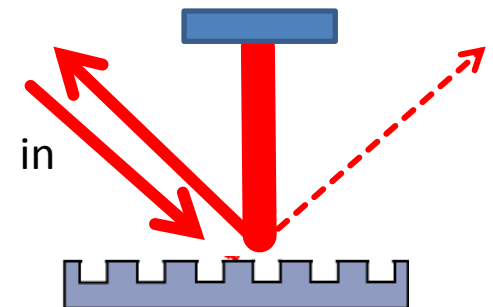
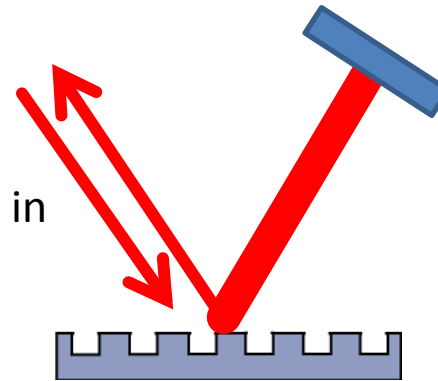
K.Sun. *et al.*, *Opt.Lett.* **23**, 567(1998)

DF. *et al.*, *Opt.Lett.* **33**, 101 (2008)

- 1st/2nd order Littrow gratings



- Cavity coupler



K.Sun. *et al.*, *Opt.Lett.* **23**, 567 (1998)

A.Bunkowski *et al.*, *Appl.Opt.* **45**, 5795 (2006)

A.Bunkowski *et al.*, *Opt.Lett.* **31**, 2384 (2006)

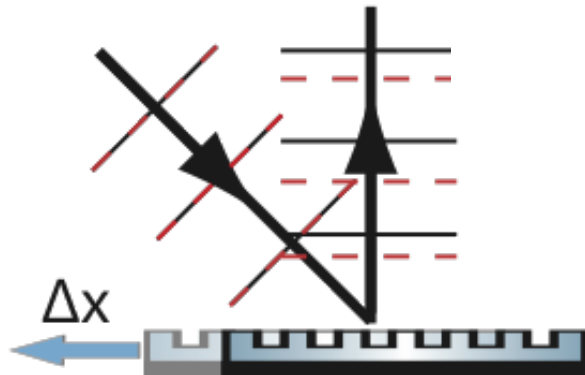
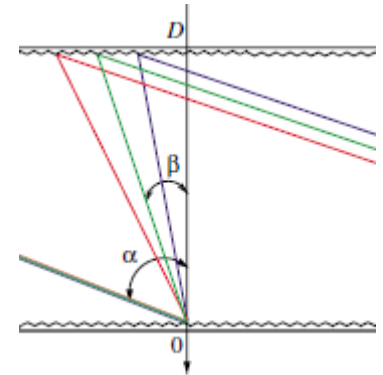
M.Edgar *et al.*, *Opt.Lett.* **34**, 3184 (2009)

M.Britzger *et al.*, *Appl.Opt.* **50**, 4340 (2011)

# The “uninvited guest”

- Lateral displacement induces phase shift

*S.Wise et al., PRL 95, 013901 (2005)*



$$\phi_m = -m \frac{\Delta x}{d} 2\pi$$

diffraction order  $\uparrow$        $\uparrow$  grating period

- Lateral displacement noise

*A.Freise et al., New Journal of Physics 9, 433 (2007)*

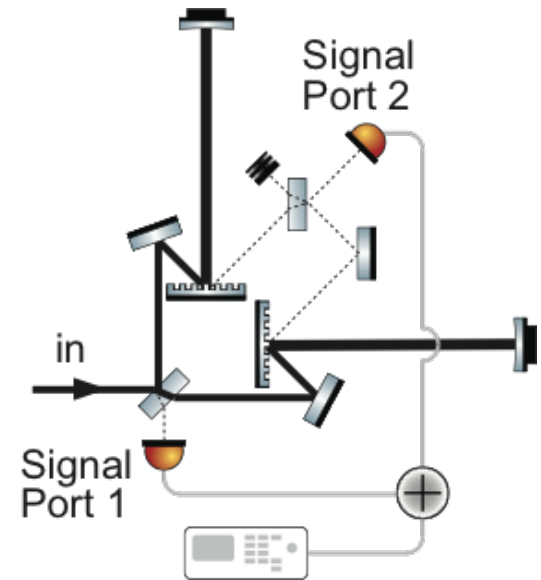
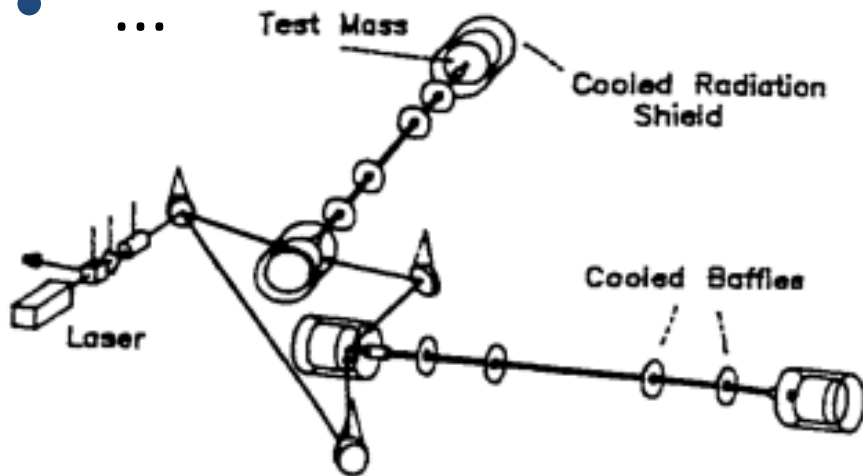
*J. Hallam et al., J. Opt. A: Pure Appl. Opt. 11, 085502 (2009)*

*B.Barr et al., Opt.Lett. 36, 2746 (2011)*

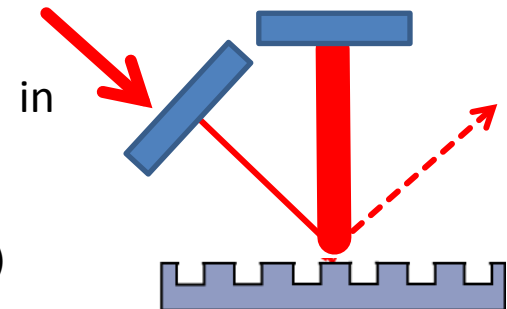
- Unsolved problem so far, but...

# New topologies

- ..., many possibilities left e.g.
- Having two signal ports →
- Add recycling mirrors ↘
- Connect the arms ↓
- ...



M.Britzger, pers.comm.



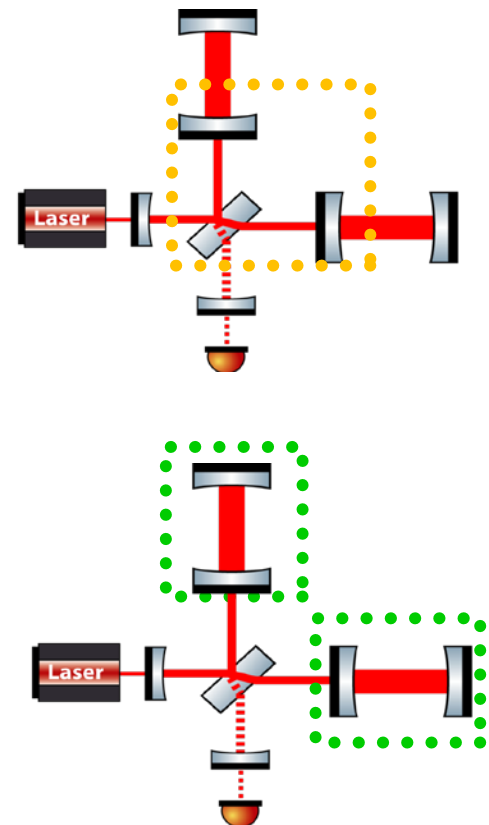
R.W.P.Drever, Proc. of the 7th Marcel Grossman Meeting on Gen.Rel. , 1401 (1995)

O.Burmeister et al., Opt.Express. **18**, 9119 (2010)

M.Britzger et al., Opt.Express **19**, 14960 (2011) 13

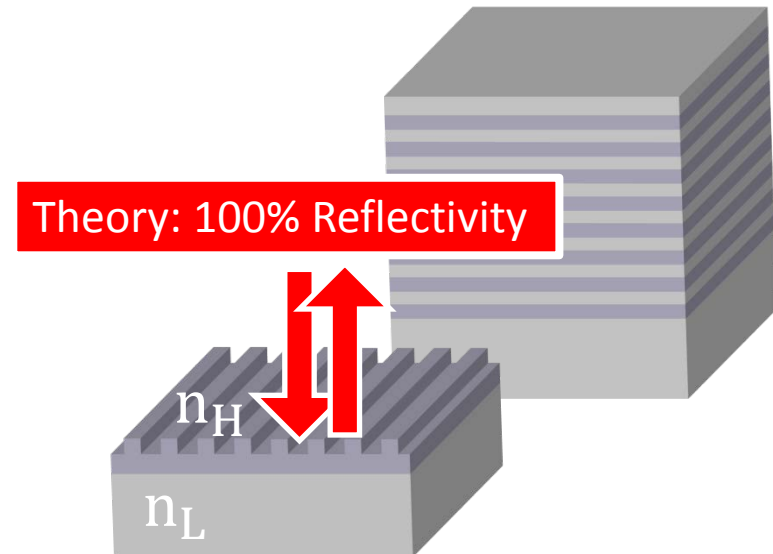
## Outline of this talk

- All-reflective interferometry
  - Avoid transmission through substrates
  - Reflection gratings as BS or ITMs
- Coating free mirrors
  - Avoid mechanical lossy multilayer coatings
  - Waveguide gratings as ITMs and ETMs
- Summary

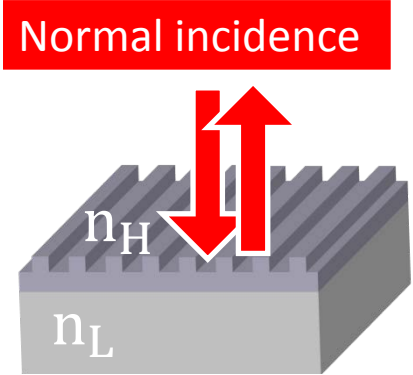
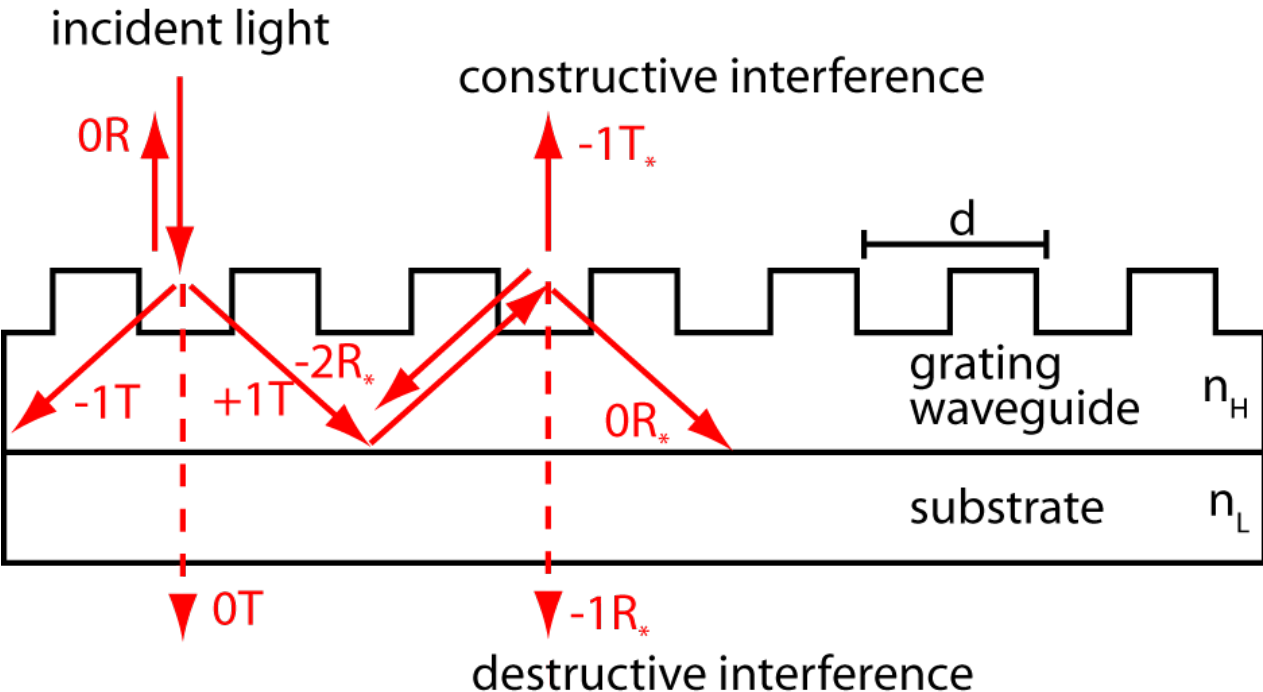


# Waveguide Gratings (WGGs)

- Motivation: Coating thermal noise
- Approach: Significant reduction of coating material
- Resonant excitation of light  
*A. Hessel et al. Appl. Opt. 4, 1275 (1965)*
- Structured surfaces
- Indices of refraction ( $n_H > n_L$ )



# Ray Picture



- Existence and direction of diffraction orders  $m$

$$n_b \sin(\beta_m) = n_a \sin(\alpha) + \frac{m\lambda}{d}$$

- Restrict diffraction orders

Only 0th order in air  $d \leq \lambda$

$\pm 1$ st orders in waveguide  $\lambda/n_H \leq d \leq 2\lambda/n_H$

Only 0th order in substrate  $d \leq \lambda/n_L$



# WGGs @ 1064nm

- Proposed as low thermal noise mirror
- Design based uses on 1st generation materials

A. Bunkowski et al., CQG 23, 7297 (2006)

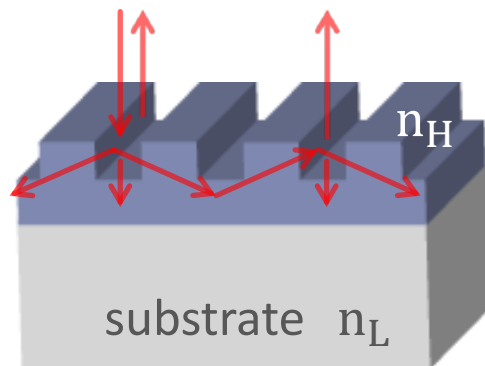
- Design via rigorous methods (RCWA)

M.G. Moharam et al. J. Opt. Soc. Am. 71 (1981)

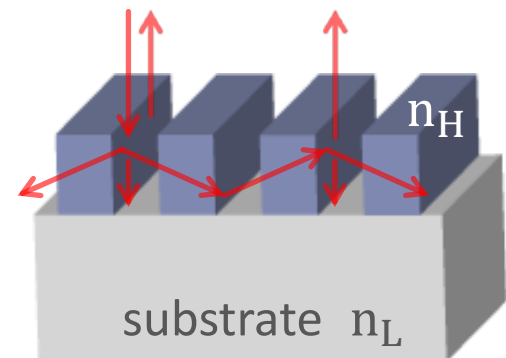
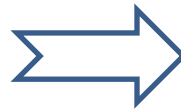
1064nm laser wavelength

Ta<sub>2</sub>O<sub>5</sub> grating ( $n_H=2.04$ )

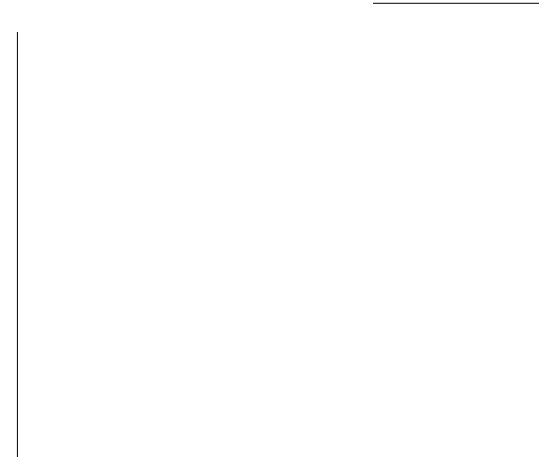
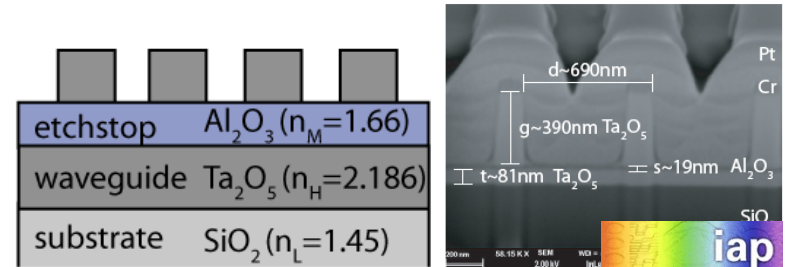
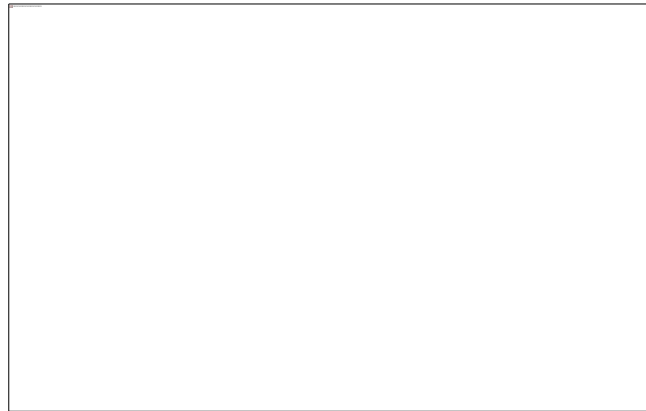
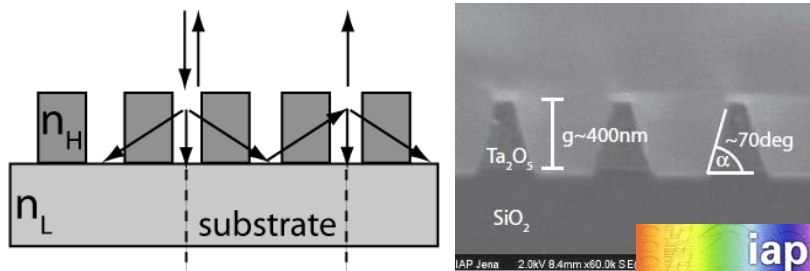
SiO<sub>2</sub> substrate ( $n_L=1.45$ )



Only ridges



# WGGs @ 1064nm



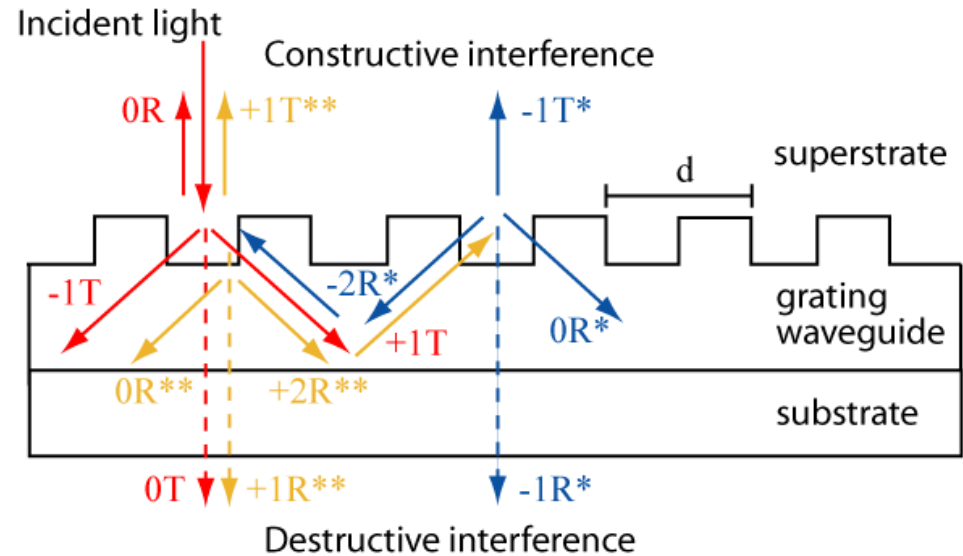
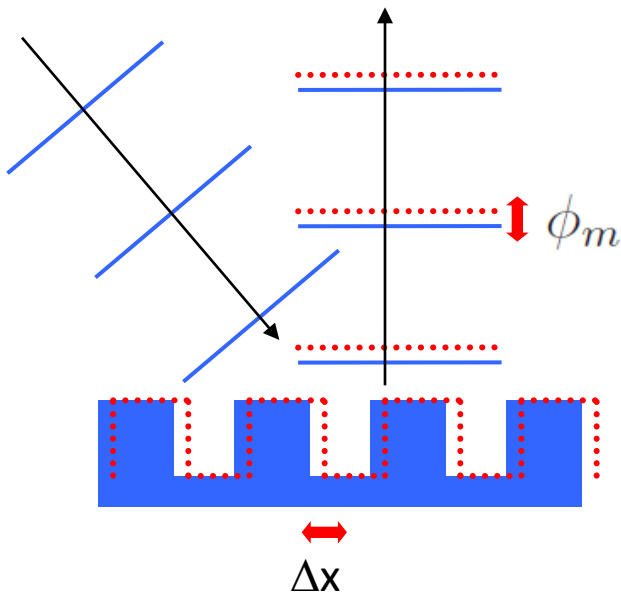
- Single ridges
- Table-top experiment  
Finesse = 660 ( $\pm 30$ )  
 $\rightarrow R = 99.08 (\pm 0.04)\%$

- Etch stop design
- Fully suspended 10 meter cavity  
Finesse = 790 ( $\pm 100$ )  
 $\rightarrow R \geq 99.2 (\pm 0.1)\%$



# Lateral displacement

$$\phi_m = -m \frac{\Delta x}{d} 2\pi$$



- ✓ All phase shifts cancel (geometry)
- Also tested with rigorous methods

*DF, PhD thesis*

# Silicon WGGs @ 1550nm

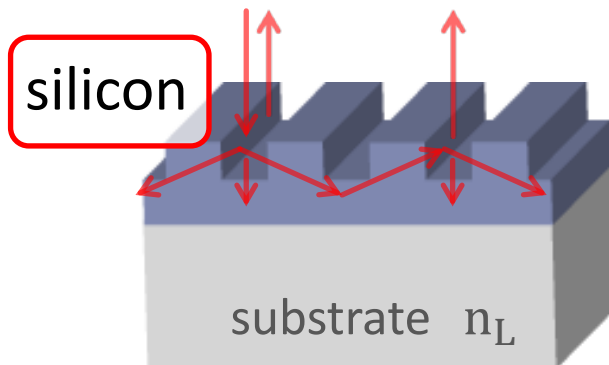
- Promising material for **3rd generation detectors**

Design study: ET-0106C-10

- Very well suited for **cryogenic temperatures**

- Thermoelastic noise  
~0 @ T=18 and 120K

- Low mechanical loss  
 $\phi_{Si} \sim 10^{-9}$  @ T=10K



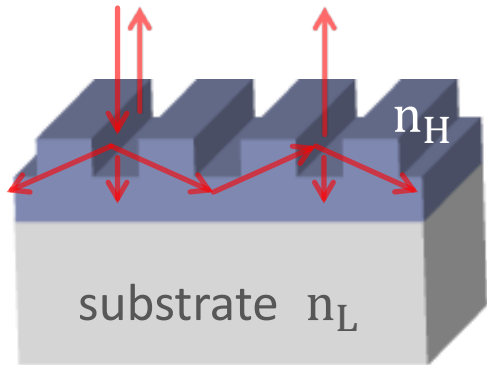
- Very well suited for **WGG**

$n_H = 3.5$  @ 1550nm

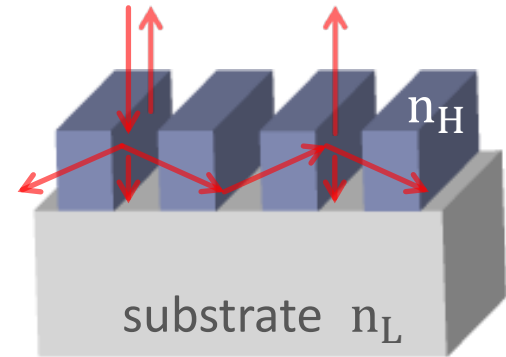
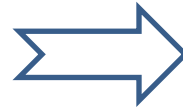
→ high coupling efficiencies

→ parameter tolerant WGG

# Reduction of Low Index Material



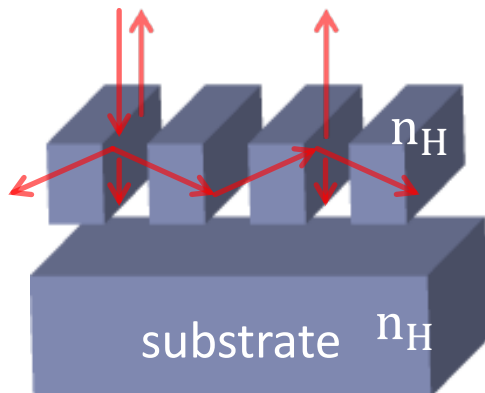
Only ridges



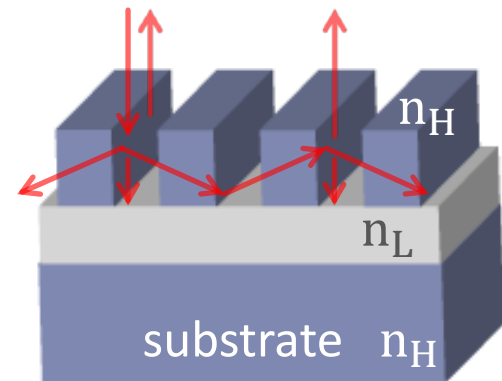
*F. Brückner et al. Opt. Express* **17** (2009)



Reduce low index material



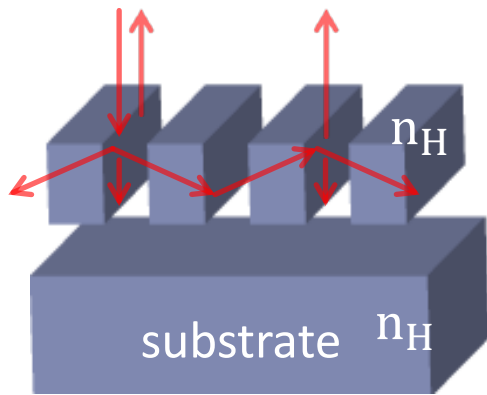
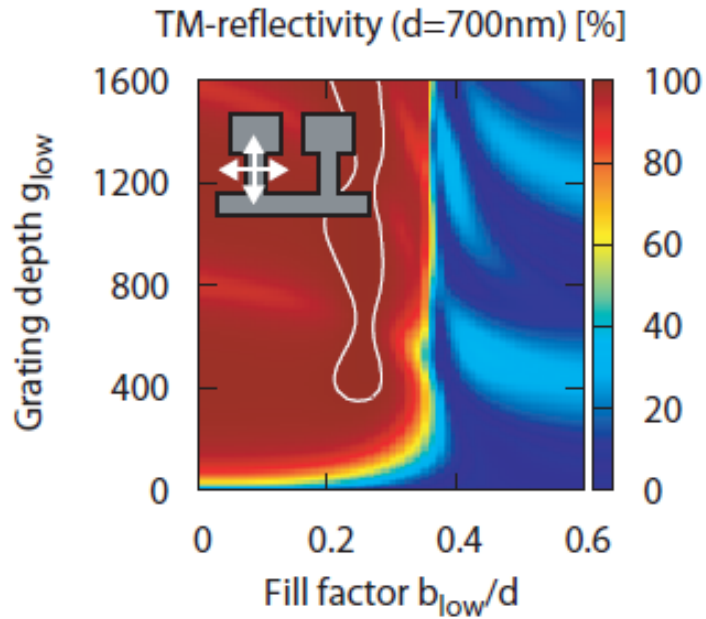
Replace by air



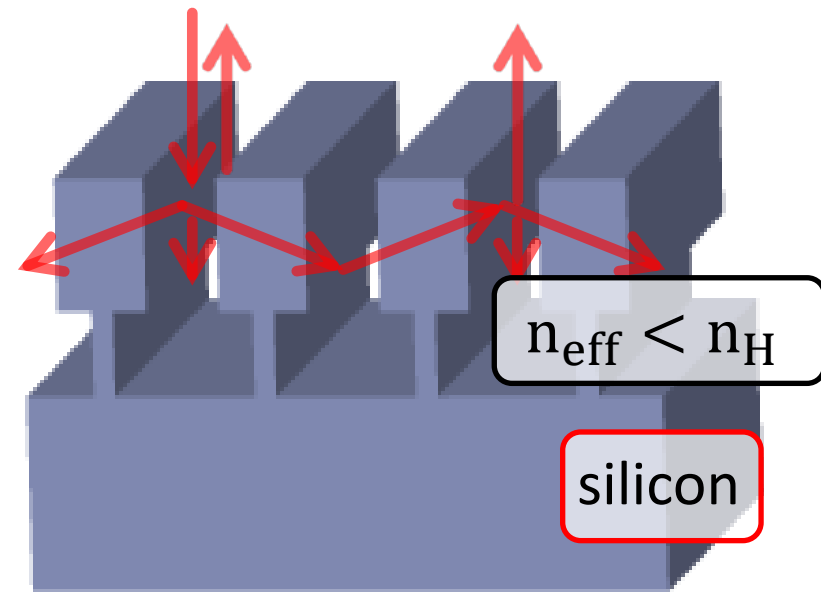
*J.-S. Ye et al., J. Mod. Opt* **53**, 1995 (2006)

*C.F.R. Mateus et al. IEEE Phot. Tech. Lett.* **16**, 1676 (2004)

# Monolithic Design



Thin grating structure

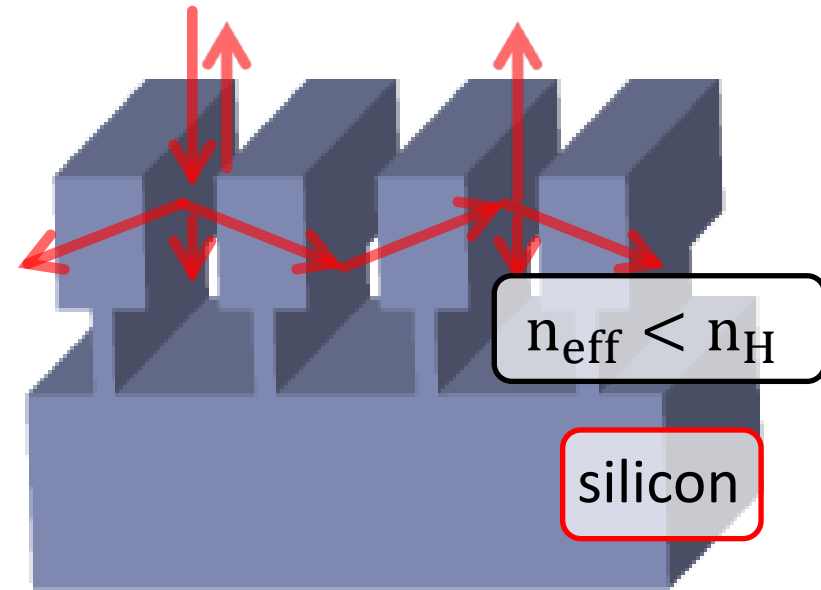
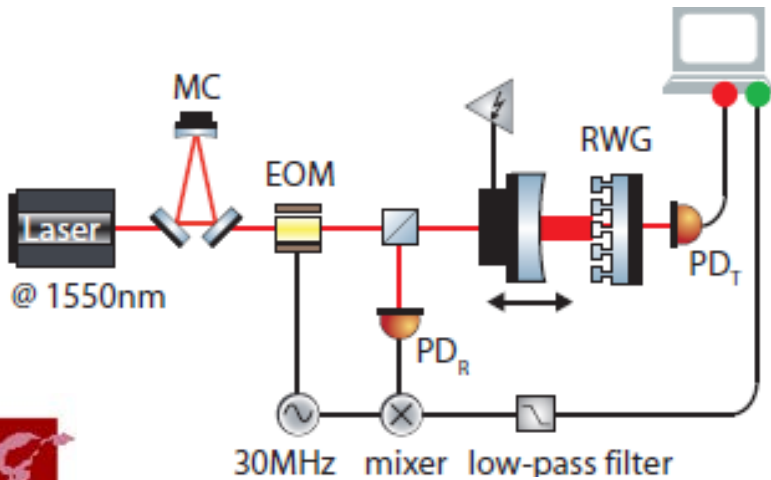
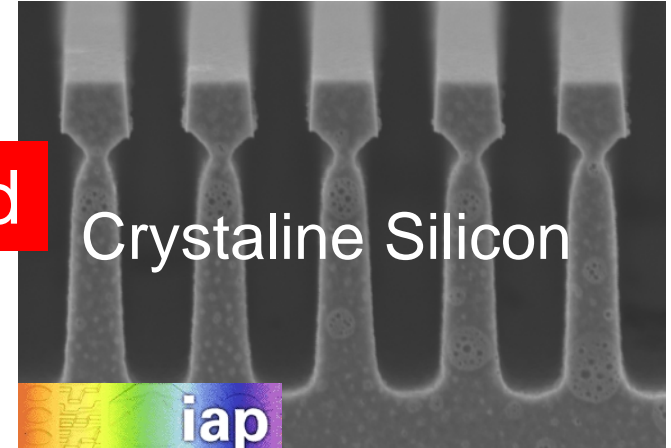


J.-S. Ye et al., *J. Mod. Opt.* **53**, 1995 (2006)

F. Brückner et al. *Opt. Lett.* **33**, 264 (2008)

# Monolithic Realization

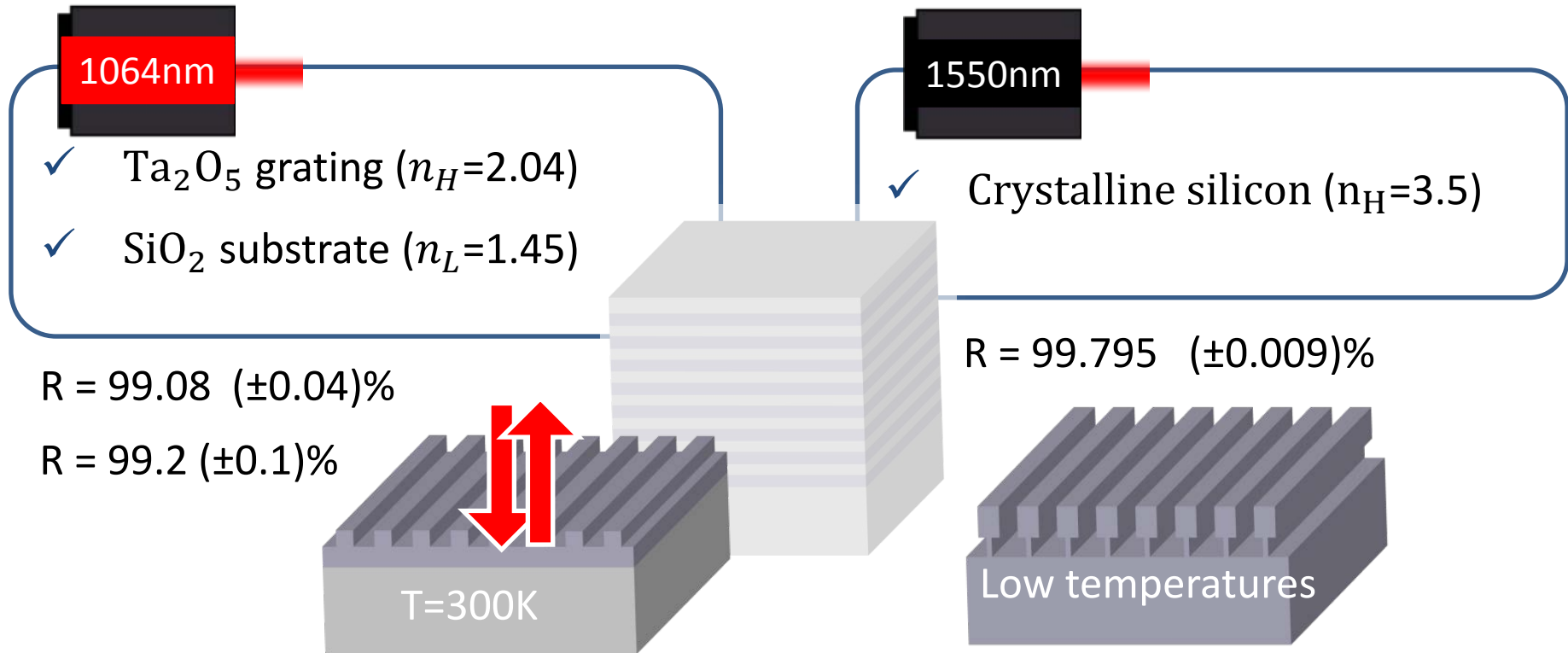
no material is added



Finesse 2780 ( $\pm 100$ )

$\rightarrow R = 99.795 (\pm 0.009)\%$

# Summary: Waveguide Gratings

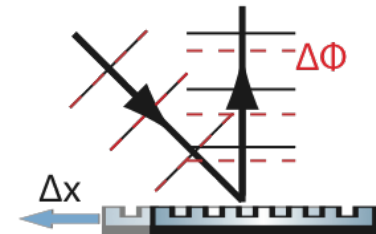
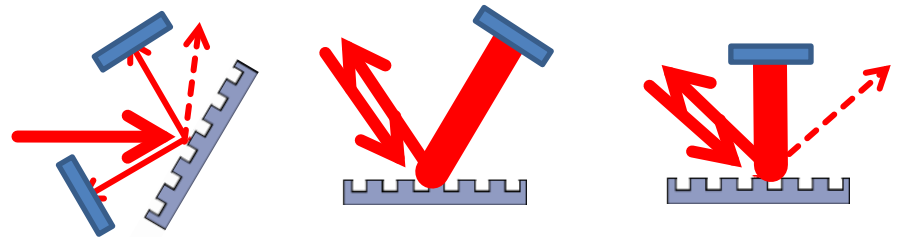
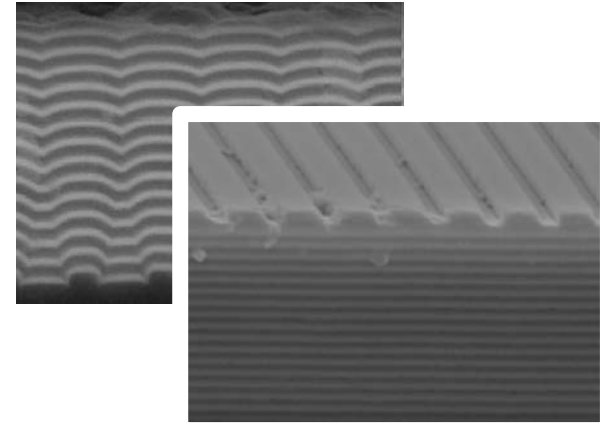


- Thermal noise needs further investigation
- Mirror quality and size need further improvements
- No fundamental differences to multilayer coatings found yet

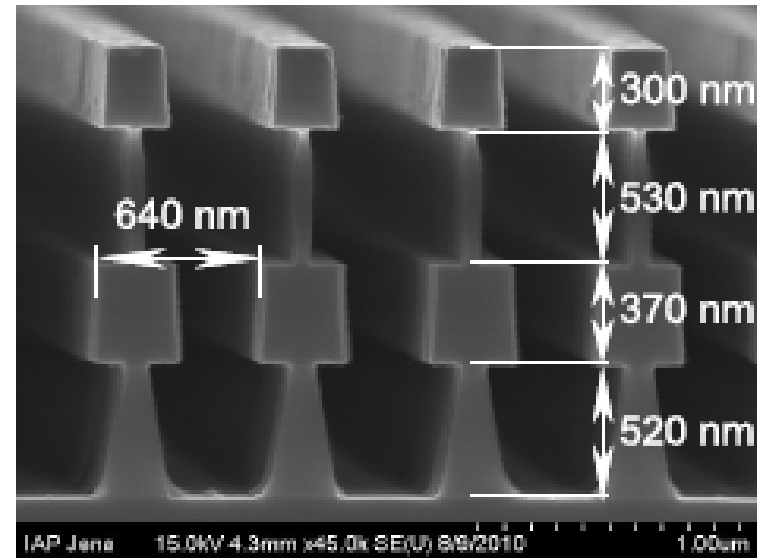
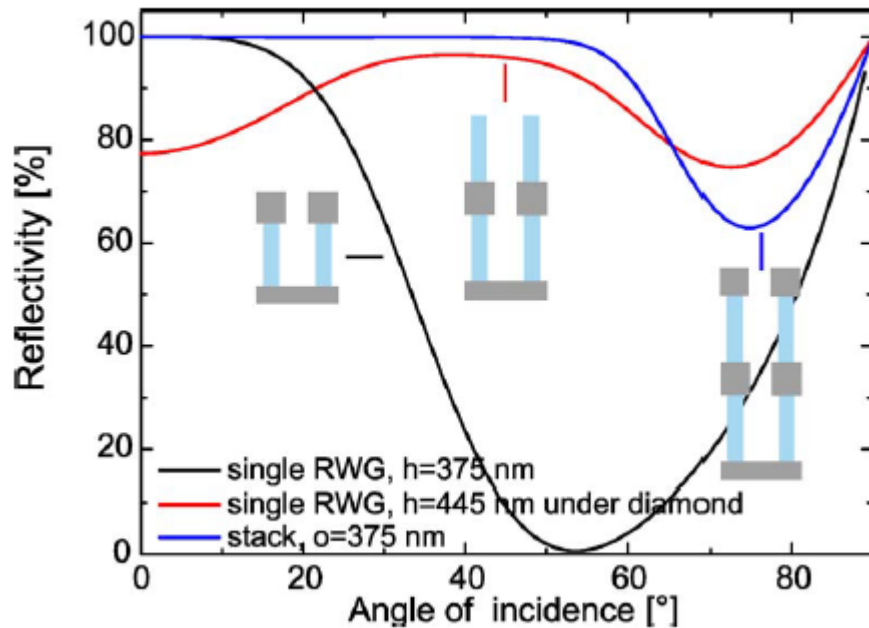


# Summary: Reflection Gratings

- All-reflective interferometry
- Avoid transmission related issues (absorption, heating, ...)
- Potential of using opaque materials
- Various concepts
- Need to find solution for phase noise



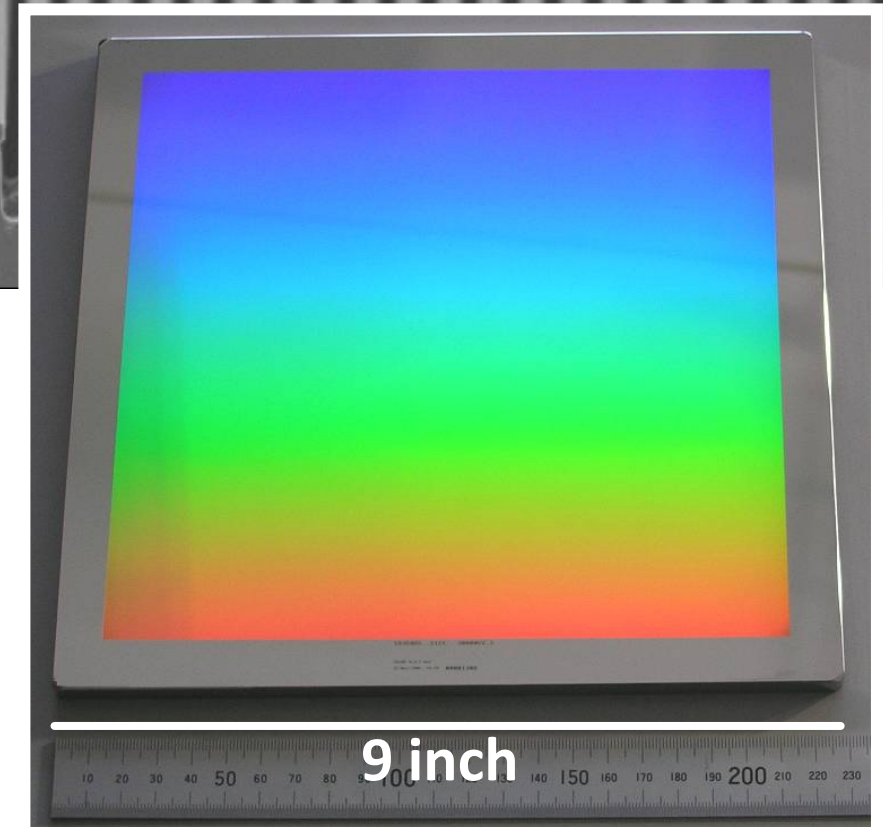
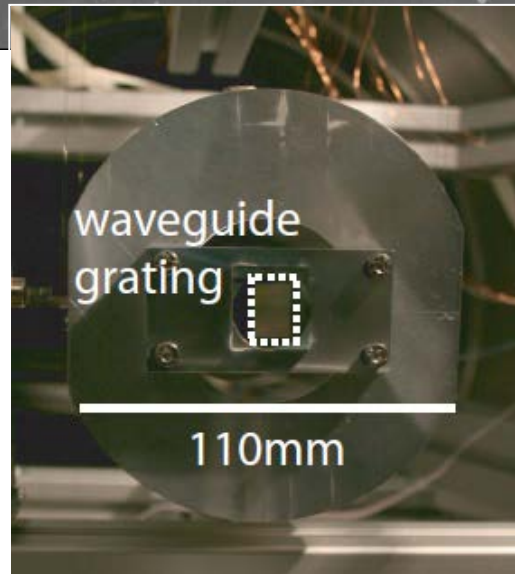
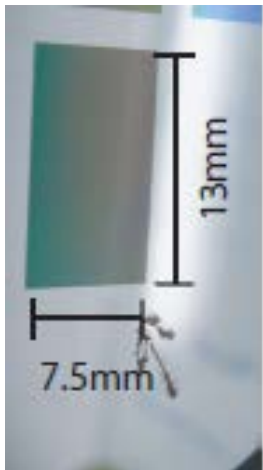
# Merging the two concepts



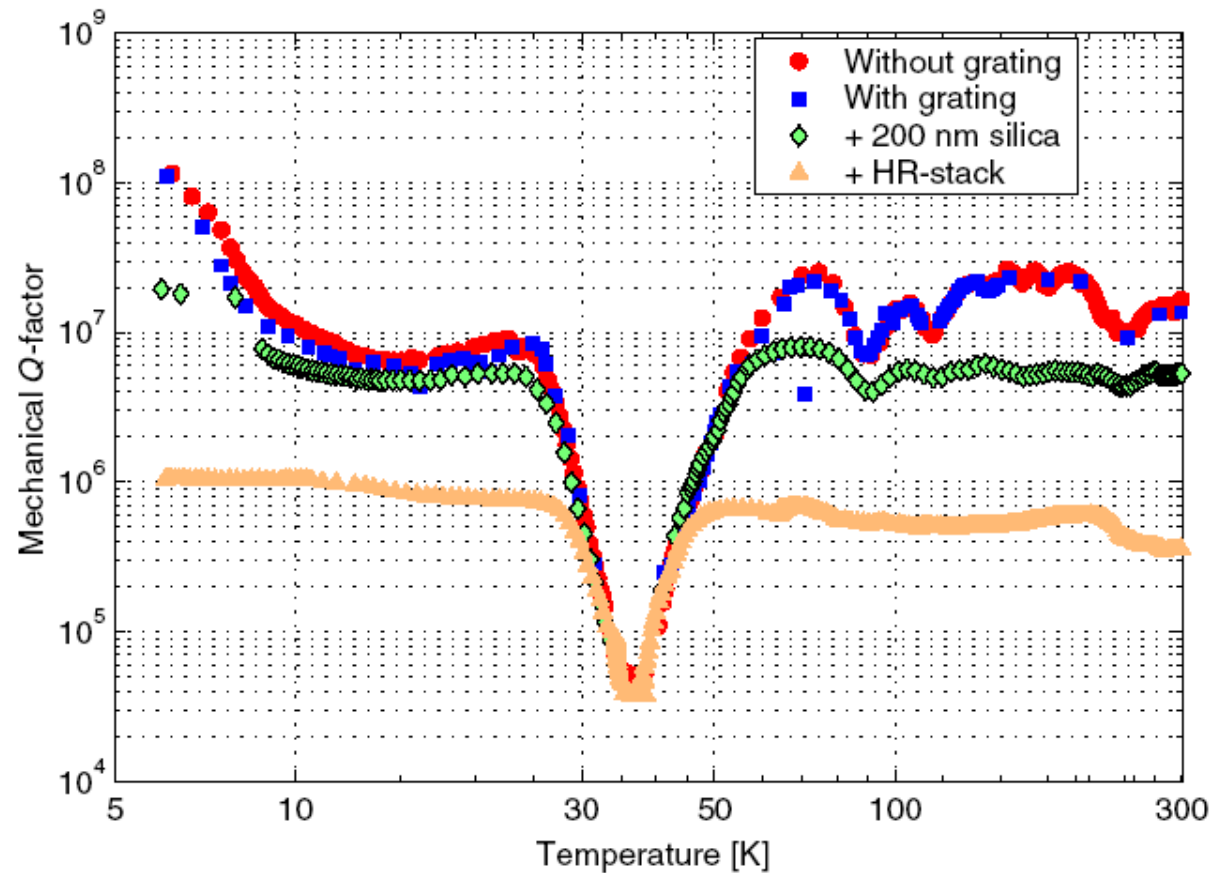
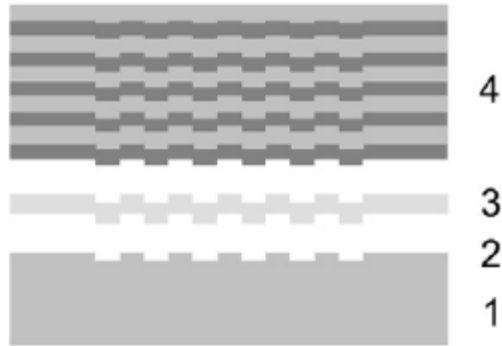
S. Kroker et al., Opt. Lett. **36**, 537 (2011)

S. Kroker et al., Opt.Express. **19**, 16469 (2011)

# Thank You



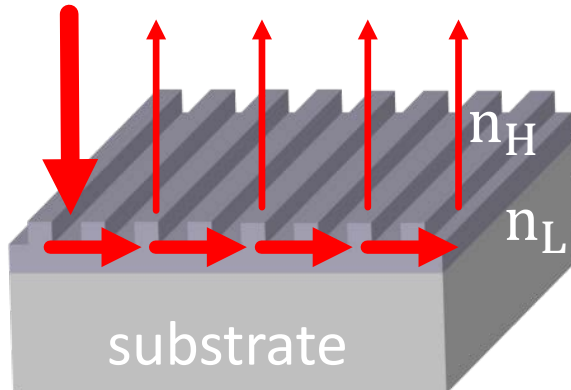
# Mechanical loss of nanostructures



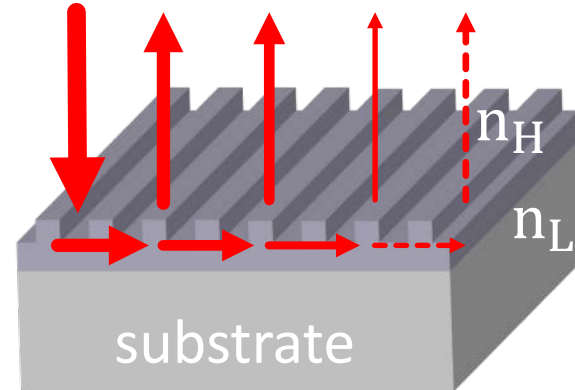
- Grating structure does not „destroy“ high Q-factor of substrate!
- but surface loss is crucial, need to be measured seperately!

# Resonant Excitation

- Small coupling  
→ Long storage time



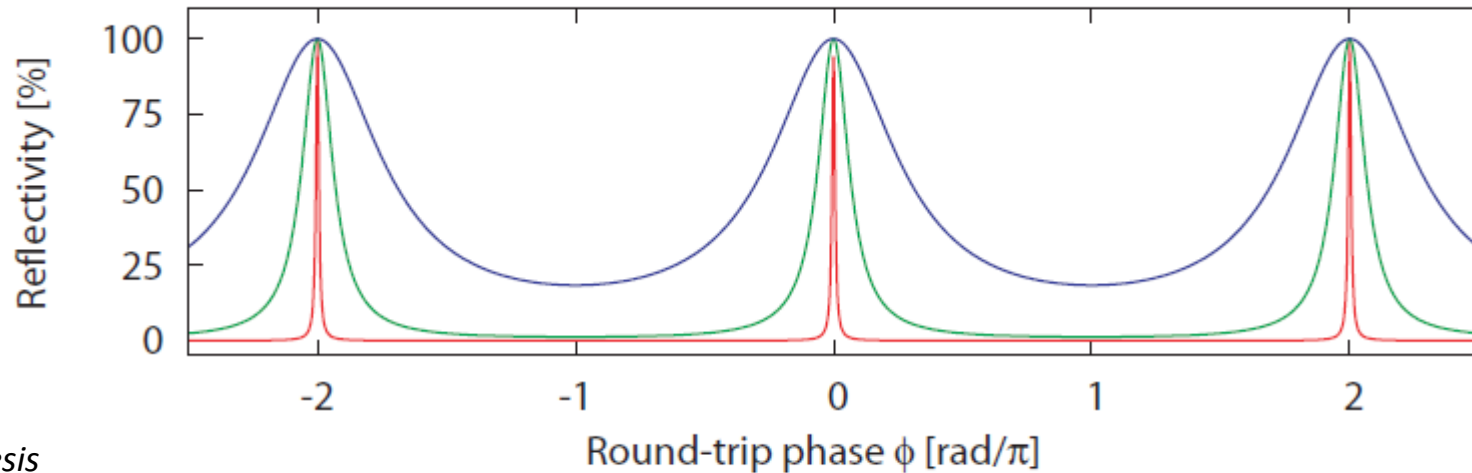
- Strong coupling  
→ Short storage time



$$|\eta_{\pm 1T}|^2 = 0.01$$

$$|\eta_{\pm 1T}|^2 = 0.1$$

$$|\eta_{\pm 1T}|^2 = 0.3$$

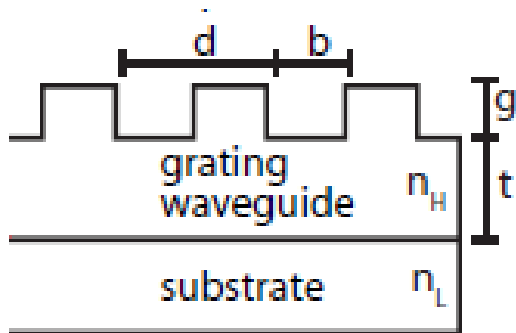


# Diffraction efficiencies

- Rigorous coupled wave analysis (RCWA)

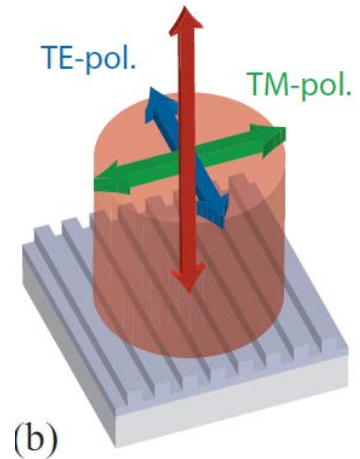
*M.G. Moharam et al. J. Opt. Soc. Am. 71 (1981)*

- For given **wavelength**, **materials** and **polarization**



$d$  grating period  
 $b$  ridge width  
 $g$  groove depth  
 $t$  waveguide thickness

}  $b/d$  fill factor

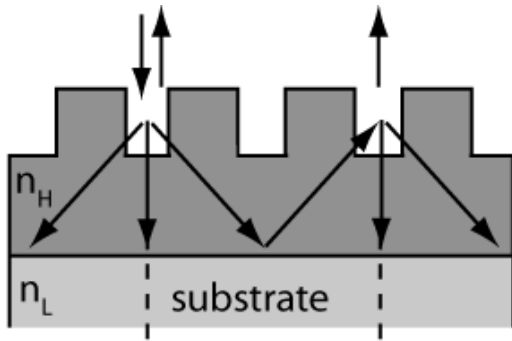


- Numerical implementation: e.g. UNIGIT

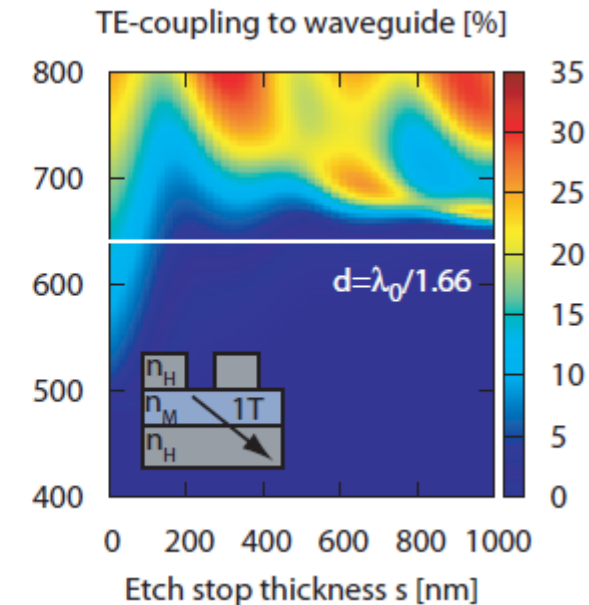
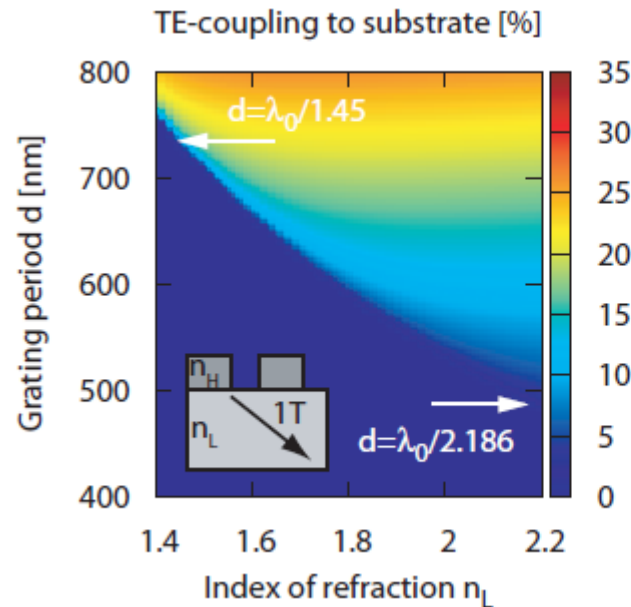
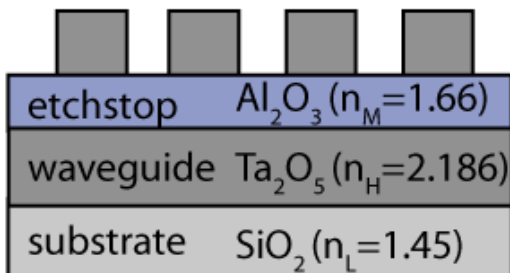
[www.unigit.com](http://www.unigit.com)



# WGG Including Etch Stop Layer

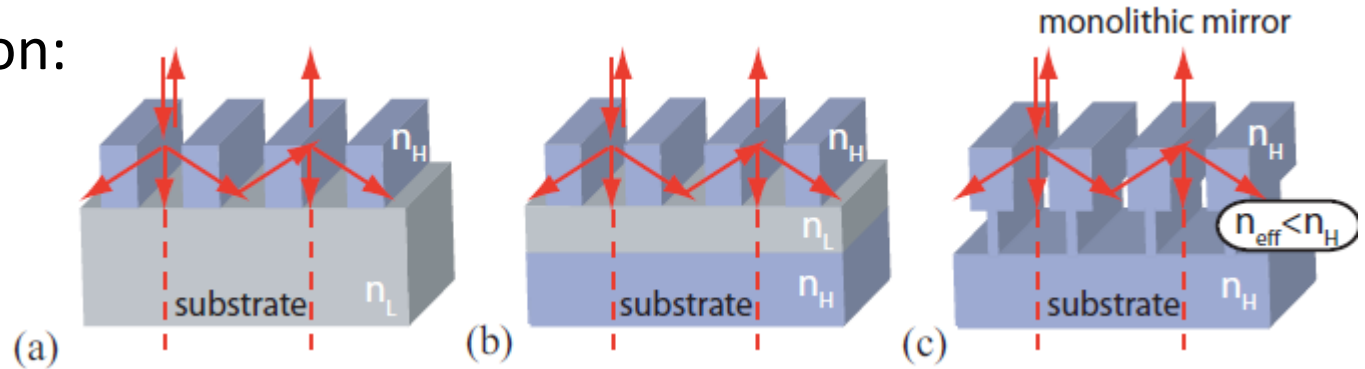


- Etch stop  
→ defines grating depth / waveguide thickness
- Thin etch stop layer  
→ Optical properties can be preserved

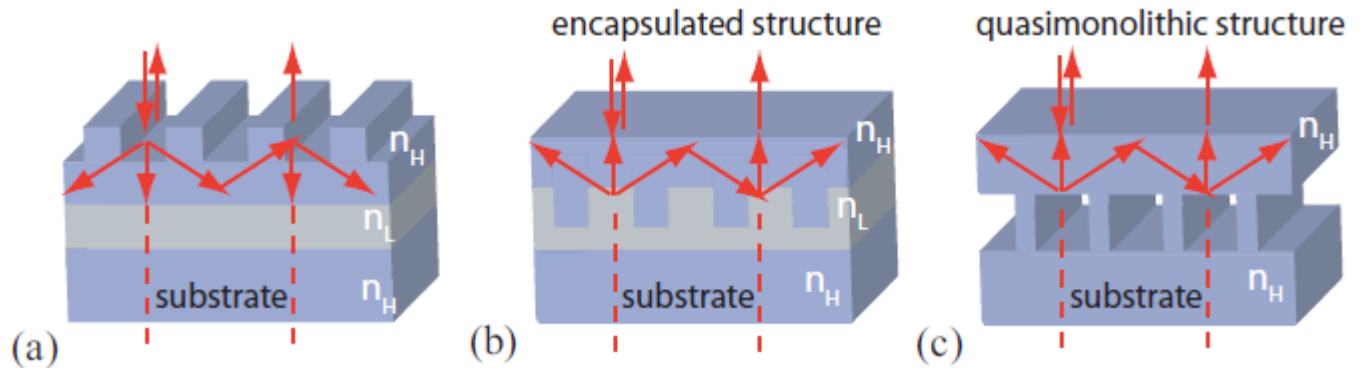


# A Variety of WGGs

Today's presentation:



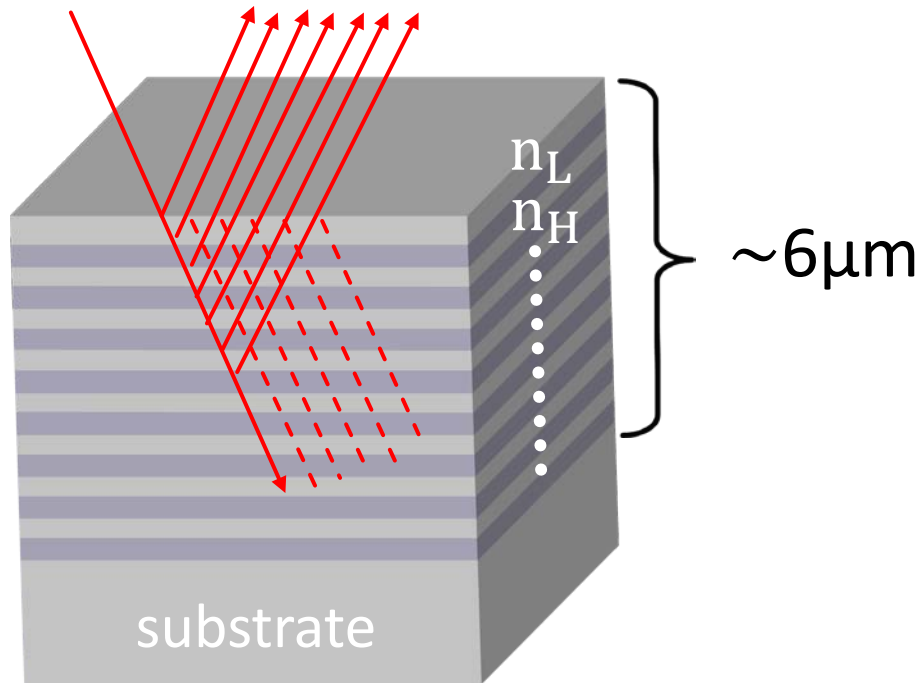
Flat surfaces:



*F. Brückner et al. Opt.Express 17, 24334 (2009)*



# Mirror Brownian Thermal noise



- Temperature  $T$
- Mechanical dissipation  $\phi$
- Beam radius  $r_0$
- Coating thickness  $h$

$$S_x^2 = \frac{2k_b T}{\pi^{3/2} f Y} \frac{1}{r_0} \left[ \underbrace{\phi_{\text{sub}}}_{\text{substrate}} + \frac{h}{\sqrt{\pi r_0}} \underbrace{\left( \frac{Y'}{Y} \phi_{\parallel} + \frac{Y}{Y'} \phi_{\perp} \right)}_{\text{coating}} \right]$$