

Current Status of ASC Design for LCGT

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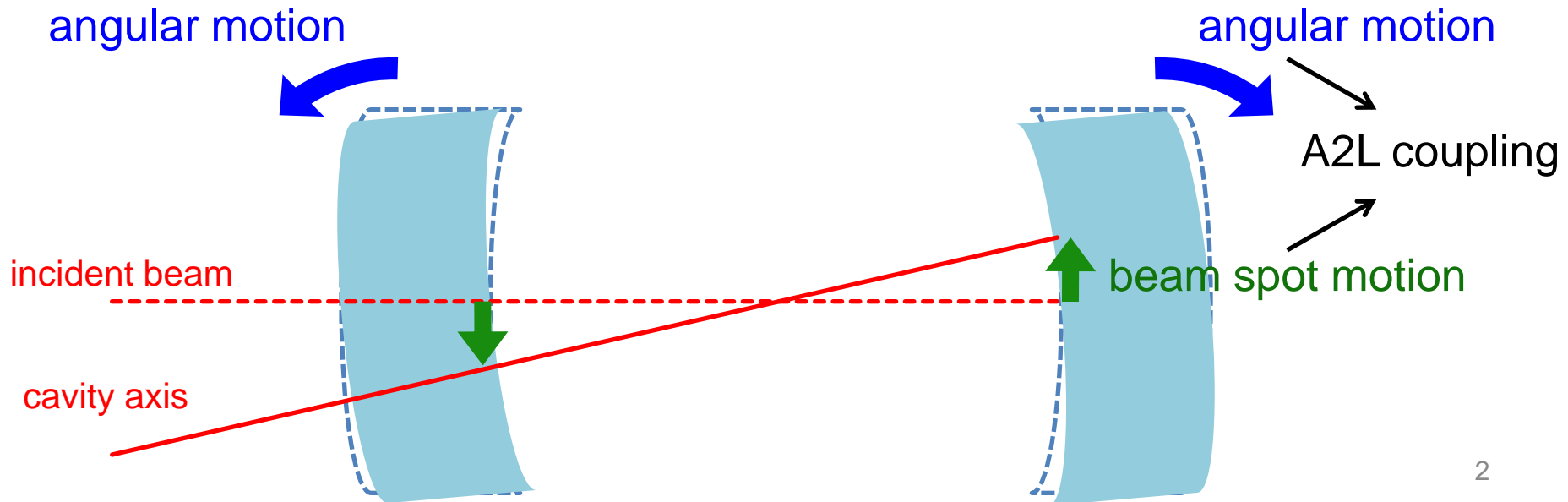
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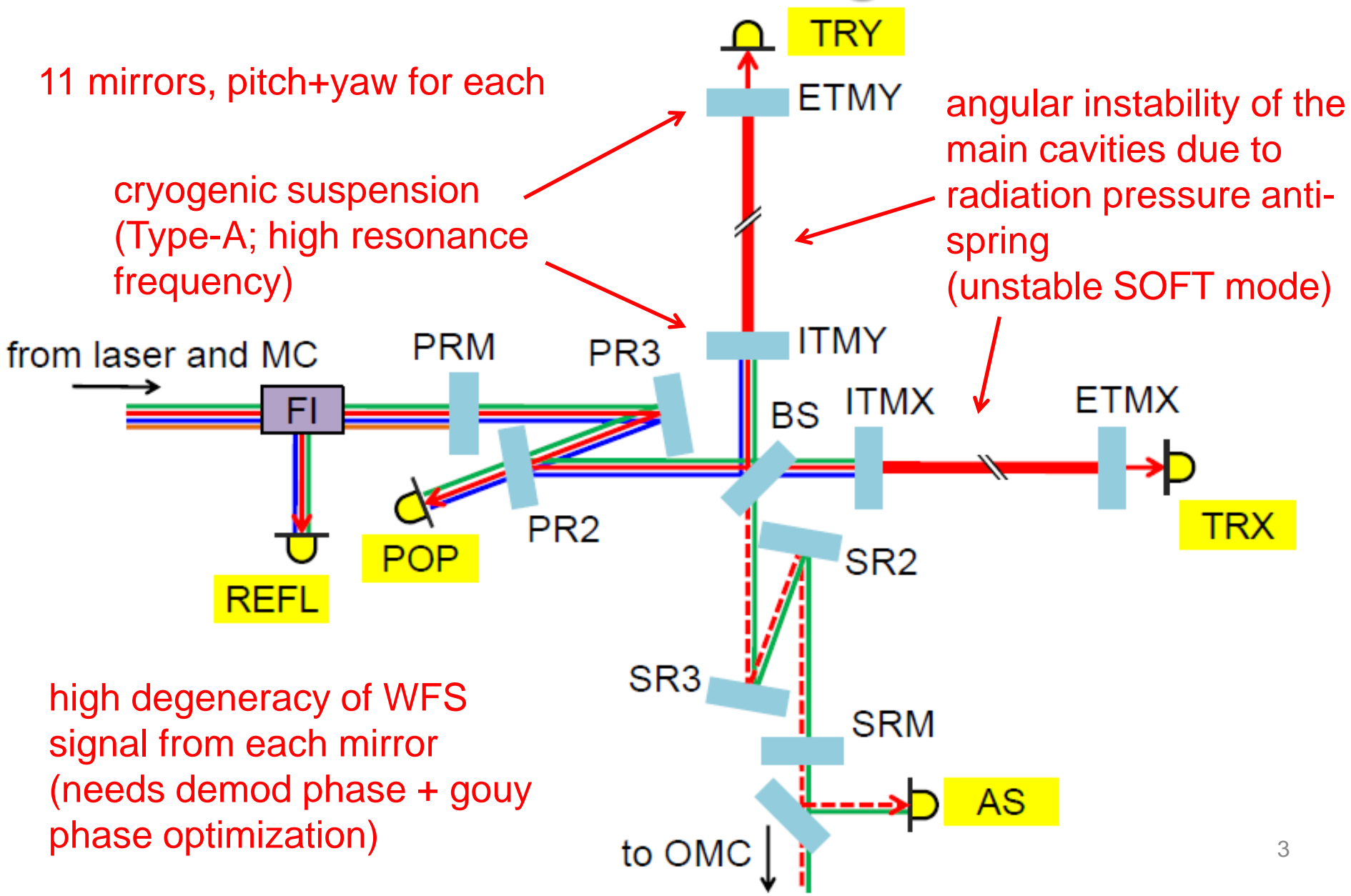
Main Interferometer Group
and Takanori Sekiguchi

What is ASC?

- Alignment Sensing and Control
- angular motion makes beam spot motion and $(\text{angular motion}) \times (\text{BSM})$ makes length fluctuation
→ angular motion must be controlled
- global control(WFS) and local control(OpLev etc)



ASC is tough



What we have done

- developed 3D rigid body model for modeling suspension (by T. Sekiguchi)
- developed a tool for simulating/designing WFS servo loop (this talk)
 - optical response of IFO is simulated using *Optickle*
 - loop noise calculation similar to *pickle* (aLIGO ASC tool)
 - uses suspension TF, angular seismic noise as input
 - matrix based, frequency domain
($11 \times 11 \times \text{freq}$ matrix)

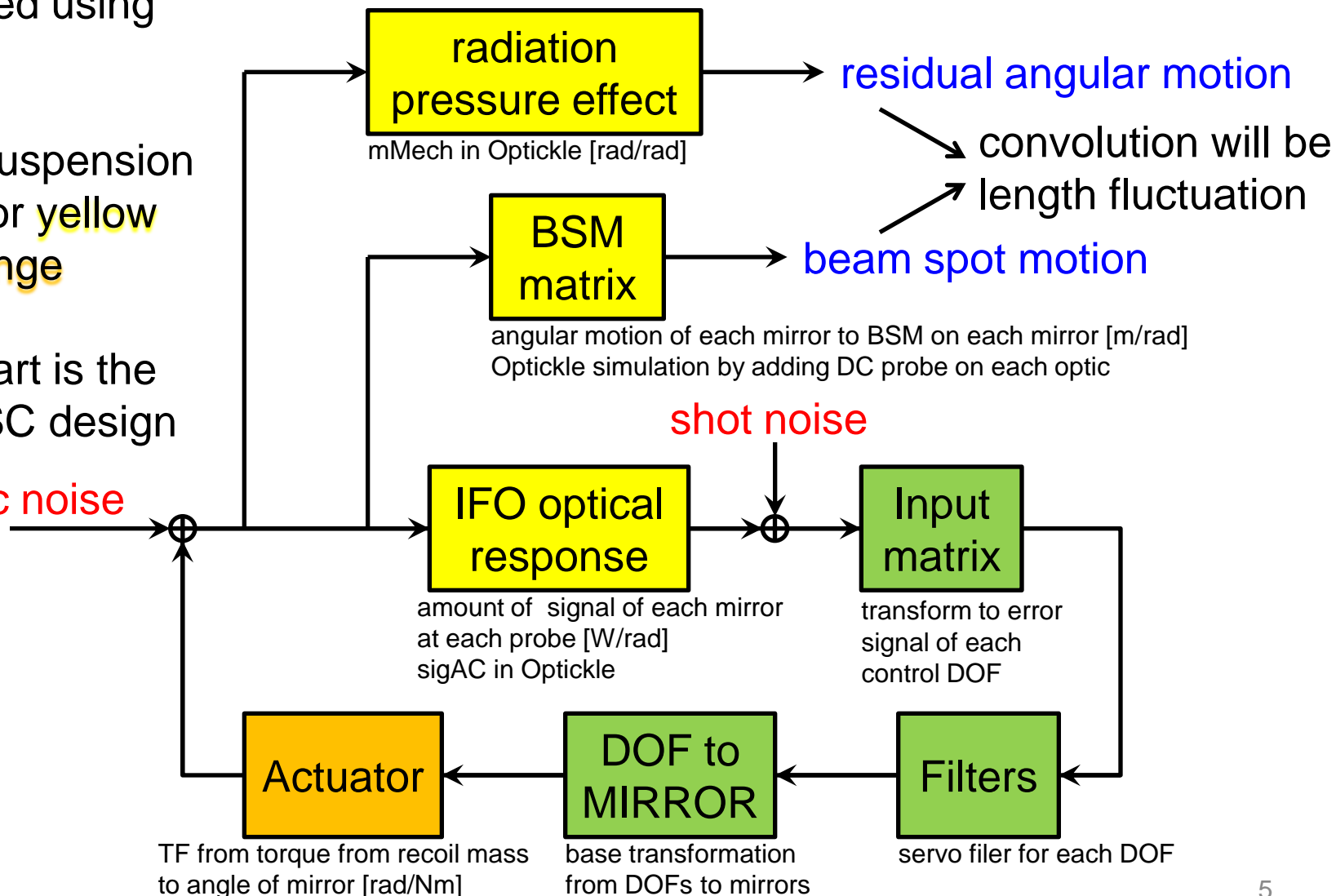
Structure of ASC model

yellow matrices are
calculated using
Optickle

needs suspension
model for yellow
and orange

green part is the
main ASC design

seismic noise



ASC design procedure

- step 0. choose control DOF
- step 1. select sensing ports
demodulation/gouy phase optimization
- step 2. design servo filters (control loop)
- step 3. calculate residual angular motion
- step 4. calculate residual beam spot motion
- step 5. estimate A2L coupling
- step 6. do 0-5 for pitch and yaw
→ is total A2L noise below LCGT sensitivity?

1. Sensing port selection

Optimize demodulation phase + gouy phase and select sensing ports
I / Q is demod phase difference, A / B is gouy phase difference

POP DC

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-19.4	-22.0	-24.7	-81.4	-44.3	-46.9	88.1	87.0	64.5	64.5	64.5
max ampli	-42003.1	-7661.3	-8.2	-0.5	-507.3	-1310.5	-3375.0	-1680.9	1.3	0.2	0.1
Gouy	-2	-2	NaN	NaN	71	71	70	70	NaN	NaN	NaN
ampli	-28338.6	-5091.0	NaN	NaN	153.3	433.5	-2268.6	-1136.5	NaN	NaN	NaN
contami	-1.2	6.8	NaN	NaN	29.4	10.4	2.0	3.9	NaN	NaN	NaN
N big sig	1	2	NaN	NaN	6	3	1	2	NaN	NaN	NaN

POP_ADC (min CS)

POP f1 demodulation

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-17.1	-32.9	51.8	51.8	39.3	-28.6	-27.3	19.6	-25.5	-25.5	-25.5
max demod	0.1	0.1	-89.9	-89.9	-71.0	-0.1	-0.1	0.5	-0.0	-0.0	-0.0
max ampli	-118.7	-119.7	53.4	-65.5	48.4	-70.7	-8.2	-8.3	-164.2	-19.7	-10.3
Gouy	64	-73	-81	-81	-82	-73	-73	-38	-73	-73	-73
demod	0	-2	-89	-89	-89	-2	-2	-90	-2	-2	-2
ampli	81.1	-91.5	-36.3	44.5	-32.3	-50.5	-5.7	0.1	-110.7	-13.3	-7.0
contami	-1.3	3.3	3.1	2.5	3.6	6.0	52.9	13.1	2.7	22.7	43.2
N big sig	1	2	2	1	3	3	7	6	1	5	6

POP_B1Q

POP_B1I (min CS)

POP f2 demodulation

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-72.6	78.6	81.8	79.5	75.5	75.5	75.5	75.4	81.5	81.5	81.5
max demod	0.1	0.1	-26.9	-23.0	0.0	0.1	0.1	0.1	-90.0	-90.0	-90.0
max ampli	-5076.6	2282.9	2.8	-4.0	1947.9	5511.2	660.5	335.8	0.0	0.0	0.0
Gouy	-17	-20	70	70	69	-20	-70	-14	NaN	NaN	NaN
demod	-90.6	-55.7	90	90	90	-2	-2	-2	NaN	NaN	NaN
ampli	-1.2	3.3	6.2	5.6	4.9	2.1	17.8	36.2	NaN	NaN	NaN
contami	1	2	4	2	2	1	4	5	NaN	NaN	NaN
N big sig	1	2	4	2	2	1	4	5	NaN	NaN	NaN

AS DC

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-16.9	-16.9	-87.3	-30.2	-6.2	-24.9	-26.6	83.7	-13.3	-12.9	23.8
max ampli	-7.5	9.2	-0.2	0.3	-2.7	5.7	0.6	0.9	12.7	1.6	1.1
Gouy	-66	-66	74	77	73	77	77	73	64	65	73
ampli	-3.5	4.3	0.1	-0.1	-0.4	-0.8	-0.1	0.6	2.0	0.2	0.5
contami	-5.5	4.5	22.3	53.4	8.4	3.9	31.1	4.9	3.1	24.5	5.9
N big sig	3	2	6	9	5	1	8	1	1	7	4

AS_BDC (min CS/CH)

AS f1 demodulation

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	84.8	81.4	89.5	86.2	-13.4	89.6	89.5	88.6	76.8	77.1	-67.5
max demod	-90.0	-90.0	-90.0	-90.0	-90.0	-90.0	-90.0	-90.0	-90.0	-90.0	89.3
max ampli	-0.3	-0.0	-1511.0	-245.9	9.2	0.5	0.1	0.0	-0.0	-0.0	-0.0
Gouy	NaN	NaN	0	0	-1	NaN	NaN	NaN	NaN	NaN	NaN
demod	NaN	NaN	0	0	0	NaN	NaN	NaN	NaN	NaN	NaN
ampli	NaN	NaN	0.0	-0.0	0.0	NaN	NaN	NaN	NaN	NaN	NaN
contami	NaN	NaN	1.1	2.3	3.9	NaN	NaN	NaN	NaN	NaN	NaN
N big sig	NaN	NaN	1	1	3	NaN	NaN	NaN	NaN	NaN	NaN

AS_A1Q (max DS)

REFL DC

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-3.5	3.8	-0.8	-16.8	2.1	3.9	4.0	36.0	83.8	83.8	83.8
max ampli	-66522.5	-57318.2	-57.7	43.8	-28726.4	-81234.2	-9402.2	-3818.7	-2485.2	-297.9	-156.4
Gouy	-86	86	NaN	NaN	-6	86	86	-87	-86	-86	-86
ampli	-6172.3	-5533.9	NaN	NaN	-20108.3	-7887.1	-923.3	1472.1	1729.5	207.3	108.9
contami	-1.7	3.7	NaN	NaN	8.6	2.6	22.4	7.3	6.1	50.9	96.9
N big sig	1	2	NaN	NaN	4	1	6	3	2	5	6

REFL f1 demodulation

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-89.9	85.9	71.8	71.1	-13.8	-22.3	-57.0	19.2	-6.2	-6.2	-6.2
max demod	0.0	0.0	77.6	-88.3	0.6	0.0	0.0	0.0	-0.1	-0.1	-0.1
max ampli	-161213.2	26218.0	-128.0	-153.4	-909.2	-3111.6	-620.1	6313.7	-384.4	-46.1	-24.2
Gouy	-71	0	0	0	0	0	0	0	0	NaN	NaN
demod	-1	-3	-90	-90	-90	-3	-3	-3	-4	NaN	NaN
ampli	-152357.5	-1858.0	40.5	-49.7	35.9	-2876.0	-337.4	5954.7	-381.3	NaN	NaN
contami	-1.2	6.7	3.3	2.7	3.7	4.4	37.1	2.1	32.8	NaN	NaN
N big sig	1	3	2	1	3	2	6	1	5	NaN	NaN

REFL_B1I (min CS)

REFL f2 demodulation

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-89.9	84.0	78.4	-86.7	-74.9	-75.4	-78.1	26.3	-79.3	-79.3	-79.3
max demod	0.1	0.2	8.5	-16.5	0.0	0.0	0.0	-0.0	89.8	89.8	89.8
max ampli	-63972.4	19501.2	-21.6	13.3	-4926.0	-14407.0	-2073.0	6213.0	0.0	0.0	0.0
Gouy	-78	40	NaN	-9	0	0	0	-1	NaN	NaN	NaN
demod	-90	-90	NaN	-90	-90	-90	-90	-87	NaN	NaN	NaN
ampli	-265.0	105.4	NaN	-3.7	67.6	185.4	21.8	291.7	NaN	NaN	NaN
contami	-1.2	3.7	NaN	87.6	5.7	2.1	17.8	1.2	NaN	NaN	NaN
N big sig	1	2	NaN	3	3	1	4	1	NaN	NaN	NaN

REFL_A2I (max CS)

TRX DC

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-25.6	74.8	-25.6	74.8	-10.4	0.5	0.4	-0.6	-36.3	-36.3	-36.3
max ampli	-43183.8	15641.0	-43183.3	15640.8	0.0	-43.4	-5.2	-2.6	0.0	0.0	0.0
Gouy	-15	64	-15	64	NaN	NaN	NaN	NaN	NaN	NaN	NaN
ampli	30013.6	10865.5	30013.4	10865.4	NaN	NaN	NaN	NaN	NaN	NaN	NaN
contami	2.0	2.0	2.0	2.0	NaN	NaN	NaN	NaN	NaN	NaN	NaN
N big sig	1	1	2	2	NaN	NaN	NaN	NaN	NaN	NaN	NaN

TRX_ADC (min CS/DS)

TRY DC

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM
max Gouy	-25.6	74.8	-25.6	74.8	0.5	0.5	0.4	-0.6	-23.9	-23.9	-23.9
max ampli	-43183.8	15641.0	-43183.4	15640.8	-30.6	-43.4	-5.2	-2.6	-0.0	-0.0	-0.0
Gouy	-15	64	-15	64	NaN	NaN	NaN	NaN	NaN	NaN	NaN
ampli	30013.7	10865.5	30013.5	10865.4	NaN	NaN	NaN	NaN	NaN	NaN	NaN
contami	2.0	2.0	2.0	2.0	NaN	NaN	NaN	NaN	NaN	NaN	NaN
N big sig	1	1	2	2	NaN	NaN	NaN	NaN	NaN	NaN	NaN

TRY_ADC (min CS/DS)

1. Sensing port selection

sensing ports

WFS Sensing Matrix [W/mrad/sqrt(2/pi)]

(Gouy phases at POP A:70.6, POP B:-72.9 REFL A:-89.9, REFL B:-0.1, AS A:89.5, AS B:73.1, TR A:64.4 deg)

	CS	CH	DS	DH	BS	PR3	PR2	PRM	SR3	SR2	SRM	
REFL_A2I	163.97	19.39	0.02	0.01	-4.76	-13.95	-2.03	-2.74	0.00	0.00	0.00	
TRX_ADC	0.03	10.88	0.03	10.88	0.00	-0.01	-0.00	-0.00	-0.00	-0.00	-0.00	
AS_A1Q	0.00	0.00	1.51	0.25	0.00	-0.00	-0.00	-0.00	0.00	0.00	0.00	
TRY_ADC	0.03	10.88	-0.03	-10.88	-0.01	-0.01	-0.00	-0.00	-0.00	-0.00	-0.00	
POP_B1Q	-0.00	-0.00	0.03	-0.04	0.03	-0.00	-0.00	-0.00	-0.00	-0.00	-0.00	
REFL_BDC	-46.95	-40.43	-0.04	0.03	-20.30	-57.30	-6.63	-2.18	-0.19	-0.02	-0.01	
POP_ADC	0.03	0.24	0.00	0.00	0.15	0.43	-2.28	-1.14	0.00	0.00	0.00	
REFL_B1I	0.27	-1.81	-0.00	-0.00	-0.88	-2.88	-0.34	5.96	-0.38	-0.05	-0.02	
POP_B1I	-0.00	-0.09	0.00	-0.00	0.02	-0.05	-0.01	0.00	-0.11	-0.01	-0.01	
AS_BDC	-0.00	0.00	0.00	-0.00	-0.00	-0.00	-0.00	0.00	0.00	0.00	0.00	

← control DOF

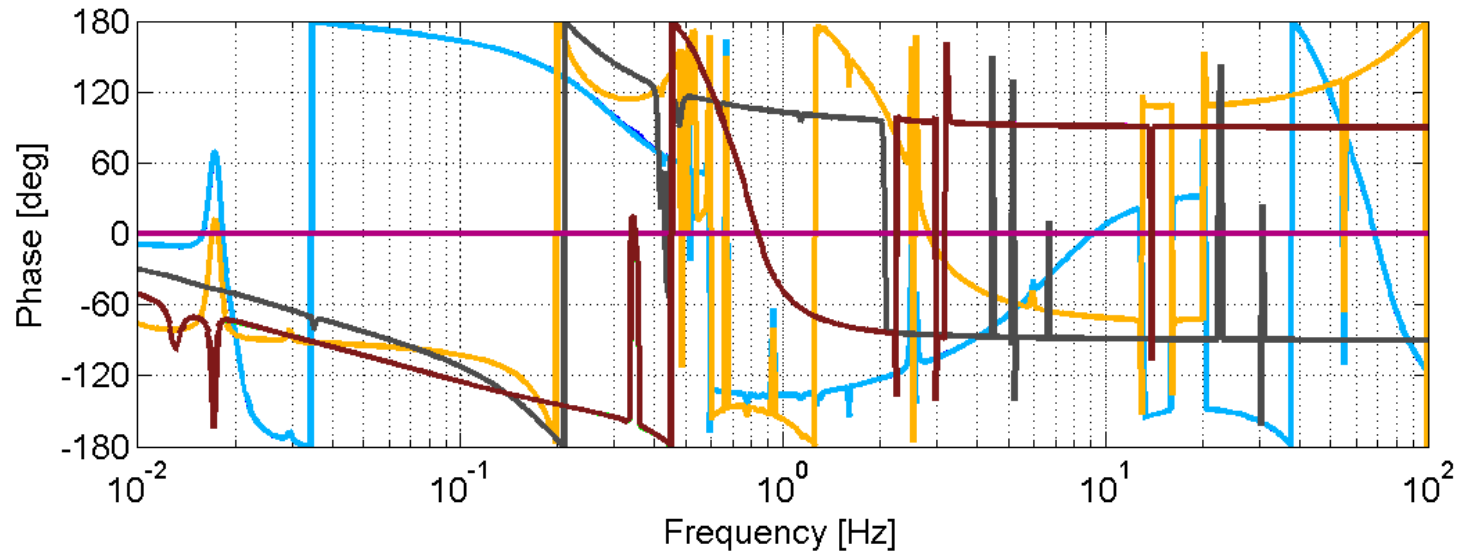
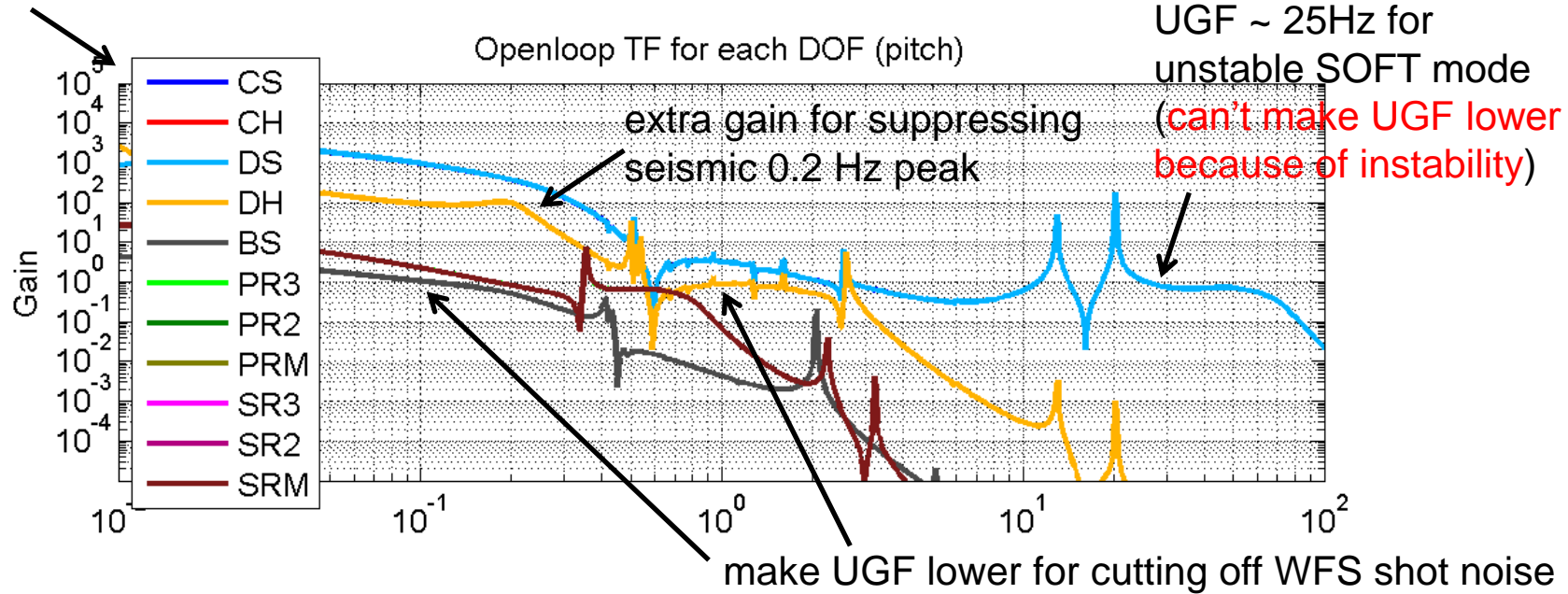
barely diagonalized

reconstruct error
signal for each DOF
by combining signal
from sensing ports
(input matrix)

small WFS signal, so no WFS control for SR2

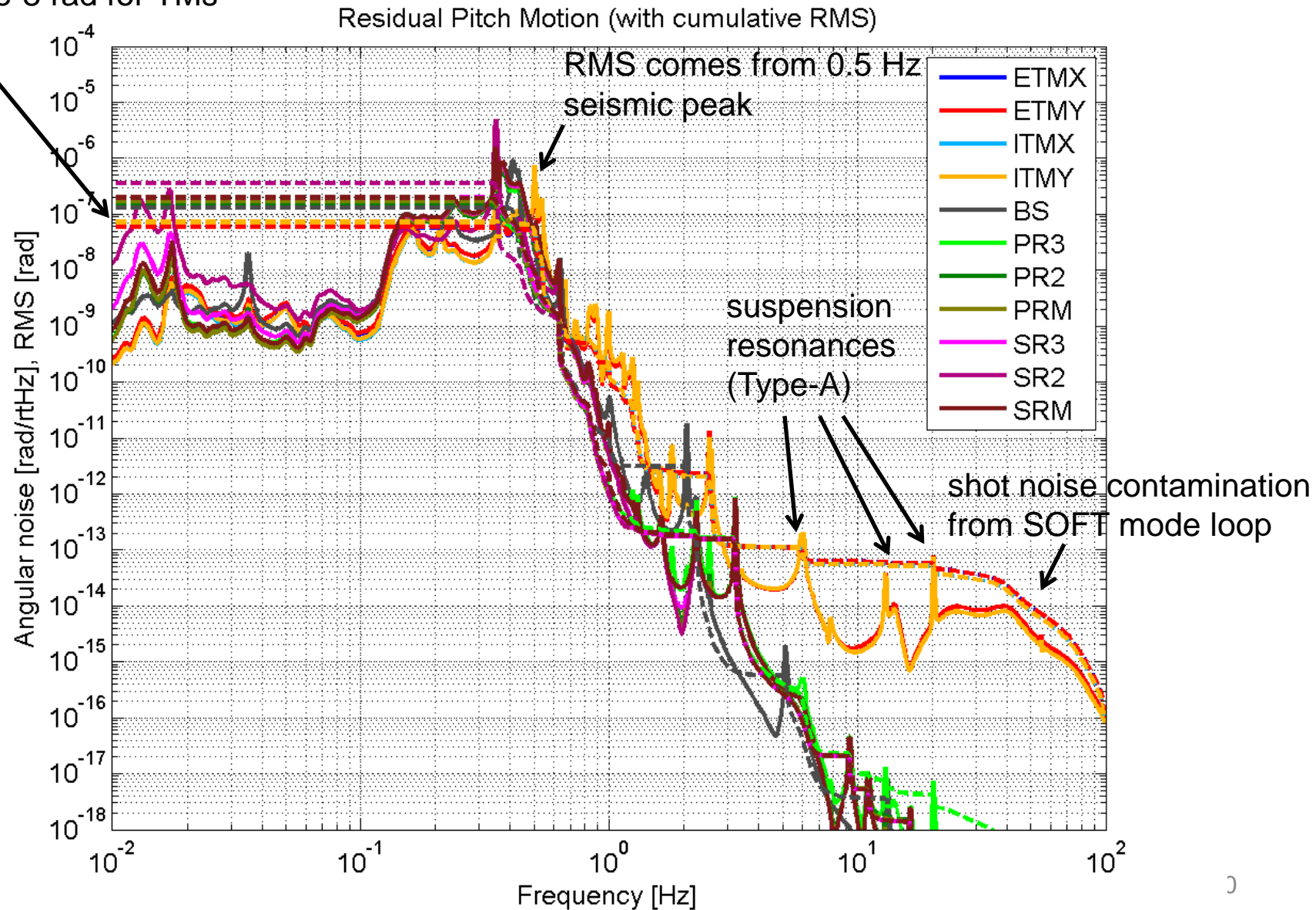
high gain at DC
for drift control

2. Design control loop



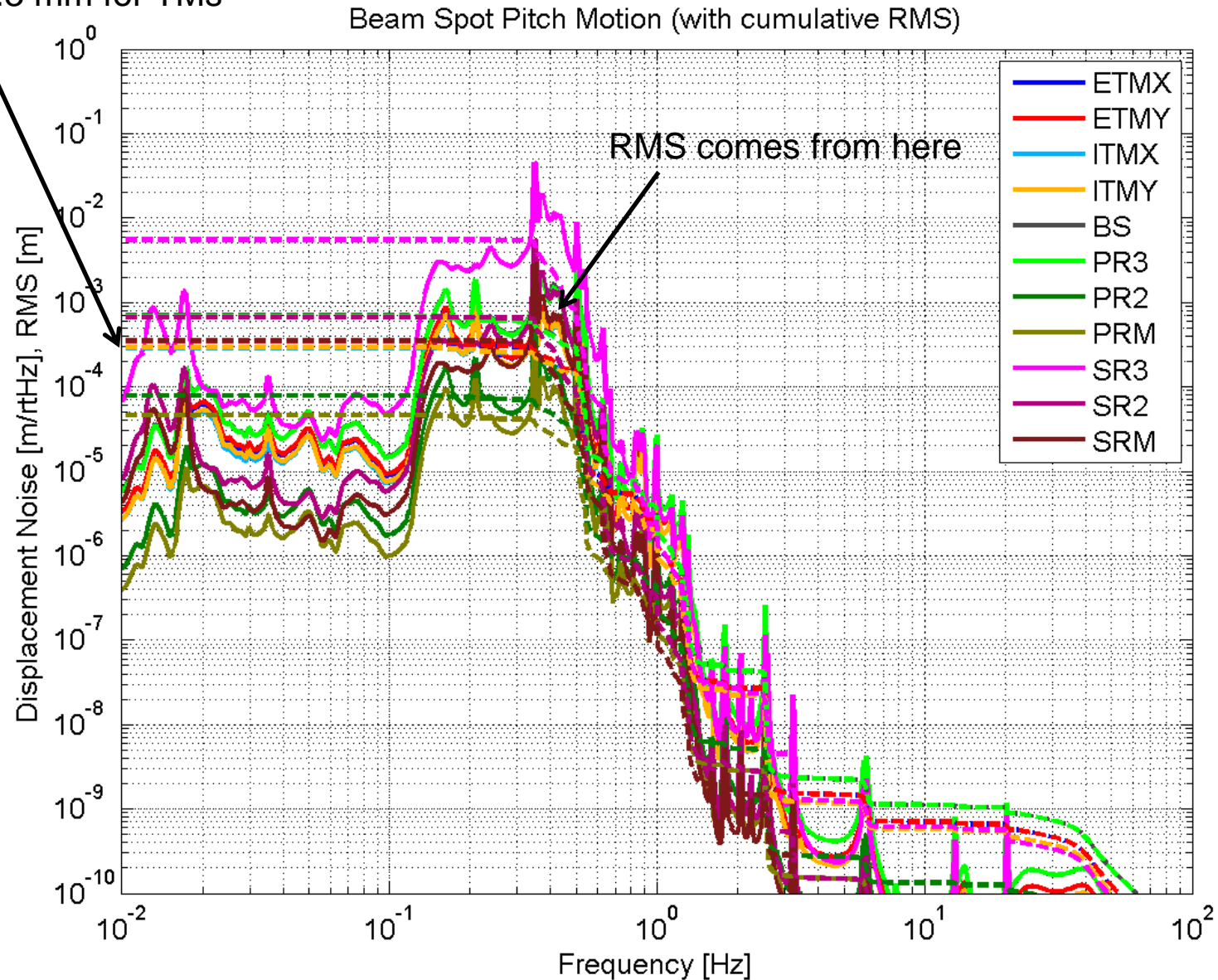
3. Residual angular motion

RMS $\sim 6e-8$ rad for TMs

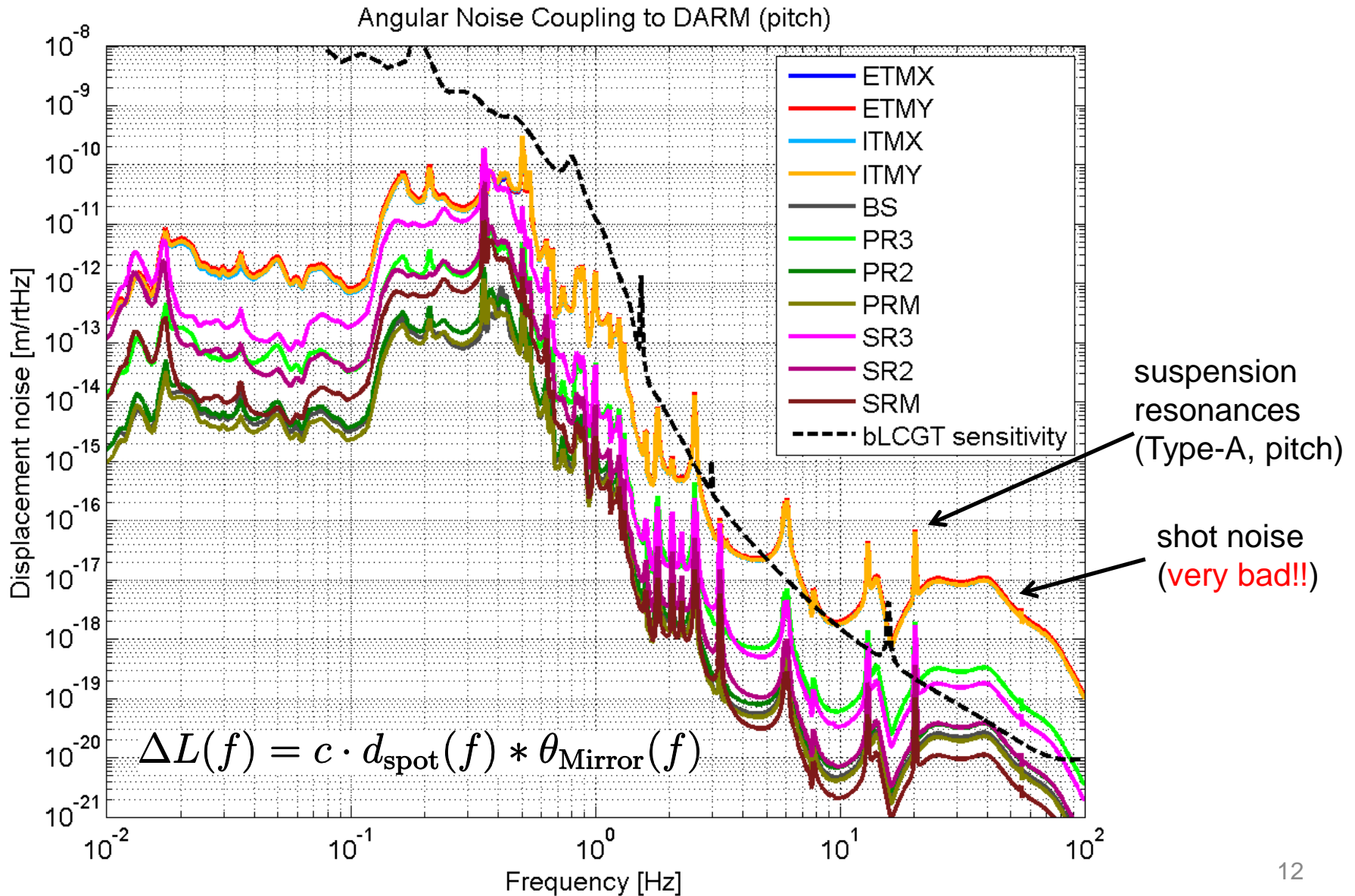


4. Beam spot motion

RMS ~ 0.3 mm for TMs



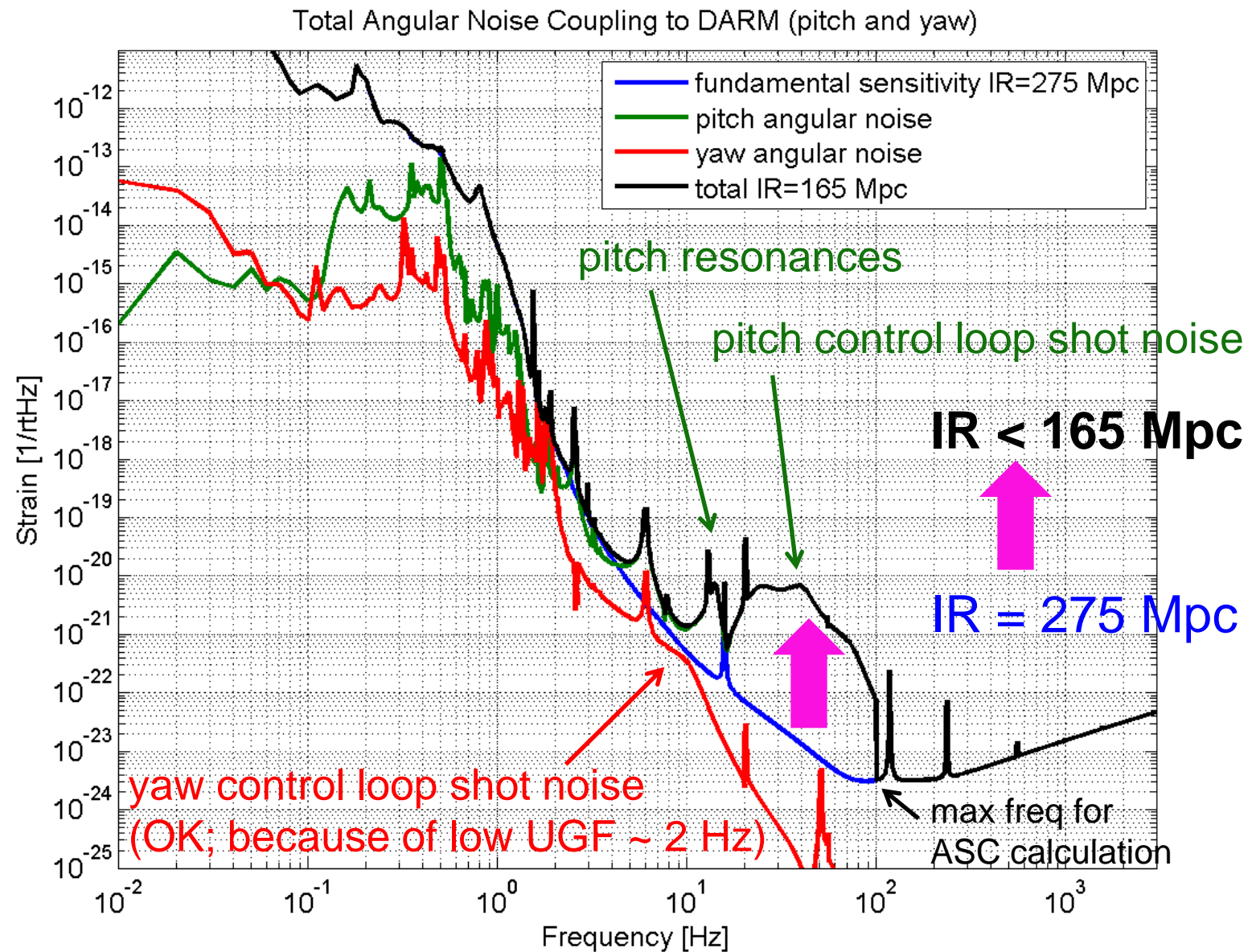
5. A2DARM coupling



6. Pitch and yaw

- plots above are for pitch control loop
 - do the same thing for yaw
- total A2DARM coupling

Total A2DARM coupling



How to reduce A2DARM?

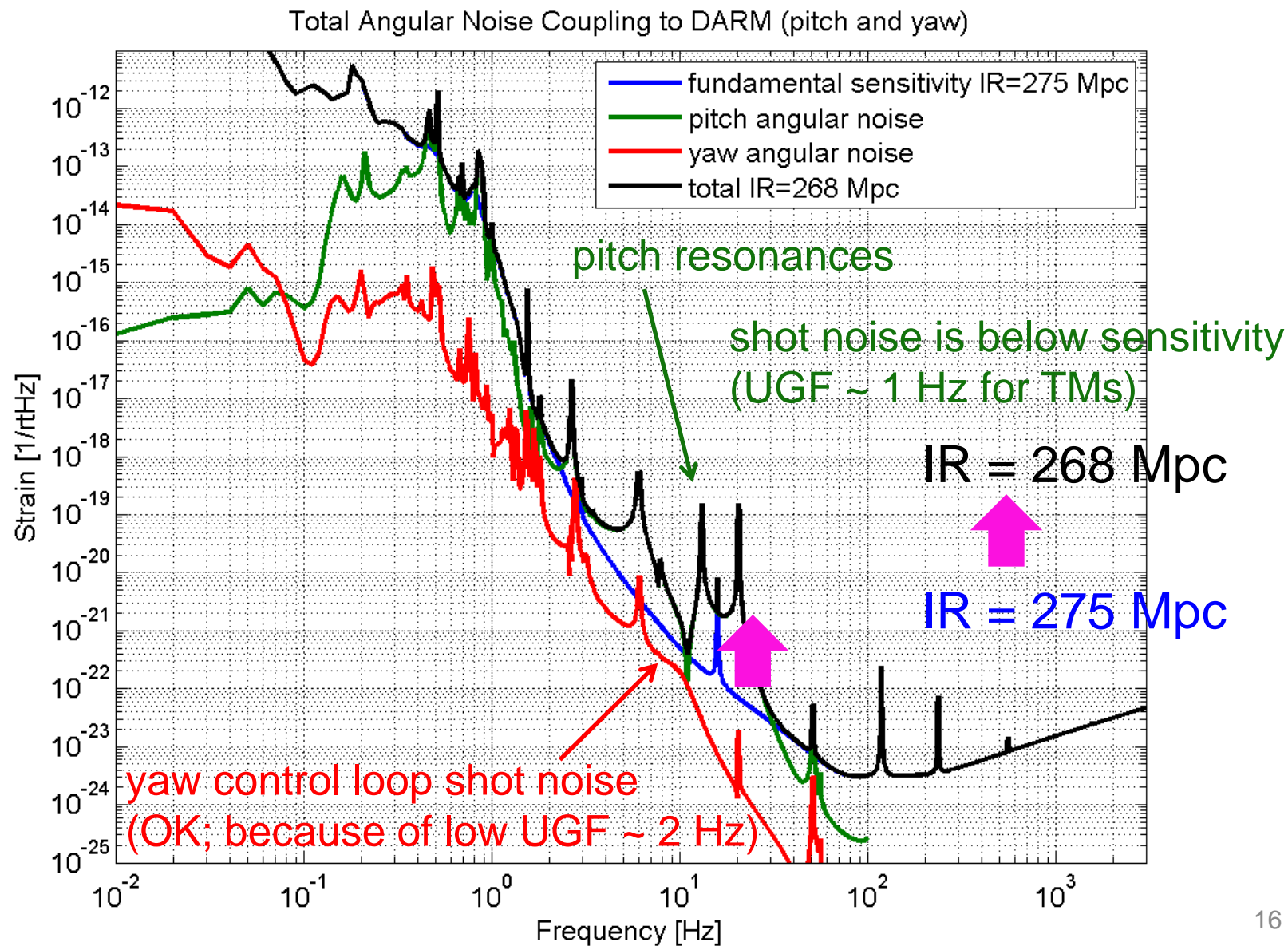
- make pitch SOFT mode stable
 - increase mechanical restoring torque of Type-A(TM) pitch by factor of ~20%
 - negative g-factor
 - smaller radiation pressure anti-spring
 - we can lower UGF of TM control
 - smaller beam spot motion

unstable if;

radiation pressure
anti-spring(SOFT mode) $>$ mechanical
restoring torque

current default design is positive g (ITM: flat, ETM: R=7 km)
negative g candidate is ITM: R=1.5 km, ETM: R=1.6 km

If negative g-factor.....



Reducing A2DARM even more

- employ local damping
 - particularly, pitch 0.5 Hz peak
(difficult to damp by WFS)
 - passive + active
 - refine suspension design
 - somehow move / damp pitch ~ 20Hz peaks
- work in progress

Future plans

- include strategic local damping
cooperation with vibration isolation group
- geometrical study of beam in IFO
for better DOF selection
- upgrade WFS tool
 - compare and check with aLIGO calculation
 - adopt AdVirgo method
 - include more noise
AS shot noise, seismic noise on QPD, WFS
broadband noise
 - currently, only mirror seismic and QPD
shot noise

Summary

- developed a tool for simulating / designing ASC
- evaluated A2DARM for current design
IR will be $< 165\text{Mpc}$
- proposed negative g-factor solution
- we need better suspension (pitch)
- lots of things to do to make this tool more relevant to reality!